

# **Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>th</sup> MALAYSIA GAMES**

# **Master-Thesis**

A thesis submitted in partial fulfillment of the requirements for the degree of

Master of Engineering in Membrane Structures (M.Eng.)

submitted to

Anhalt University of Applied Sciences

Faculty of Architecture, Facility Management and Geo Information

by

Siew Moi, Tan 22<sup>nd</sup> January 1962, Batu Pahat, Malaysia

Matrikel number : 4048307

Submission date: 18 August 2012

First Tutor: Prof. Robert Off

Second Tutor:



### Statement

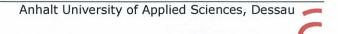
I hereby declare that the work presented in this Master thesis, entitled "Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>th</sup> MALAYSIA GAMES", is entirely my own and that I did not use any sources or auxiliary means other than those referenced.

Singapore, 18 August 2012

AL Tan Siow Moi

TAN SIEW MOI





3

	CONTENTS			8.4	LOADING AND STATICAL ANALYSIS
				8.5	LOCAL DESIGN CHECK
1.	INTRODUCTION	5 - 6		8.6	BIAXIAL TEXT
	1.1 THE REPORT			8.7	CUTTING PATTERN
	1.2 MALAYSIA			8.8	SUMMARY OF DETAILS
	1.3 MALAYSIA GAMES - SUKMA				
	1.4 PROJECT AND SITE		9.	STEEL E	RECTION
				9.1	LIFTING CHECK
2.	ARCHITECTURE CONCEPT & DESIGN DEVELOPMENT	7 - 15		9.2	ERECTION SEQUENCE
	2.1 ARCHITECT'S INTENT				
	2.2 DESIGN DEVELOPMENT		10.	MEMBRA	NE INSTALLTION
	2.3 FINAL DESIGN CONCEPT			10.1	MEMBRANE HANDLING
				10.2	MEMBRANE TENSIONING
3.	PROJECT ORGANISATION	16 - 17		10.3	ERECTION SEQUENCE
	3.1 FLOW CHART OF PROJECT EXECUTION				-
	3.2 GEOGRAPHICAL LOCATION OF PROJECT OFFICE		11.	APPEND	IX
				11.1	WORK PROGRAMME
4.	GENERAL INFORMATION	18 - 19		11.2	ENGINEERING DRAWINGS
	4.1 PROJECT BRIEF			11.3	ERECTION SEQUENCE
	4.2 REFERENCE DOCUMENT				PHOTO IMAGES OF STEEL WORK
	4.3 UNIT				PHOTOS IMAGES OF FABRIC WORK
	4.4 DESIGN CODE AND STANDARD				PHOTO IMAGES OF COMPARISON BEF
	4.5 COORDINATES SYSTEM				AERIAL VIEW PHASE 1 COMPLETION
	4.6 MATERIAL				AERIAL VIEW PHASE 1 COMPLETION -
	4.7 METHOD OF ANALYSIS				NEWS PAPER ARTICLES BEFORE THE
					PHOTO IMAGES DURING THE GAMES
5.	STRUCTURAL SYSTEM	20			BIAXIAL TEST REPORT
					DESIGN CALCULATION
6.	LOADING ASSUMPTION	21 - 23			
	6.1 SELF WEIGHT				
	6.2 DEAD LOAD OF CATWALK				
	6.3 PRESTRESS LOAD				
	6.4 IMPOSED LIVE LOAD				
	6.5 WIND LOAD				
7.	STEEL ANALYSIS AND DESIGN	24 - 34			
	7.1 DESIGN METHOD				
	7.2 DESIGN MODEL				
	7.3 BASIC LOAD CASES & LOAD COMBINATION				
	7.4 BOUNDARY CONDITION				
	7.5 DESIGN OF STEEL MEMBER				
	7.6 LOCAL DESIGN CHECK				
	7.7 SUMMARY OF CONNECTION DETAILS				
8.	MEMBRANE ANALYSIS AND DESIGN	35 - 47			
	8.1 GENERAL INFORMATION				
	8.2 FORM FINDING				

TAN SIEW MOI

8.3 CONTOUR



49 - 50 51 52 - 53 54 - 72 73 - 80 81 - 87 88 - 94 N BEFORE & AFTER ERECTION 95 - 97 ΓΙΟΝ 98 -99 TION - IMPRESSION 100 - 101 THE GAMES 102 - 103 AMES 104 - 105 106 - 113 114 - 153

C

48 - 49

#### 1. INTRODUCTION

#### 1.1 THE REPORT

This report is about the design, analysis, detailing, fabrication and execution of tensile membrane roof over existing Wisma Belia swimming pool at Kuantan for aquatic events for the XV Malaysia Games from 7th July to 16July 2012.

#### 1.2 MALAYSIA

Malaysia is located in Southeast Asia, just north of the Equator. It comprise of East Malaysia and Peninsula Malaysia. They comprise of 13 states and 3 federal territories. Malaysia is the only federal constitutional monarchy in Southeast Asia.

th Chin 66"30 N Malaysia ASIA EUROPE 🜐 worldatlas CANCER (Sumatra Malaysia LICK HERE FOR LARGER MAP MALAYSIA 150 mi AFRICA (C) Grap Ocean TROPIC OF 23051 1500 mi AUSTRALIA 🕀 worldatlas 1500 km

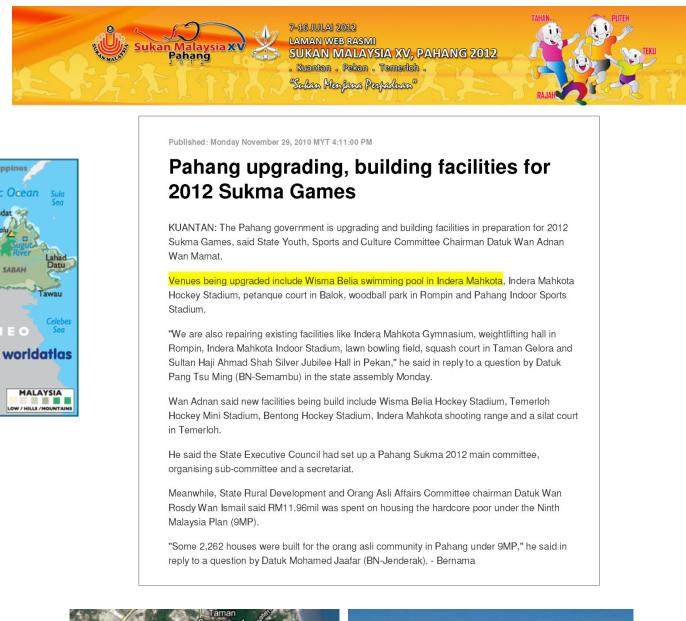
The population is estimated to be about 29 millions (July,2011 est.) and represented by the multiple ethnic groups of mainly of Malays 50.4%, Chinese 23.7%, indigenous 11%, Indian 7.1% and others 7.8% (2004 est.). And the official language is Bahasa Malaysia.

#### 1.3 MALAYSIA GAMES - SUKMA

In 1986, Malaysian Games SUKMA which is an acronym for Sukan Malaysia in Malay language is introduced to unearth new talents for international competition and also to rapport harmony among the multiple ethnic populations.

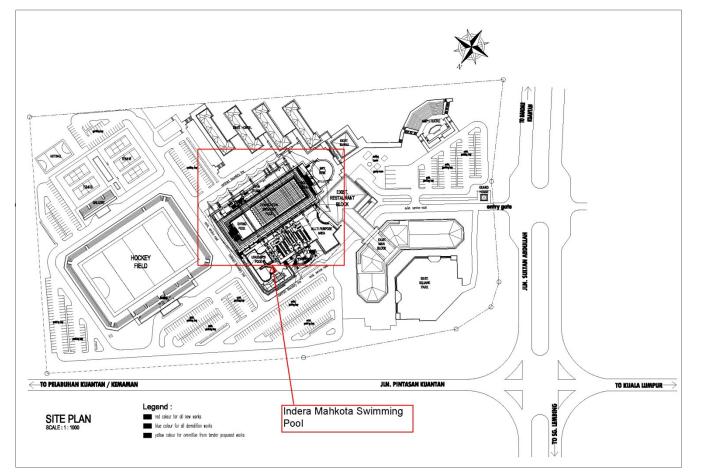
It was a biyearly event which was first held in Kuala Lumpur, the capital of Malaysia. It was change to annual event in 2011 and this year 2012 the 15<sup>th</sup> Malaysia Games is hosted by state of Pahang from 7 July to 16 July. Pahang is on the east coast of Peninsula Malaysia.

At end of 2010, the Pahang state government announced to upgrade building facilities for 2012 Sukma Games. And the existing Wisma Belia swimming Pool at Indera Mahkota (Indera Mahkota Youth Complex), Kuantan is one of the chosen venue for aquatic events.





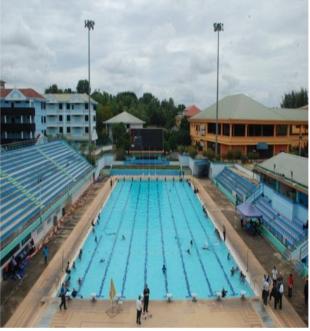




SITE PLAN



EXISTING POOL LOOKING TO HOCKEY STADIUM AT FAR END



EXISTING POOL LOOKING TO EXISTING RESTAURANT

TAN SIEW MOI



EVENT SIGNBOARD FOR SWIMMING EVENTS





EVENT SIGNBOARD BESIDE ENTRY GATE







BANNERS ALONG ROAD TO SITE



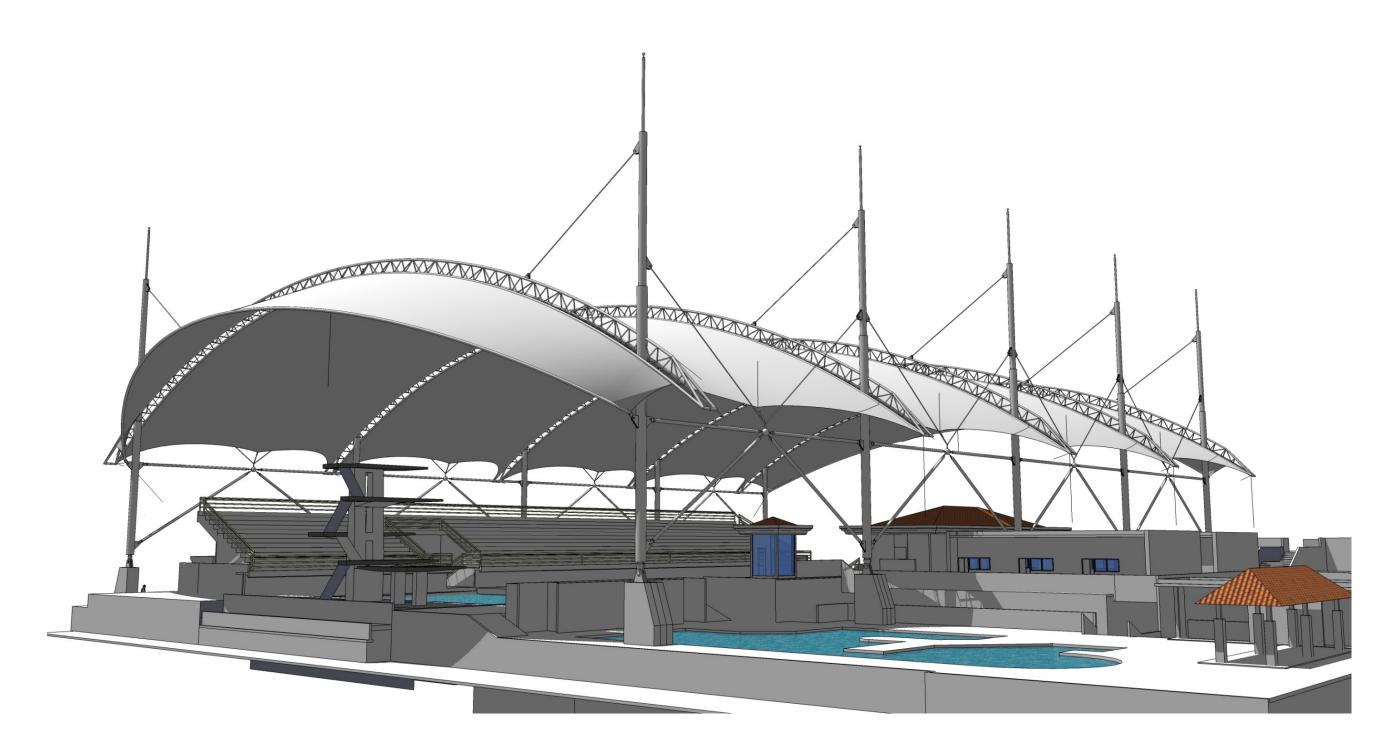


MORE BANNERS ALONG ROAD TO SITE



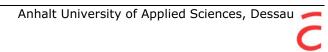
## 2. ARCHITECTURE CONCEPT & DESIGN DEVELOPMENT

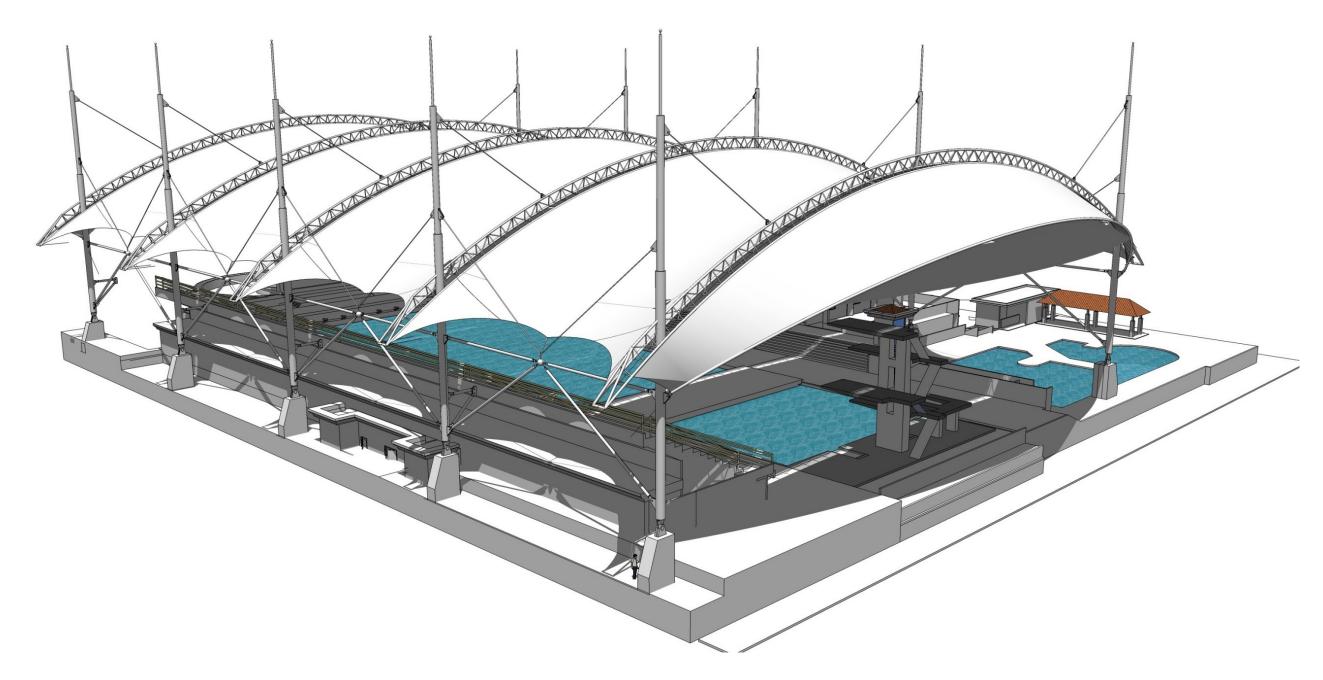
### 2.1 ARCHITECT'S INTENT



VIEW FROM FRONT





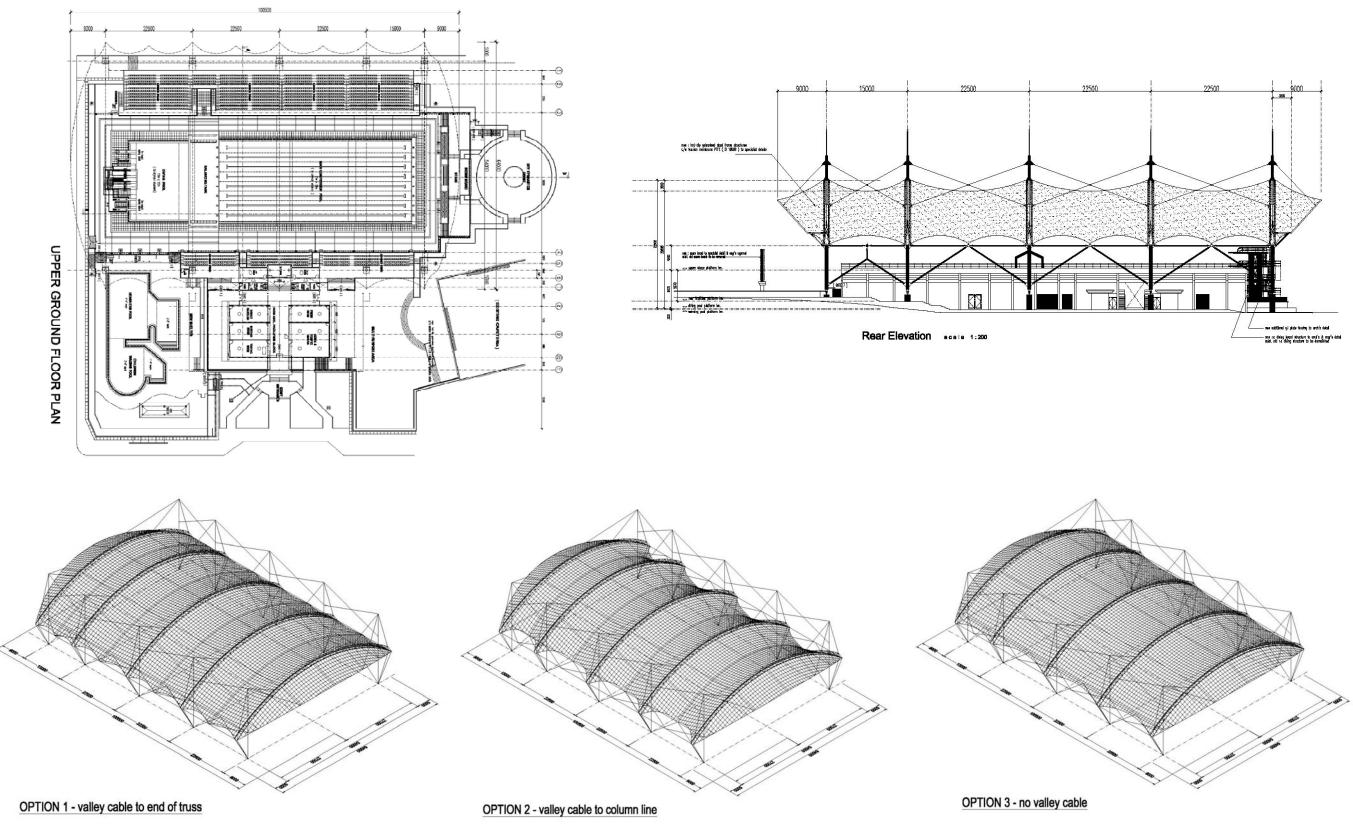


# VIEW FROM REAR



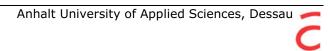
### 2.2 DESIGN DEVELOPMENT

# 2.2.1 ORIGINAL UNEQUAL GRIDS



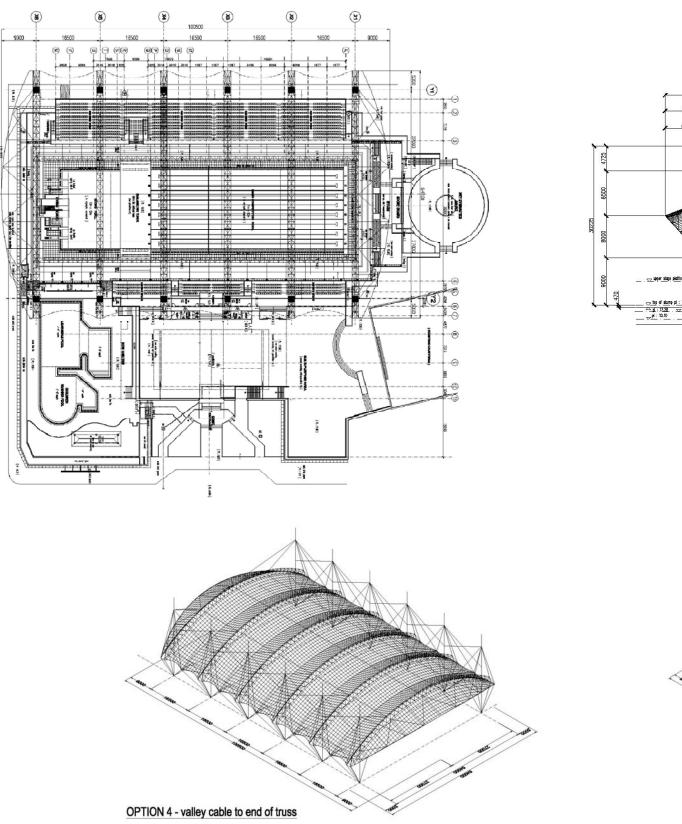
TAN SIEW MOI

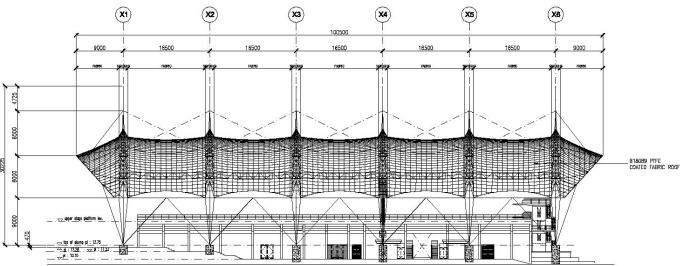




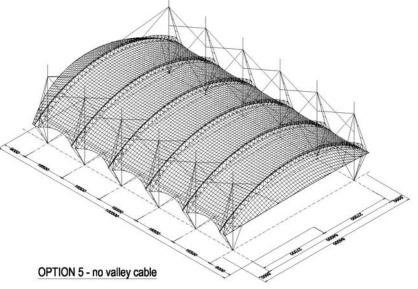
9

FLOOR PLAN



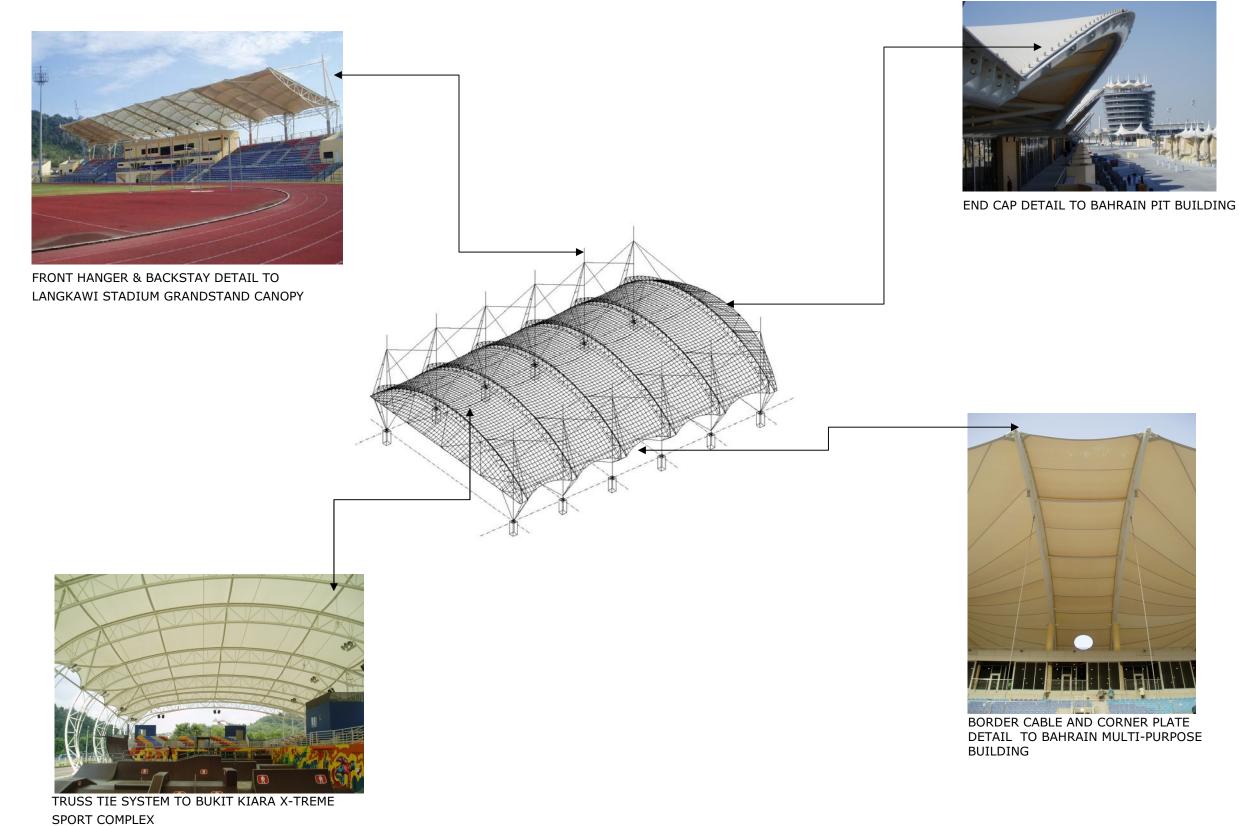


REAR ELEVATION





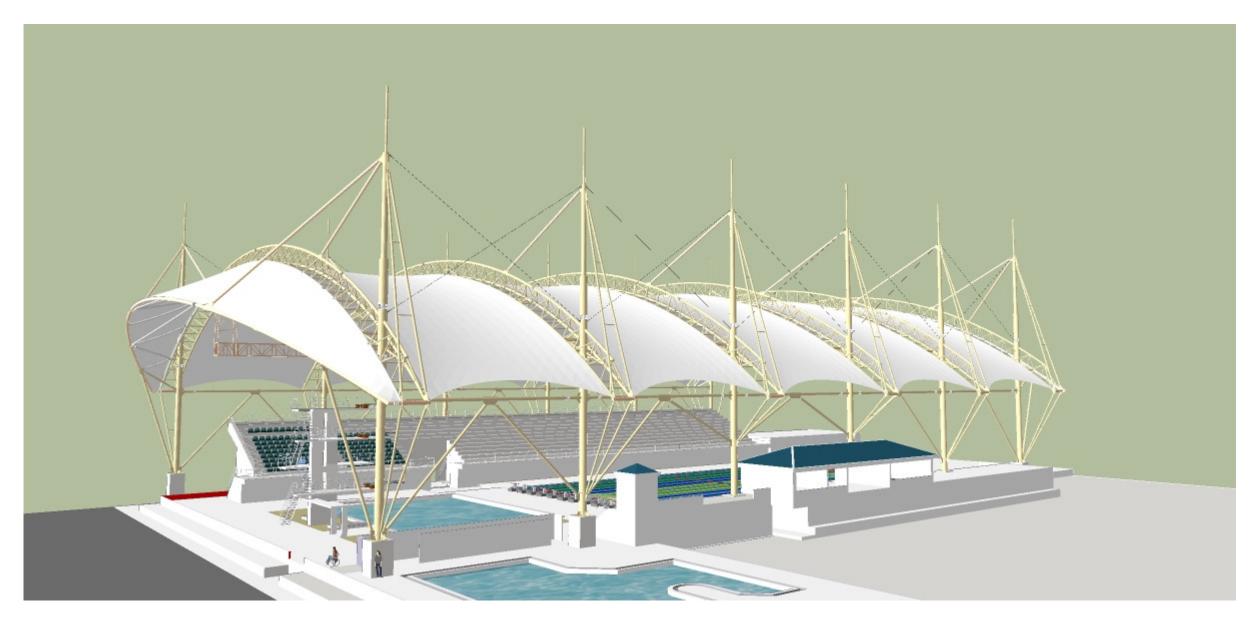
#### 2.2.3 DETAILS AND DESIGN REFERENCE FROM JOB DONE



TAN SIEW MOI

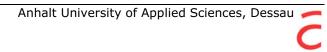


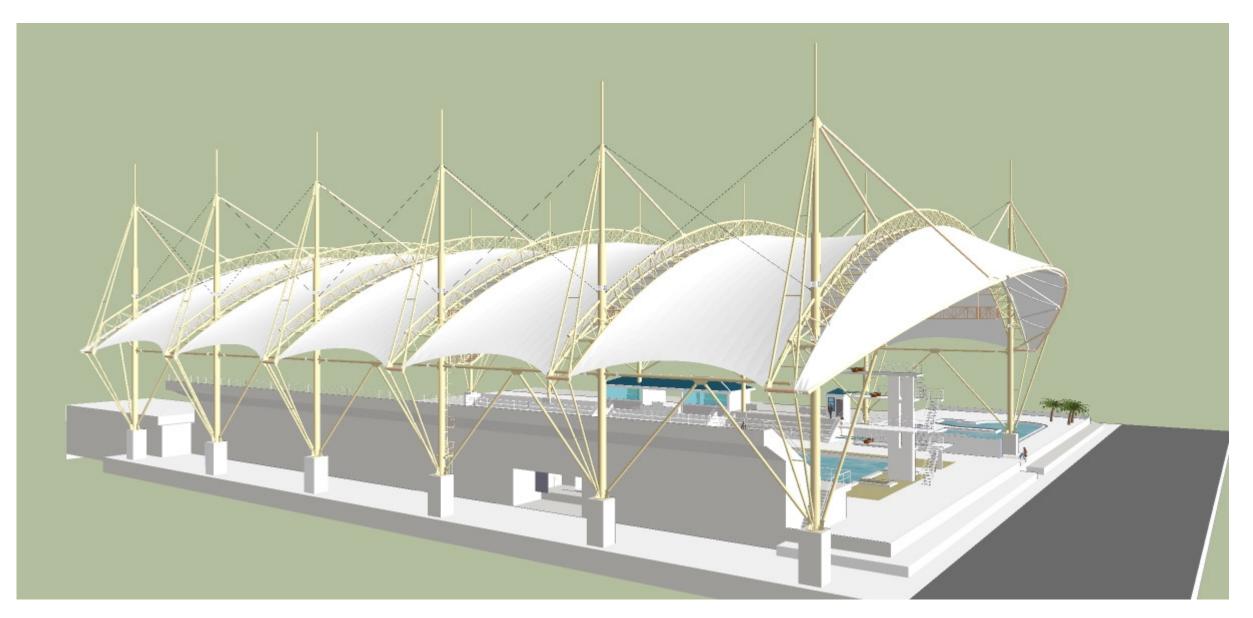
# 2.3 FINAL DESIGN CONCEPT



# VIEW FROM FRONT

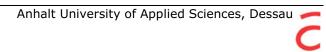


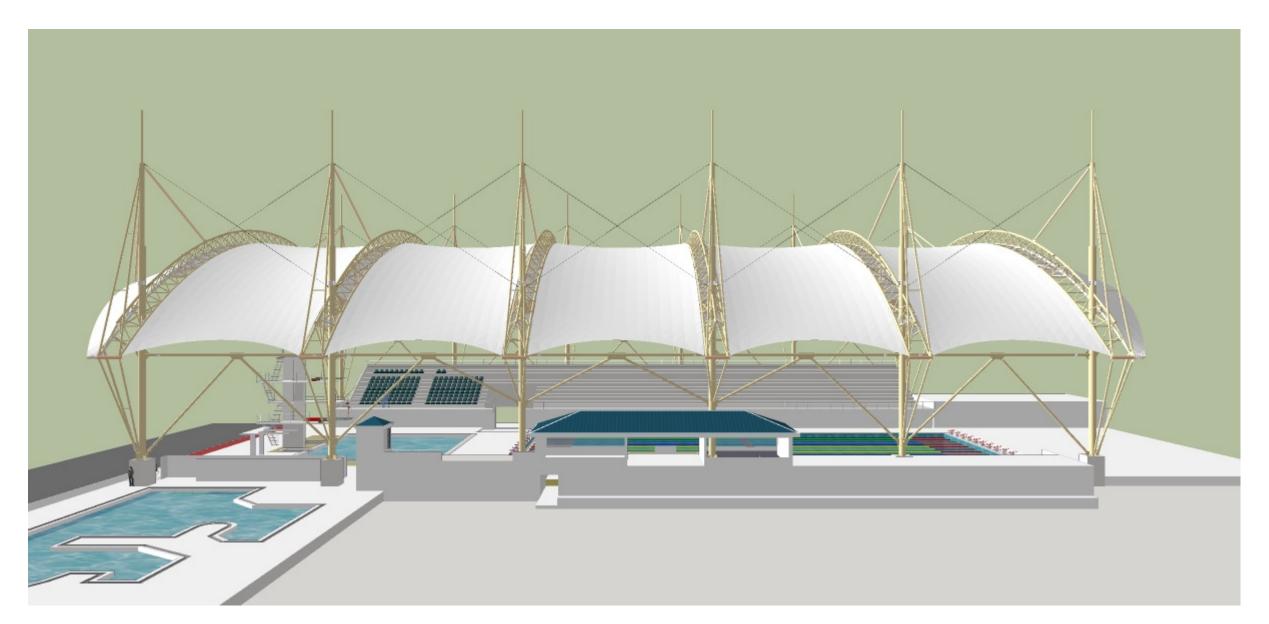




# VIEW FROM REAR

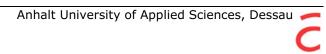






# FRONT ELEVATION

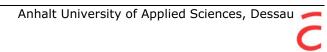






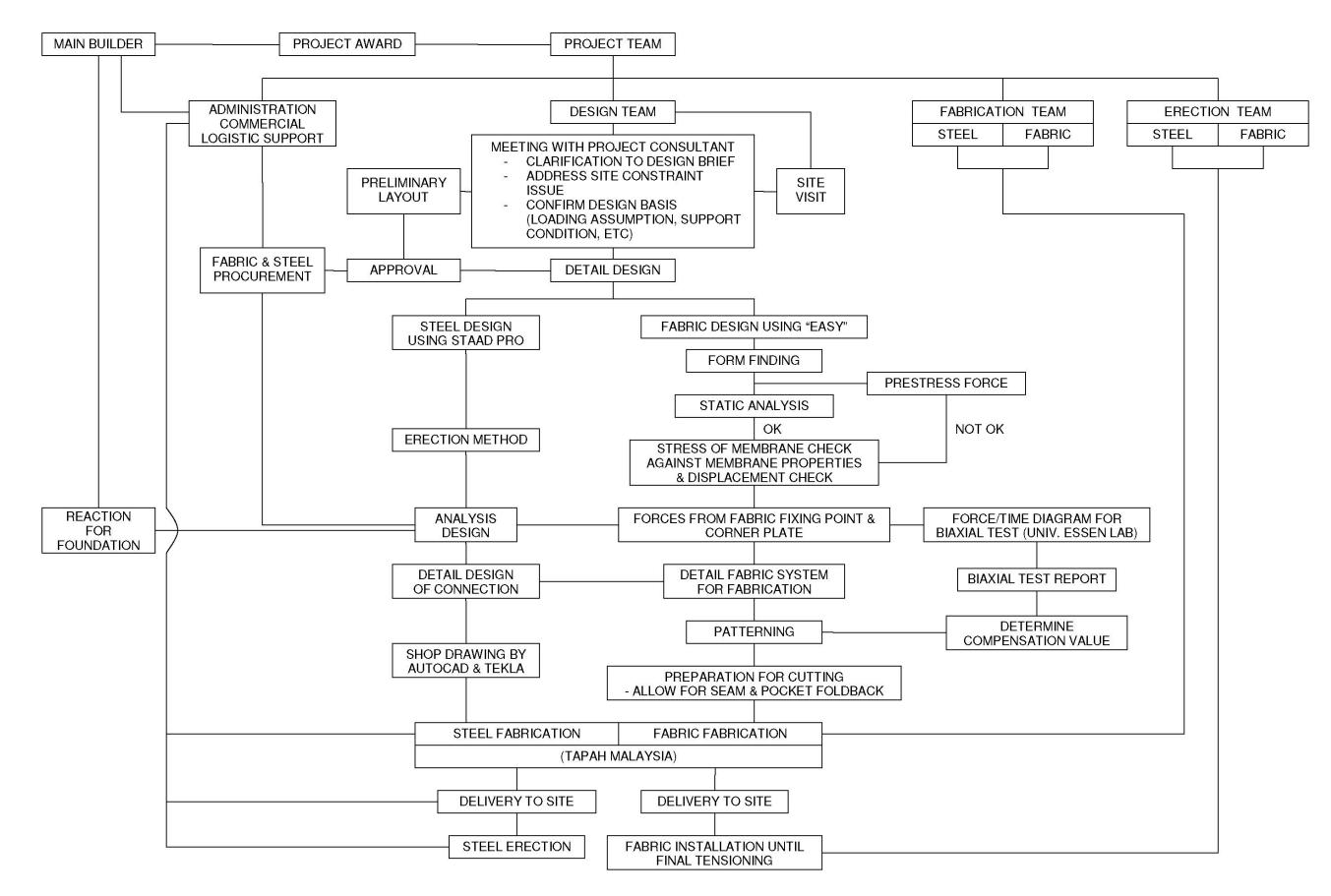
# **LEFT ELEVATION**





### 3. PROJECT ORGANISATION

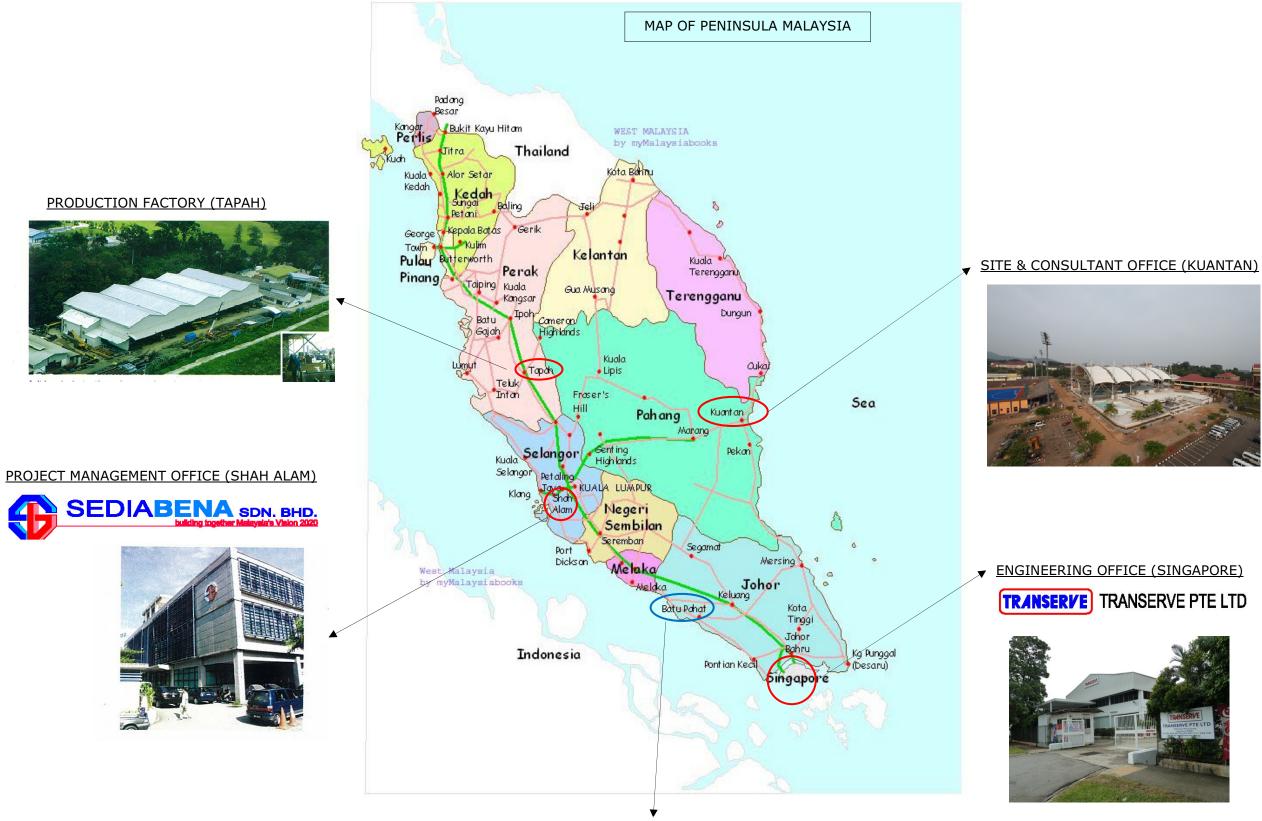
### 3.1 FLOW CHART OF ENGINEERING DESIGN PROCESS IN RELATION TO PROJECT EXECUTION



TAN SIEW MOI







My home town (Batu Pahat)



#### 4. GENERAL INFORMATION

#### 4.1 PROJECT BRIEF

The proposed tensile PTFE (polytetrafluoroethylene) coated glass fiber roof is under the care of the Kuantan Town Council or Majlis Perbandaran Kuantan (MPK) in Malay language. The roof cover a main competition pool of 21m x 50m and a diving pool of 15m x 20m, both are of Olympic standard. The membrane used is B18089 of Verseidag, Germany. The foot print of the roof is approximately 100m x 64m on plan.

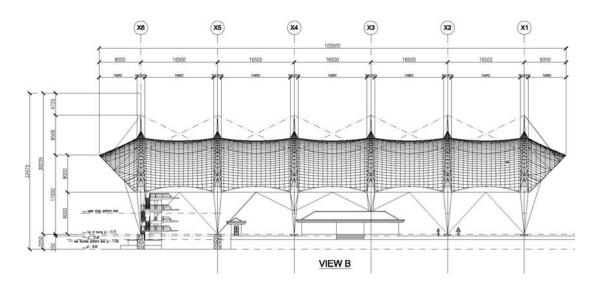
The swimming pool roof is a barrel vault like structure of 82.5m length with both end a eyelid canopy cantilevered 9m out and sloped 24 deg downward.

The steel roof structure comprise of 6 nos of 3D triangular truss of 1.7m width x 1.5m constant depth and spaced at 16.5m. Each truss is integrated with steel mast at 54m center to center at both end. The overall height of columns are 30m and top of truss is 22m above the general pool level. These columns are stabilized with front hanger and upper and lower backstay at rear. There are 1 column near the main entrance which 'punch' through the existing roof of the VIP room. The overall structure are braced longitudinally along the column gridline and also 3 single member curved tie beam at 3 location of bottom chord of the 3D truss. The base of column mast is then bolted to the precast holding down bolt to 1.5mx1.5m RC stump. And all steel frame are bolted connections.

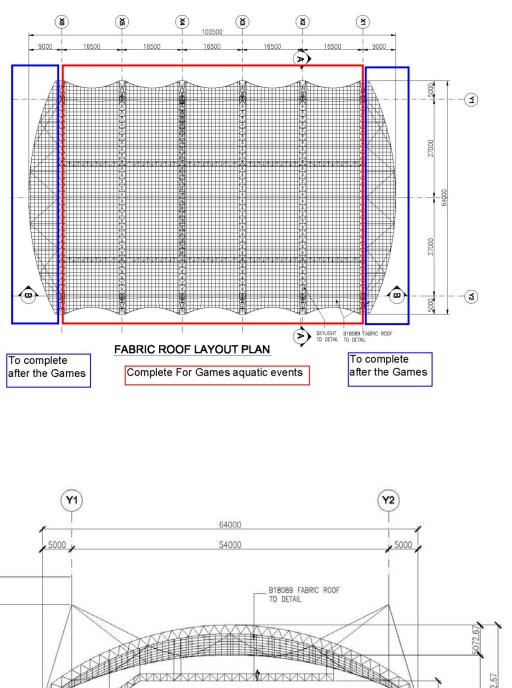
Approximately 220m run of 1.2m wide catwalk is hanged from these 3D truss at 15 location to provide access for maintenance of light fitting which is also fixed on the railing of catwalk.

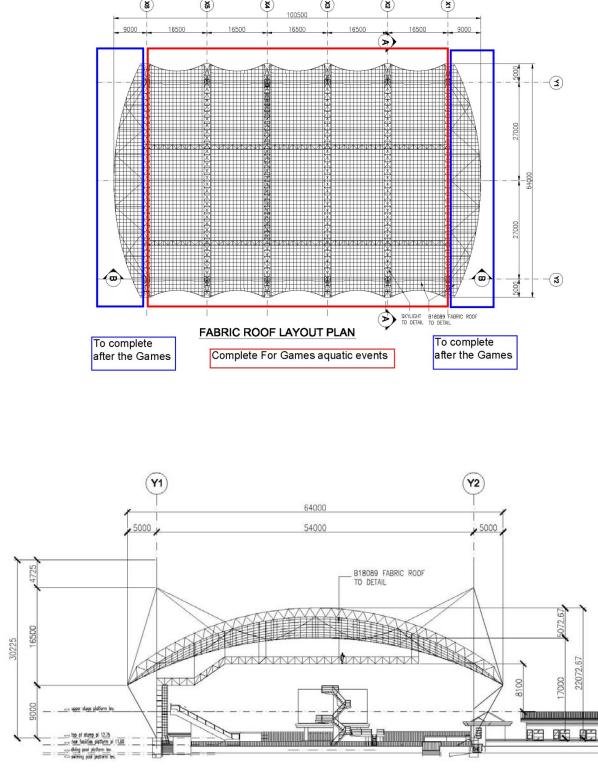
The fabric roof is make up of 5 internal panels and 2 end panels. The internal fabric panel is fixed across the bottom chord of 2 nos of 3D truss at 16.5m center to center and inside of the triangular truss is then fixed with 4mm thick solid polycarbonate sheet.

In summary, the project contract of approximately 6.2 million Malaysia Ringgit is to be completed in 5 months time for 6000m<sup>2</sup> of membrane, 250 tons of steel frame, and 25 tons of 220m long of catwalk.



In considering the short project time, it is agreed with the client MPK that there will be 2 phase of completion, before the games to finished installed all 5 internal panels from gridline X1 to X6 and after the games to continue to completed the 2 remaining end frame.





**VIEW A** 



#### 4.2 **REFERENCE DOCUMENTS**

Malaysia Standard MS 1553 : 2002 Code of Practice on Wind Loading For Building Structure

#### 4.3 UNIT

The S.I system shall be used : ie mm, m, KN and etc

#### 4.4 DESIGN CODE AND STANDARD

CP 3 : Chapter V-2 : 1993 Incorporating Amendment Nos. 1, 2, 3, 4 and 5 - Wind Loads

BS 6399 : Part 1 : 1996 – Code of practice for dead and imposed loads

BS 6399 : Part 3 : 1988 – Code of practice for imposed roof loads

BS 5950-1 : 2000 – Code of practice for design – Rolled and welded sections

#### 4.5 COORDINATES SYSTEM

The design model structural axis system is as follow:

- +X from grid line X6 to X1
- +Y from grid line Y2 to Y1
- +Z vertically up

### 4.6 MATERIAL

#### 4.6.1 STEEL

All circular hollow section to BS EN 10210 S275 or equal and general plates to BS EN 10025 S275 or equal. The corner plate is using S355 material. The choice of material used is subject to availability of material. For analysis and design of the structure steel roof, yield stress of 275  $N/mm^2$  is assumed.

#### 4.6.2 CABLE

Border cable use PE coated galvanized steel wire rope, and safety cable is galvanized steel wire rope dry type.

#### 4.6.3 MEMBRANE

PTFE fabric B18089 from Verseidag, Germany.

#### 4.7 METHOD OF ANALYSIS

The analysis of the tensioned membrane structure is done in two parts. Firstly is to do the form finding of the membrane. Then by using the forces from the static analysis of the prestressed membrane and applied to the steel structure and do a design check of the steel structure.

#### 4.7.1 FABRIC ROOF

The task of determining appropriate forms of the membrane based on the given outline is using the software EASY from Germany.

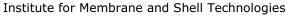
The EASY form finding method is based on the method of force density algorithm. After the equilibrium shape is formed, the form is then applied with external load, ie imposed load, wind load and etc. and static analysis of the fabric is then carried out.

External load which will be applied to the surface of the membrane will be represented by nodal forces.

#### 4.7.2 STRUCTURAL STEEL SYSTEM

The output forces from the membrane for all the load case from EASY is then extract for use as input forces to the structural steel and then for design purposes.

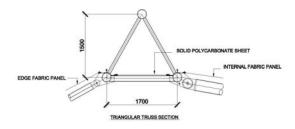
The finite element software used for the steel analysis is STAAD PRO2007, developed by Research Engineers International, USA.



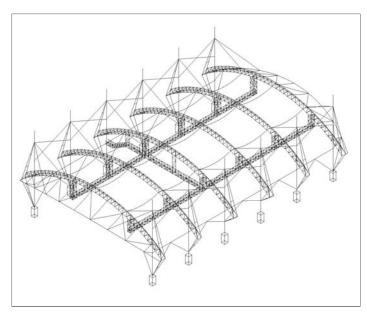


#### 5. STRUCTURAL SYSTEM

The steel roof structure comprise of 6 nos of 3D triangulated truss of 1 top chord 1.5m height and 2 bottom chord of 1.7m wide. These trusses are spaced at 16.5m and integrated with steel column at 54m center. The overall length of the truss is 64m with 11.6m rise at the center. Each of these integrated truss with column height of 30m is stabilized with 1 front stay and 2 upper and lower backstay.



The 3D trusses is also providing supports to about 220m run of catwalk at 15 location of general 4 hanging point each. There are 2 row of 82.5m long catwalk parallel to and about 15m high from the swimming pool. Between these catwalk, there is interconnecting link along gridline X4. The catwalk is approximately 1.2m wide x 1.2m high.

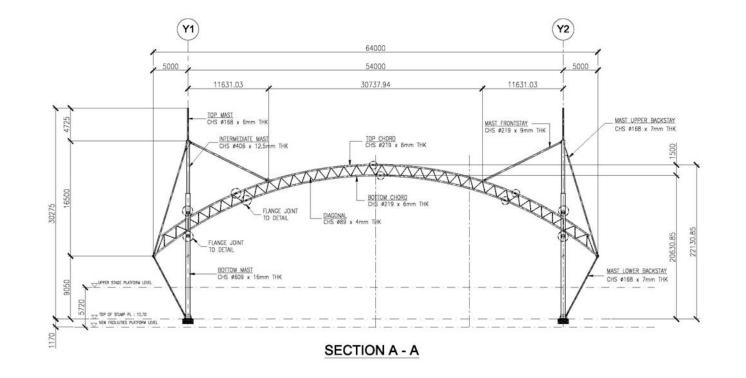


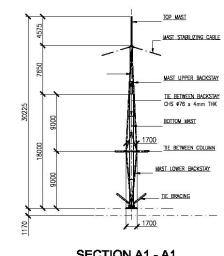
3D VIEW OF CATWALK SUPPORT BY TRIANGULAR TRUSSES

The stability of the structure is dependent on ties and bracing along the column longitudinally. They are also tied quarterly at 3 locations across the bottom chord of the trusses. At the upper part of the column, a pair of crossly brace safety cable is introduced.

Due to limitation and constrain for site access, the steel structure is designed such that it will be able to be lifted by a small tonnage crane eg. 30 tons and so bolted connection is decided.

The 64m truss is then make up of 4 segment with flange joint connection. The 30m high column is divided into 3segment and connected at just before and after the 3D truss with flange joint. So is the bracing and ties along the columns, and the end canopies frame are also assembled in 3 parts by bolting system.





SECTION A1 - A1

TAN SIEW MOI





Anhalt University of Applied Sciences, Dessau 🦟

#### 6. LOADING ASSUMPTION

The fabric roof and steel structure is subjected to the following loading:

- a) Self weight of steel truss, column, bracing etc.
- b) Dead load of catwalk
- c) Prestress force in the membrane
- d) Imposed live load on membrane roof and catwalk
- e) Wind load

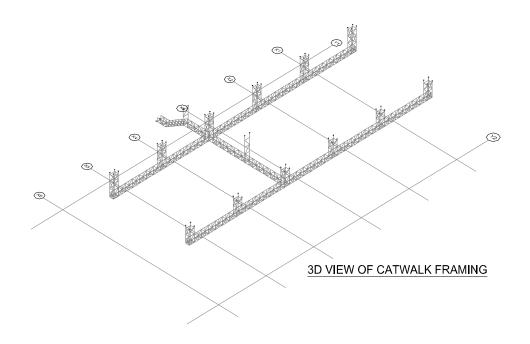
#### 6.1 Self weight (SW)

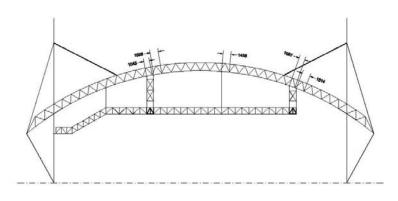
Self weight of steel member = automatically calculated in the software

Self weight of fabric =  $1.15 \text{ kg/m}^2$ (Insignificant so it is ignored in the membrane load)

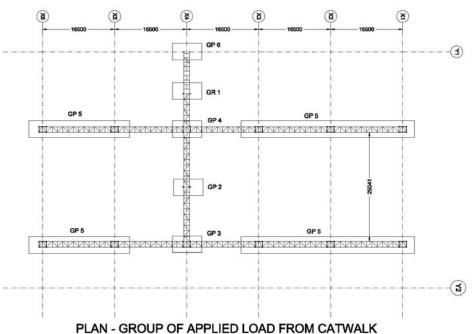
### 6.2 Dead Load of catwalk (DCW)

The catwalk is supported from the 3D truss at 15 Groups of generally 4 point from the bottom chord at 1.7m x 1.275m apart each except at gridline X4 where it is the main access.





## SECTION VIEW AT GRIDLINE X4



The weight of catwalk with expanded mesh + M&E load assumed to be 150 kg/m run Group 1 load per point =  $[(7.544+7.2)/2 \times 150]/2 = 553 \text{ kg} (5.53 \text{ KN})$ Group 2 load per point =  $[(25/2) \times 150]/2 = 937 \text{ kg} (9.4 \text{ KN})$ Group 3 load per point =  $[(16.5 + 6.25) \times 150] / 4 = 853 \text{ kg} (8.53 \text{ KN})$ Group 4 load per point =  $[(6.25 + 16.5 + 7.55/2) \times 150]/4 = 995 \text{ kg} (9.95 \text{ KN})$ Group 5 load per point =  $(16.5 \times 150) / 4 = 618 \text{ kg} (6.2 \text{ KN})$ Group 6 load per point =  $[(7.544/2 + 3.3) \times 150]/2 = 530 \text{ kg} (5.3 \text{ KN})$ 



#### 6.3 Prestress Load (PRE)

Prestress is induced to increase membrane stiffness and obtain a stable form which is in equilibrium. In this case, a prestress force of 3KN/m is assumed for warp and weft direction.

#### 6.4 Imposed Live Load

6.4.1) Membrane roof (VL)

Imposed live load on membrane roof =  $0.25 \text{ KN/m}^2$ 

This load is applied vertically downward to the fabric roof.

6.4.2) Catwalk (LCW)

For localized catwalk design, assumed live load =  $1.5 \text{ KN/m}^2$ 

For global analysis of the structure roof, assumed live load applied simultaneously on all catwalk =  $0.75 \text{ KN/m}^2$ 

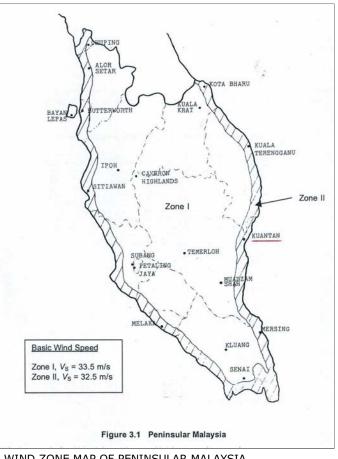
Using the same loading group as in the dead load case, Live load =  $0.75 \text{ KN/m}^2 \times 1.2 \text{m}$  internal clearance of catwalk = 0.9 KN/m

Group 1 load per point =  $[(7.544+7.2)/2 \times 0.9]/2 = 3.32$  KN Group 2 load per point =  $[(25/2) \times 0.9]/2 = 5.62$  KN Group 3 load per point =  $[(16.5 + 6.25) \times 0.9]/4 = 5.12$  KN Group 4 load per point =  $[(6.25 + 16.5 + 7.55/2) \times 0.9]/4 = 5.96$  KN Group 5 load per point =  $(16.5 \times 0.9)/4 = 3.71$  KN Group 6 load per point =  $[(7.544/2 + 3.3) \times 0.9]/2 = 3.18$  KN

#### 6.5 Wind Load

Reference to Malaysian Standard MS 1553 :2002 : Code of Practice on wind loading for Building Structure

As Kuantan fall in Zone II as shown in Figure 3.1, so basic wind speed of 32.5 m/s is adopted for the wind load calculation.



WIND ZONE MAP OF PENINSULAR MALAYSIA

Reference to CP3 : Chapter V : Part 2 1993 for dynamic wind pressure

Dynamic pressure due to wind is given by :

 $a = k V s^2 N/m^2$ 

where k = 0.613

Vs = VxS1xS2xS3

Basic wind speed V = 32.5 m/s

S1 - topography factor = 1.0S2 - ground roughness, structure size and height above ground factor

Ground roughness = 3Maximum height = 20 mClass = CTherefore S2 = 0.85

S3 – statistical factor = 1.0

Vs = 32.5x1.0x0.85x1.0 = 27.6 m/s $q = 0.613 \times 27.6 \times 27.6 = 467 \text{ N/m}^2 \text{ say } 0.5 \text{ KN/m}^2$ 



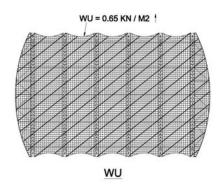
Anhalt University of Applied Sciences, Dessau 🦟

Assumed the fabric roof is duopitch canopy of roof angle approx = 20 deg

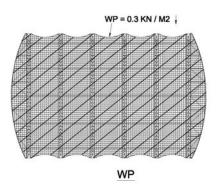
Therefore from Table 13, Assumed the entrance and audience stand is 100% obstruct,

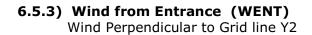
Solidity ratio  $\emptyset = 1$  (obstruct) Min Overall Cp = -1.3 and Max Overall Cp = +0.6

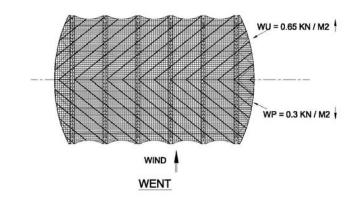
6.5.1) Wind Uplift (WU) Wind uplift  $Wu = -1.3 \times 0.5 = -0.65 \text{ KN/m}^2$ 



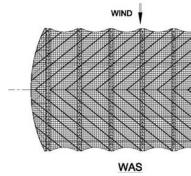
6.5.2) Wind Pressure (WP) Wind pressure Wp =  $+0.6 \times 0.5 = 0.3 \text{ KN/m}^2$ 



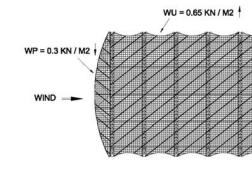




6.5.4) Audience stand (WAS) Wind Perpendicular to Grid line Y1 WIND

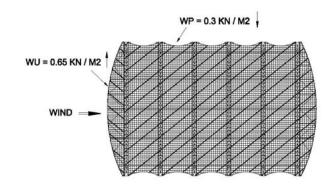


6.5.5) Wind from Driving Pool Side when End bay is Wind Pressure (WDP\_P) Wind Perpendicular to Grid line X6



WDP\_P

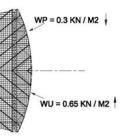
6.5.6) Wind from Driving Pool Side when End bay is Wind Uplift (WDP\_U) Wind Perpendicular to Grid line X6



WDP\_U

TAN SIEW MOI

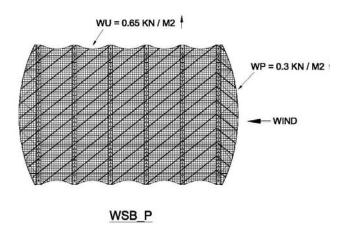




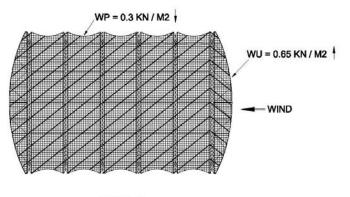




6.5.7) Wind from Score Board Side when End Bay is Wind Pressure (WSB\_P) Wind Perpendicular to Grid line X1



6.5.8) Wind from Score Board Side when End Bay is Wind Uplift (WSB\_U) Wind Perpendicular to Grid line X1



WSB U

#### 7. STEEL ANALYSIS AND DESIGN

#### 7.1 DESIGN METHOD

For the in-placed analysis there will be 2 limit state analysis, service limit state and the ultimate limit state.

The service limit state relate to performance under normal service conditions, e.g deflections. And ultimate limit state are related to safety and load carrying capacity of the structure where the specified loads is multiplied by relevant partial factor.

The design facility available in STAADPRO software shall be used to code check the members for member forces and moment due to the various loading combinations for both limit states.

## 7.2 DESIGN MODEL

The steel structure has been modeled as a 3 dimensional frame model along the center line of the steel section. The ends of frame member are connected by nodes. All the steel member in this case uses all circular hollow section.

All the steel member are assumed to be frame type except the mast frontstay, backstay, ties between truss and bracings between column. These are assumed to be truss member which will have a bolted connection at both end.

The stabilizing cable between top of mast are assumed to be tension only Member with small diameter solid round bar representing the cables.

The following properties is used for the analysis on the steel member: -

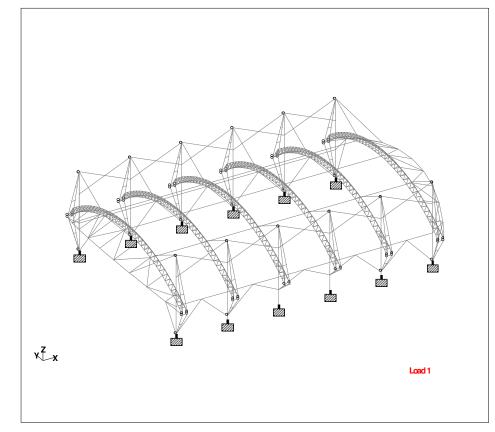
Young's Modulus =  $2.10E08KN/m^2$ Shear Modulus =  $8.0E07 \text{ KN/ } \text{m}^2$ Poisson Ratio = 0.3Mass density of steel =  $7850 \text{ kg/m}^3$ Gravitational acceleration =  $9.81 \text{ m/s}^2$ Coefficient of thermal expansion = 11.7E-06 /deg C



Anhalt University of Applied Sciences, Dessau 🦟

For ease of reference, the steel member of the design model has been group as follow;

- a) member 1 to 456 = bottom curved chord of 3D trussb) member 457 to 536 = edge member of eyelid canopy c) member 537 to 782 = bottom horizontal chord of 3D truss d) member 783 to 992 = top curved chord of 3D truss e) member 993 to 1928 = diagonal chord of 3D truss f) member 1929 to 1962 = bracing and prop member to eyelid canopy g) member 1963 to 1977 = tie member between 3D truss h) member 1978 to 2041 = lower, intermediate and upper mast i) member 2042 to 2061 = tie member at between lower masts j) member 2062 to 2077 = mast front stay k) member 2078 to 2193 = mast backstay I) member 2194 to 2227 = internal short tie of backstay m) member 2228 to 2255 = longitudinal bracing between lower mast
- n) member 2256 to 2275 = stabilizing cable at intermediate mast



7.3. BASIC LOAD CASES & LOAD COMBINATION

The membrane roof and steel structure system are analyzed based on the following load cases and load combinations.

#### 7.3.1 BASIC LOAD CASES

LOAD 1	(SW) =	Self weight of steel structure au software
LOAD 2	(DCW)	= Dead load of catwalk + ME loa
LOAD 3	(LCW)	= Imposed Live Load on catwalk

LOAD 4 (PRE) = Prestress load from membrane roof WITHOUT any external load

The following external load is applied on to a stable and prestressed membrane form. So the following load case actually consist of prestressing load.

LOAD 5 (VL) = Imposed Live Load on membran
LOAD 6 (WU) = Wind Uplift on membrane roof
LOAD 7 (WP) = Wind Pressure on membrane roo
LOAD 8 (WENT) = Wind from Entrance side (Y2)
LOAD 9 (WAS) = Wind from Audience Stand ( $\gamma$
LOAD 10 (WDP_P) = Wind from Driving Pool side
LOAD 11 (WDP_U) = Wind from Driving Pool side
LOAD 12 (WSB_P) = Wind from Score Board sid
LOAD 13 (WSB_U) = Wind from Score Board sid
And all the above load case are unfactored load.

STEEL DESIGN MODEL



```
utomatically calculated by the
```

```
bad
```

ne roof

```
oof
```

(Y1)

le (X6), End bay wind pressure

de (X6), End bay wind uplift

ide (X1), End bay wind pressure

de (X1), End bay wind uplift

#### 7.3.2. SERVICE LOAD COMBINATION

LOAD 100 =	SW + DCW + PRE
LOAD 101 =	SW + DCW + LCW + VL
LOAD 102 =	SW + DCW + WU
LOAD 103 =	SW + DCW + WP
LOAD 104 =	SW + DCW + WENT
LOAD 105 =	SW + DCW + WAS
LOAD 106 =	SW + DCW + WDP_P
LOAD 107 =	$SW + DCW + WDP_U$
LOAD 108 =	SW + DCW + WSB_P
LOAD 109 =	SW + DCW + WSB_U

#### 7.3.3 ULTIMATE LOAD COMBINATION

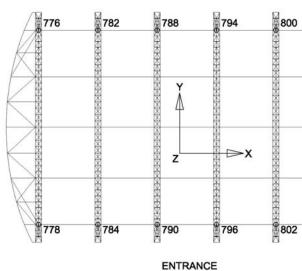
LOAD 200	=	1.4(SW + DCW+PRE)
LOAD 201	=	1.4(SW+DCW) + 1.6(LCW+VL)
LOAD 202	=	1.0(SW + DCW) + 1.4WU
LOAD 203	=	1.2(SW + DCW) +1.2WP
LOAD 204	=	1.2(SW + DCW) + 1.2(WENT)
LOAD 205	=	1.2(SW + DCW) + 1.2(WAS)
LOAD 206	=	1.2(SW + DCW) + 1.2(WDP_P)
LOAD 207	=	1.0(SW + DCW) + 1.4(WDP_U)
LOAD 208	=	1.2(SW + DCW) + 1.2(WSB_P)
LOAD 209	=	1.0(SW + DCW) + 1.4(WSB_U)

The design of the member sizes are based on the above load combination.

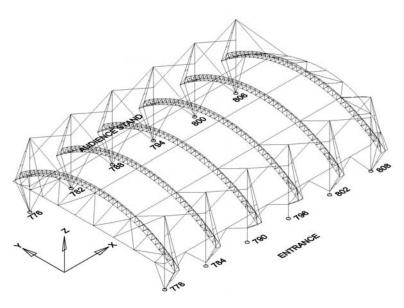
### 7.4. BOUNDARY CONDITION

The steel structure is supported on top of 12 nos of RC stump at spacing of 16.5m x 54m to each other. The mast base supports are assumed to be fixed condition which restrained in X, Y direction horizontally and Z direction vertically and also restrained in the X, Y and Z moment.

#### AUDIENCE STAND

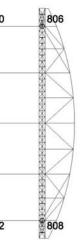


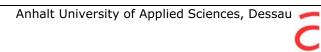
### SUPPORT NODE NUMBER LAYOUT PLAN



#### SUPPORT NODE NUMBER 3D VIEW







#### **7.5. DESIGN OF STEEL MEMBERS**

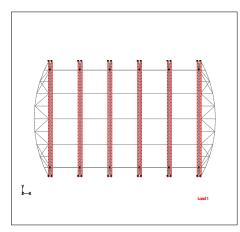
The design of the member size complied to BS5950 where the ultimate strength is used and the relevant load factor is applied to the imposed loading.

For deciding the correct pipe size for every member, compression will be the deciding factor and the compression capacity depends on the slenderness ratio (l/r) and the tension capacity only depends on the sectional area.

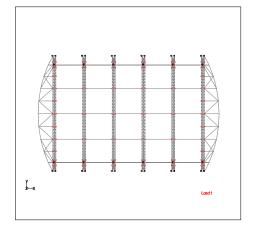
The final member size for individual member are determined from the worst force and moment from the ultimate load combination.

The software is able to check the sizes assigned based on the output from the worst load combination. The member sizes layout is attached for reference.

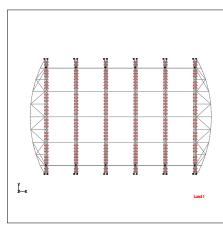
### 7.5.1 MEMBER SIZES LAYOUT



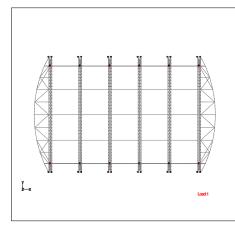
BOTTOM CURVED CHORD - 219Ø X 6



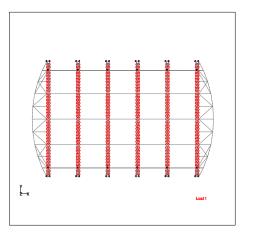
HORIZONTAL BOTTOM & DIAGONAL - 139Ø X 6



HORIZONTAL BOTTOM - 89Ø X 4



HORIZONTAL BOTTOM - 139Ø X 8



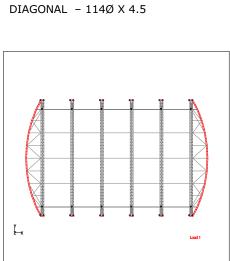


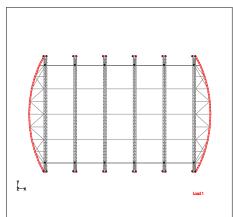
DIAGONAL - 89Ø X 4

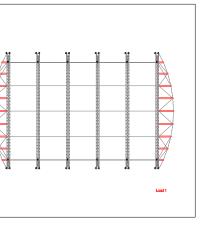
TOP CURVED CHORD - 219Ø X 6

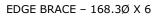
Ļ

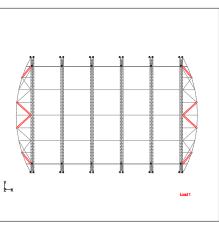
Ļ







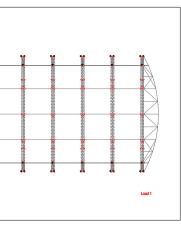






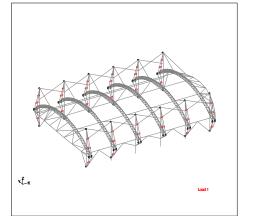






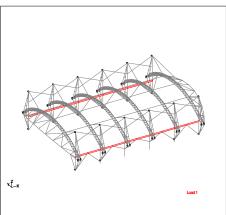
EDGE CHORD - 273Ø X 9.5

EDGE DIAGONAL BRACE - 168.3Ø X 10

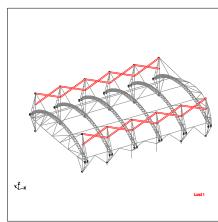




ĸŁх

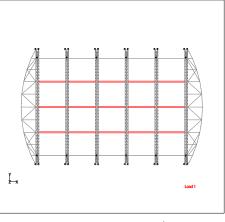




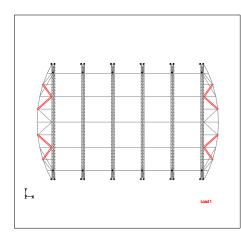


ĸЪ

SAFETY CABLE BETWEEN MAST - 16Ø

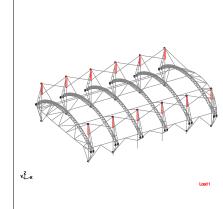


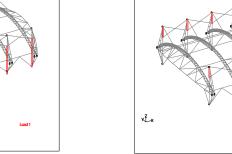
TIE BTW 3D TRUSS - 273Ø X 8



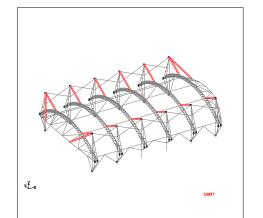
EDGE DIAGONAL BRACE - 168.3Ø X 8

ĸŁ.



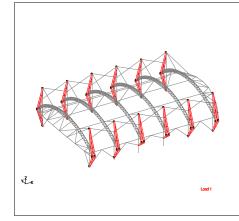


INTERMEDIATE MAST – 406.4Ø X 12.5

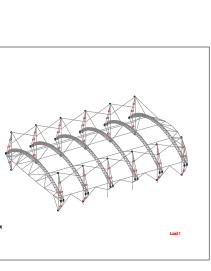


LOWER MAST – 609Ø X 16

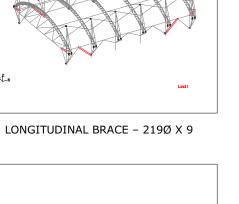
MAST FRONT STAY – 219Ø X 9



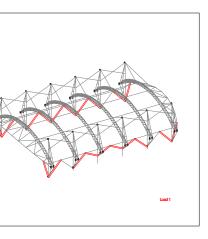
MAST BACKSTAY - 168Ø X 6



TIE BETWEEN MAST BACKSTAY – 73Ø X 5







LONGITUDINAL BRACE – 219Ø X 6

LONGITUDINAL TIE – 273Ø X 9

#### LOCAL DESIGN CHECK 7.6

#### 7.6.1 STABILIZING CABLE AT TOP OF MAST

From the steel structure analysis output,

maximum axial force = 30 KN

Proposed to use 16mm Ø 1x19 galvanized steel wire rope

Min breaking load = 211 KN >>30 KN

Therefore is ok to use 16mm Ø wire rope.

#### 7.6.2. HOLDING DOWN BOLTS

Reaction summary extracted from analysis output as shown,

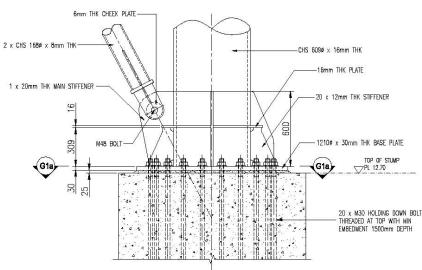
			H	orizontal	Vertical	Moment		
	Node	L/C	FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Max FX	800	208:1.2(SW+DCW)+1.2(WSB_P)	232.063	97.654	-23.855	-106.987	62.379	-22.129
Min FX	782	206:1.2(SW+DCW)+1.2(WDP_P)	-232.586	97.637	-23.505	-106.971	-60.596	20.386
Max FY	790	201:1.4(SW+DCW)+1.6(CDW+VL)	-13.887	228.469	507.055	-773.536	-39.192	3.081
Min FY	788	201:1.4(SW+DCW)+1.6(CDW+VL)	-26.716	-228.757	566.764	246.624	-4.373	-1.534
Max FZ	788	201:1.4(SW+DCW)+1.6(CDW+VL)	-26.716	-228.757	566.764	246.624	-4.373	-1.534
Min FZ	776	202:(SW+DCW)+1.4WU	-60.139	160.995	-333.775	-95.690	9.324	62.486
Max MX	788	204:1.2(SW+DCW)+1.2WEN	-42.971	-124.248	88.426	529.380	-7.790	-0.007
Min MX	790	201:1.4(SW+DCW)+1.6(CDW+VL)	-13.887	228.469	507.055	-773.536	-39.192	3.081
Max MY	802	208:1.2(SW+DCW)+1.2(WSB_P)	228.307	-97.765	13.935	171.829	278.833	22.013
Min MY	784	206:1.2(SW+DCW)+1.2(WDP_P)	-228.844	-97.713	14.756	171.682	-278.306	-19.787
Max MZ	808	208:1.2(SW+DCW)+1.2(WSB_P)	63.227	34.256	-60.780	-87.560	-27.936	124.287
Min MZ	806	208:1.2(SW+DCW)+1.2(WSB_P)	63.709	-34.308	-65.863	89.498	-29.237	-124.972

From the reaction forces summary output, max reaction forces are;

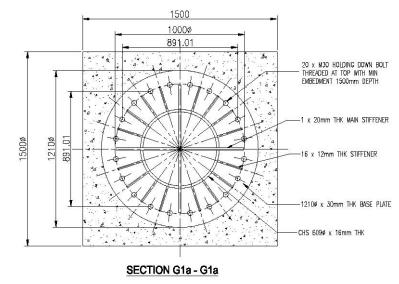
Fx = 233 / -233 KN	Mx = 530 / -774 KNm
Fy = 229 / -229 KN	My = 279 / -279 KNm
Fz = 567 / -334 KN	Mz = 125 / -125 KNm

Note : +ve Fz is the compression and -ve Fz is the tensile force

## Proposed 20 x M30 grade 8.8 in a circular arrangement at 1m diameter, and assumed only 4 bolts on each side at 0.89m apart are resisting;







Ft due to Mx per bolt = 774 / (4x0.89) = 217.4 KNDirect Ft per bolt = 334/20 = 16.7 KN Total tensile per bolt Ft = 217.4 + 16.7 = 234.1 KN

Fs due to Mz per bolt = 125 / (4x0.89) = 35.1 KNDirect Fs per bolt =  $(233^2 + 229^2)^{\frac{1}{2}}$  /20 = 16.3 KN Total Fs per bolt = 35.1 + 16.3 = 51.4 KN

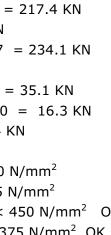
Tensile strength of Grade 8.8 bolt =  $450 \text{ N/mm}^2$ Shear strength of Grade 8.8 bolt =  $375 \text{ N/mm}^2$ ft =  $234.1xe3 / 561 = 417 N/mm^2 < 450 N/mm^2$  OK  $fs = 51.4xe3 / 561 = 92 N/mm^2 < 375 N/mm^2 OK$ 

Combined stress check, 417/450 + 92/375 = 1.172 < 1.4 OK

TAN SIEW MOI







fbu =  $\beta$  (fcu)<sup>1/2</sup> Where fbu = design ultimate anchorage bond stress  $\beta$  = 0.28 for plain bar fcu =  $35 \text{ N/mm}^2$  for concrete grade fbu =  $0.28 (35)^{\frac{1}{2}} = 1.656$ anchorage force /  $(\Pi \times \emptyset \times L) = fbu$ embedment length L = anchorage force / ( $\Pi \times \emptyset \times fbu$ )  $= 234.1 \times 163 / (\Pi \times 30 \times 1.656)$ = 1500 mm

Therefore provide minimum 1500mm embedment length is OK.

## **7.6.2.2** Base plate thickness check

Assumed the plate is bend in double curvature over the width of 590mm for 4 bolts and ignored the 16mm and 20mm thk stiffener plate,

$$M = 234.1 \times (1.0 - 0.609)/2 \times \frac{1}{2} = 22.88 \text{ KNm}$$

 $Z_{\text{provide}} = 1/6 \times 590 \times 30^2 = 88500 \text{ mm}^3$ 

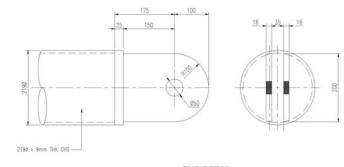
 $fb = 22.88 \times 1e6 / 88500 = 258 \text{ N/mm}^2 < 275 \text{ N/mm}^2 \text{ OK}$ 

Therefore use 30mm thk base plate with stiffener plate is OK.

## 7.6.3 DESIGN OF PIN CONNECTIONS

## 7.6.3.1 MAST FRONT HANGER

Max axial force as extracted from analysis output = 217 KN



END DETAIL

Proposed to use 1 x M48 grade 8.8 bolt with 16mm thick tongue plate,

Tensile strength of Grade 8.8 bolt =  $450 \text{ N/mm}^2$ Shear strength of Grade 8.8 bolt =  $375 \text{ N/mm}^2$ 

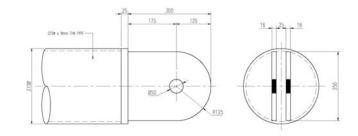
 $fs = [(217/2x1e3)]/1470 = 74 N/mm^2 < 375 N/mm^2 OK$ 

bearing stress of tongue plate, fbs = [(217/2)x1e3] / (48x16) $= 141 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK}$ 

Where 460  $N/mm^2$  is the bearing strength for S275 plate.

### 7.6.3.2 TIE BETWEEN 3D TRUSS

Max axial force as extracted from analysis output = 323 KN

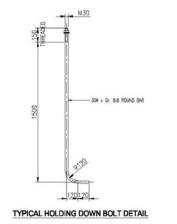


#### END PLATE FOR 273Ø PIPE

Proposed to use 1 x M48 grade 8.8 bolt with 16mm thick tongue plate,

Tensile strength of Grade 8.8 bolt =  $450 \text{ N/mm}^2$ Shear strength of Grade 8.8 bolt =  $375 \text{ N/mm}^2$ 





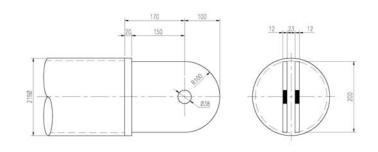
Anhalt University of Applied Sciences, Dessau 🦟

bearing stress of tongue plate, fbs = [(323/2)x1e3] / (48x16) $= 210 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK}$ 

Where 460  $N/mm^2$  is the bearing strength for S275 plate.

### 7.6.3.3 BRACE AT LOWER MAST

Max axial force as extracted from analysis output = 365 KN



END DETAIL

Proposed to use 1 x M36 grade 8.8 bolt with 12mm thick tongue plate,

Tensile strength of Grade 8.8 bolt =  $450 \text{ N/mm}^2$ Shear strength of Grade 8.8 bolt =  $375 \text{ N/mm}^2$ 

fs =  $[(365/2)x1e3] / 817 = 224 \text{ N/mm}^2 < 375 \text{ N/mm}^2 \text{ OK}$ 

bearing stress of tongue plate, fbs = [(365/2)x1e3] / (36x12) $= 422 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK}$ 

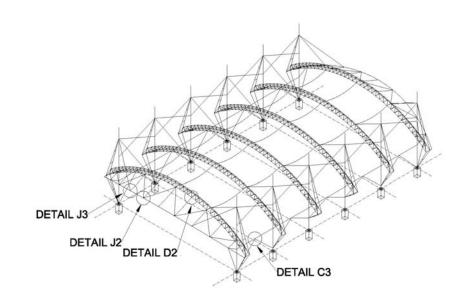
Where 460  $N/mm^2$  is the bearing strength for S275 plate.

### 7.6.4 PLATE CONNECTION TO CHS

For the tensile structure, there is a lot of connection with plate welded to circular hollow section for fixing of fabric, for bolting of bracing member and etc. To check the influences of forces to these plate and main member is quite complex, so a finite element model (FEM) is done for some typical connection to verify the von mises stresses or equivalent stress is not to exceed the yield stress of main member and plates.

The von mises stress shall not exceed 90% of the material yield stress. Therefore the connection stresses shall not exceed  $0.9x275 \text{ N/mm}^2 = 247.5 \text{ N/mm}^2$ 

Extract 4 finite element model done at four connections as shown and attached for information. And max von mises stress is 237 N/mm<sup>2</sup> at Detail J2.

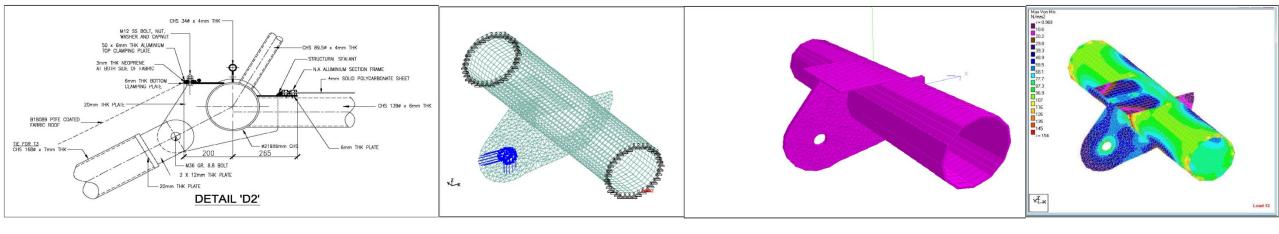


**KEY PLAN FOR CONNECTION DESIGN** 



Anhalt University of Applied Sciences, Dessau 🦟

#### 7.6.4.1 JOINT AT 3D TRUSS BOTTOM CHORD TO EDGE FRAME BRACE MEMBER

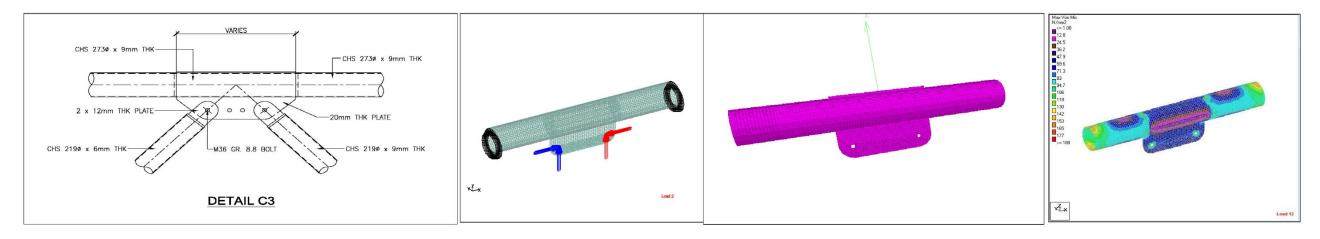


INFORMATION ON THE JOINT

FEM WITH FORCE @ BOLT HOLE

3D RENDERED

#### 7.6.4.2 JOINT AT LOWER MAST HORIZONTAL TIE & BRACE MEMBER



#### INFORMATION ON THE JOINT

FEM WITH FORCES @ BOLT HOLES

3D RENDERED

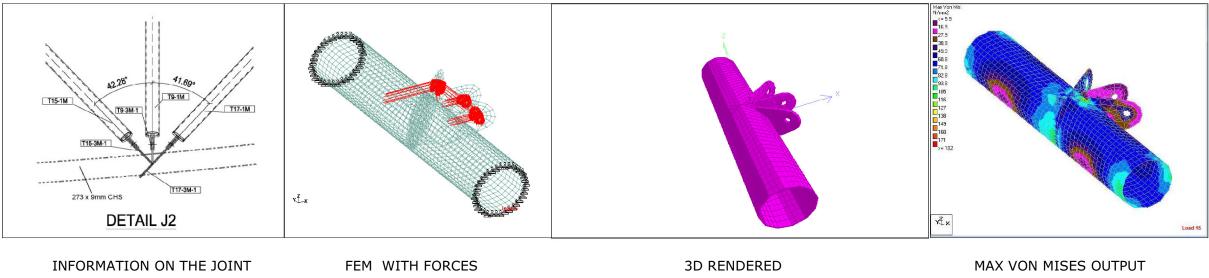




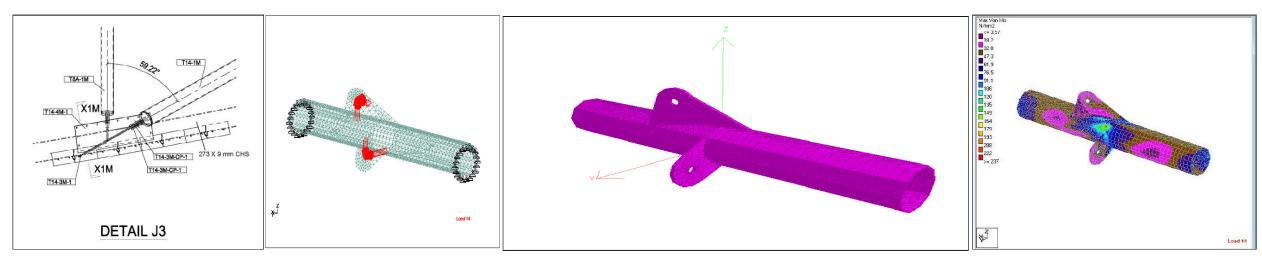
MAX VON MISES OUTPUT

MAX VON MISES OUTPUT

#### 7.6.4.3 JOINT AT EDGE FRAME WITH 3 BRACE MEMBER



#### 7.6.4.4 JOINT AT FRONT HANGAR TO EDGE FRAME WITH BRACE MEMBER



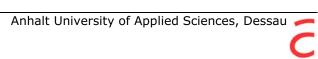
INFORMATION ON THE JOINT

FEM WITH FORCES

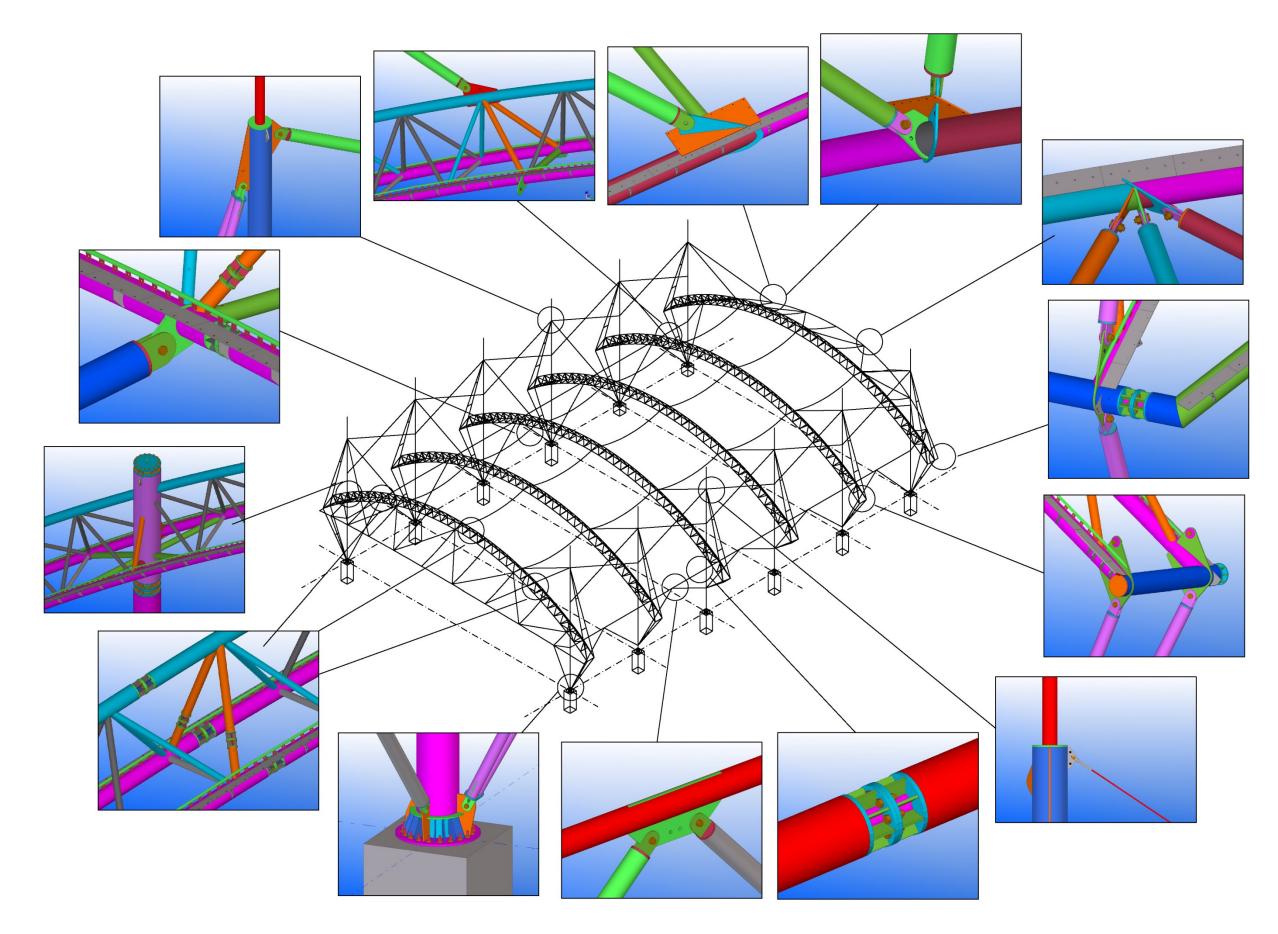
3D RENDERED

MAX VON MISES OUTPUT





# 7.7 SUMMARY OF CONNECTION DETAILS



TAN SIEW MOI



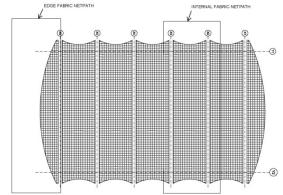
#### 8. MEMBRANE ANALYSIS AND DESIGN

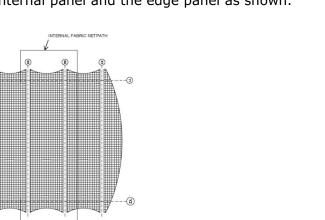
#### **8.1 GENERAL INFORMATION**

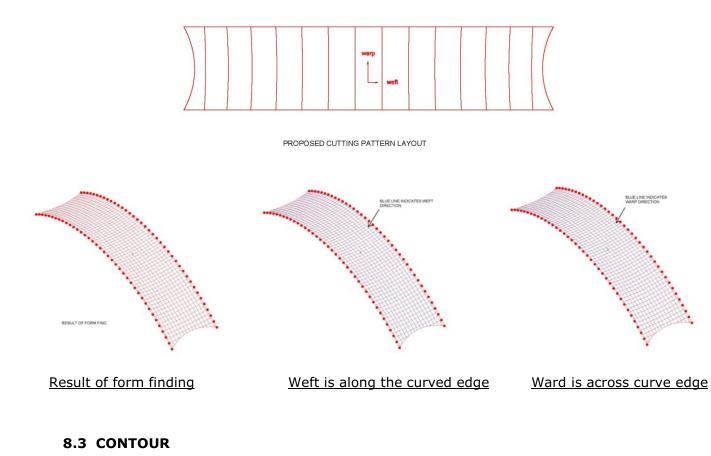
The fabric material is represented by a network of mesh formed by membrane link represented by segment of lines. For membrane design, firstly is to do a form finding to study the feasibility of the proposed shape with assumed material type and sizes. Secondly is to study the proposal when various loading is applied onto the stable form and check for the displacement and stresses in the membrane for all possible load combination and not forgetting to make sure the proposed form will not have any water pounding possibility. And lastly is to do a cutting pattern based on the available width of proposed fabric used with compensation value adopted from the result of the biaxial test and also typical production practice ie seam width and pocket allowance. And then finally the individual pattern can then be used for production.

#### 8.2 FORM FINDING

8.2.1) To identify the different netpath for the project and for the shape of this structure, there is only 2 type of netpath ie the internal panel and the edge panel as shown.



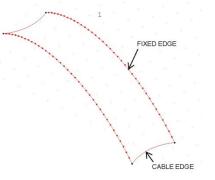


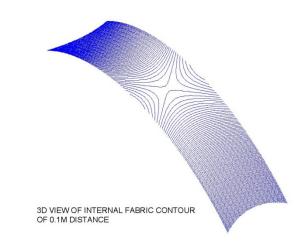


A contour line of 0.1m is plotted and it show there will not be any water stagnate problem due to the shape of the structure.

8.2.2) Prepare the boundary in cad program and then import into EASY and assign sag ratio to the cable edge and radius or sag ratio for the curved beam. Check the fixity of the boundary points for form find and also for static analysis.

In this case, the sag ratio used is 12.5% for the border cable edge and 18% or 50m radius for the curved fixing edge.





decide based on the intended cutting pattern configuration as these will affect the static analysis result later.

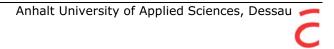




8.2.3) Then form find based on the assigned value. The warp and weft direction have to be



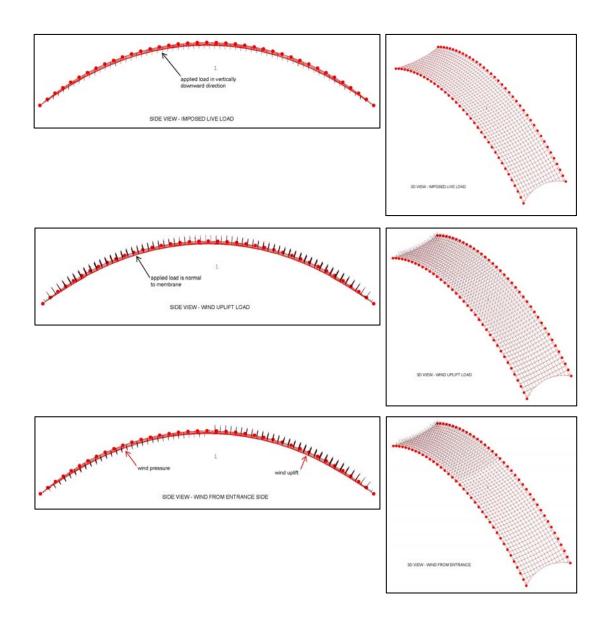
PLAN VIEW OF INTERNAL FABRIC CONTOUR OF 0.1M DISTANCE



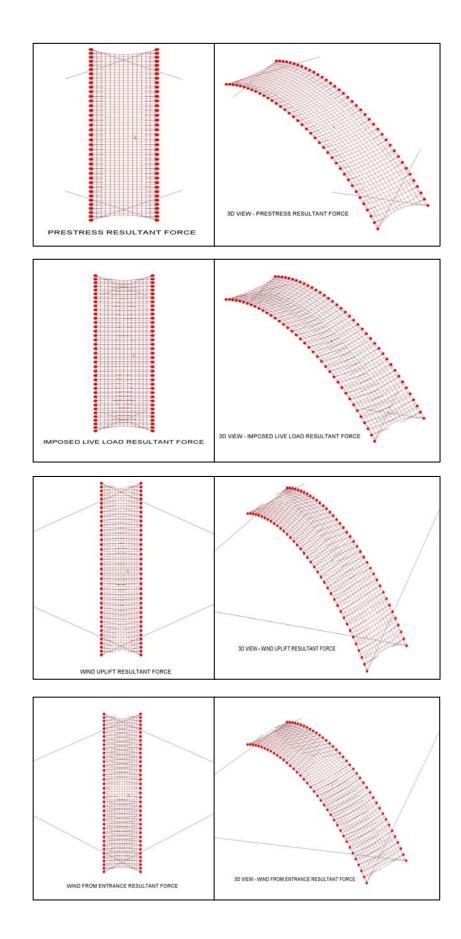
#### 8.4 LOADING AND STATICAL ANALYSIS

8.4.1) Assumed a prestress force for the final form and load the form with the calculated various loading ie. wind load or live load by creating load case. A prestress force of 3 KN/m for warp and weft is adopted for this project.

The surface load is applied as nodal load to the nodes in the mesh. And all wind load are applied normal to the membrane surface, except the imposed live load which is vertically to the surface of the membrane. Extract some applied load diagram for reference.



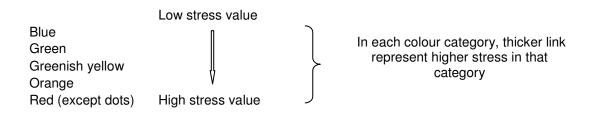
8.4.2) Then view the analysis results ie reactions at the fixing point. These are the forces that are then extract and apply to the steel structure.



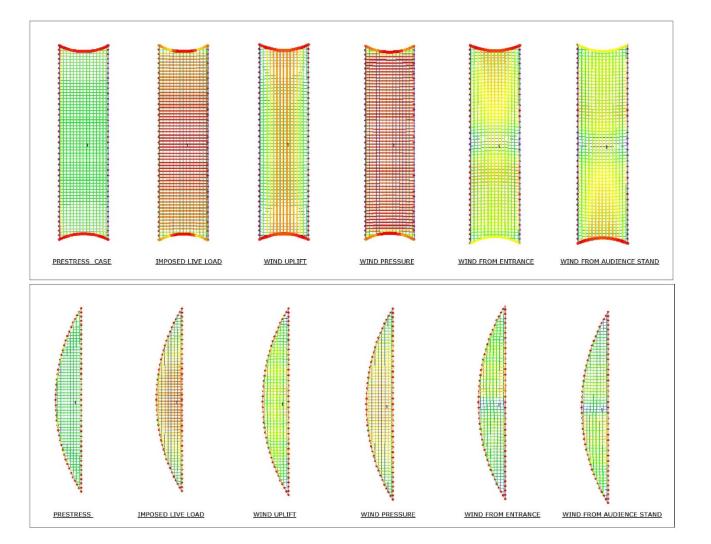
TAN SIEW MOI



8.4.3) To perform statical structural analysis, correct stiffness value have to assumed for the membrane link. In this case, 2000 and 1000 is assumed for warp and weft membrane links and 5000 assumed for cable link. Upon completion of the analysis of a typical load cases, there will be a stressed pattern shown in these membrane link. The magnitude of stresses is expressed in colour as well as width of membrane link in the following order,



Red dots seen in any stress pattern represent fixed point of fabric for design analysis. For each load case, there will be a overall stress pattern shown where the highest stressed area can be located. The following membrane stress value are not shown for clarity.



#### 8.5 LOCAL DESIGN CHECK

#### 8.5.1 MEMBRANE

Summary of Membrane Stress and Border Cable Force

	Membrane	e Link Stress	Cable Link Force
	KN/m	KN/m	KN
Load Case	Critical Low	Critical High	Critical High
Internal Fabric			
Prestress	2.224	5.056	42
Imposed Live	1.005	9.045	18
Wind Uplift	3.056	24.144	231
Wind Pressure	0.896	10.464	32
Wind from Entrance	1.923	17.307	165
Wind from Grandstand	1.953	17.577	168
Edge Fabric			
Prestress	2.442	5.098	-
Imposed Live	1.67	8.47	
Wind Uplift	4.176	15.424	-
Wind Pressure	1.433	11.137	-
Wind from Entrance	3.132	15.948	-
Wind from Grandstand	3.214	15.886	-

From the tabulated summary, the max membrane stress is 24 KN/m from wind uplift case. From the technical data of B18089 from Verseidag, , Tensile strength (N/5cm) warp/ weft = 7000 / 6000And the max stress is along the weft direction, = 120 KN/m

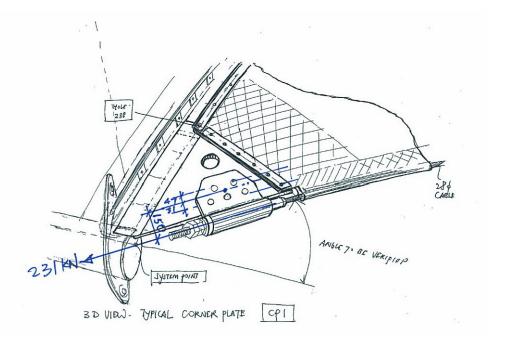
Safety factor = 120 / 24 = 5.0

Therefore the chosen membrane is ok to use for this span.

### 8.5.2 BORDER CABLE

From the tabulated summary, the max cable force is 231KN from wind uplift case. Proposed to use 28mm Ø 6 x 37 IWRC galvanized steel ire rope, Min breaking load = 49600 kg = 506 KN Safety factor = 506 / 231 = 2.2 Therefore is ok to use 28mm Ø wire rope.





The 28mm diameter border cable is fix on to a double layer 16mm thk 'burger' welded to 89  $\emptyset \times 11.3$ mm thk x 300mm long pipe section.

Max border cable force = 231 KN (unfactored load) Assumed load factor of 1.4 due to wind uplift,  $F = 231 \times 1.4 = 323.4 \text{ KN}$ 

Center of group of 5 x M36 G8.8 bolts to center of cable fitting = 155mm Moment due to cable force, M =  $323.4 \times 0.155 = 50$  KNm

This moment is to resist by the 5 bolts about the center of bolts in shear force Fs,

Therefore 2 Fs x 0.047 = 50 KNm Fs due to moment = 50/(2x0.047) = 532 KN

Or 3 Fs x 0.031 = 50 KNm Fs due to moment = 50/(3x0.031) = 538 KN

Direct shear force per bolt = 323.4/5 = 64.7 KN Therefore maximum shear force per bolt = 538 + 64.7 = 602.7 KN

Proposed to use 5 x M36 grade 8.8 bolt with 16mm thick double plate,

Tensile strength of Grade 8.8 bolt =  $450 \text{ N/mm}^2$ Shear strength of Grade 8.8 bolt =  $375 \text{ N/mm}^2$ 

 $fs = [(602.7/2x1e3)]/817 = 369 N/mm^2 < 375 N/mm^2 OK$ 

bearing stress of the double 'burger' plate, fbs = [(602.7/2)x1e3] / (36x16)= 523 N/mm<sup>2</sup> < 550 N/mm<sup>2</sup> OK

Where 550 N/mm<sup>2</sup> is the bearing strength for S355 plate.

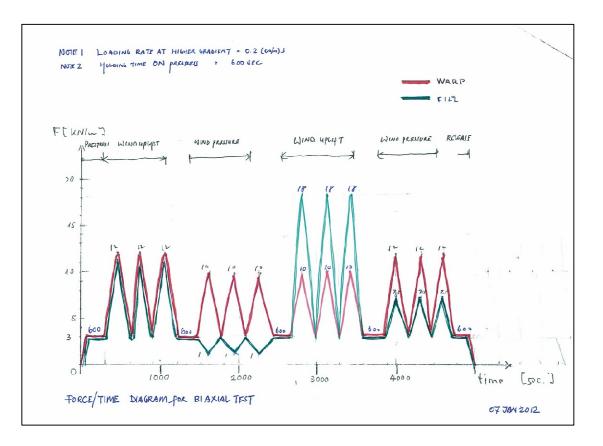
### 8.6 BIAXIAL TEST

From the membrane stress pattern, a suitable value is decided for carry out the biaxial test. In this case, a value of about 70% of the maximum stress is used for various load case is tabulated as follow. And the test is carried out by University of Essen, Germany.

These values are extracted from the membrane analysis based on wind speed of 38 m/s which is later revised to 32 m/s in the final design.

S/N	LOAD CASE	WARP DIRECTION	WEFT DIRECTION
-/		(KN/m)	(KN/m)
1	PRESTRESS	3.0	3.0
2	VERTICAL LIVE LOAD	7.5	1.4
3	WIND PRESSURE	10.0	1.0
4	WIND UPLIFT	10.0	18.0
5	WIND UPRESSURE + UPLIFT		
	PRESSURE SIDE	12.0	7.5
	UPLIFTSIDE	12.0	12.0

The following sketch is the force-time diagram proposed to University of Essen for the load ratio and sequences and the numbers of loads.

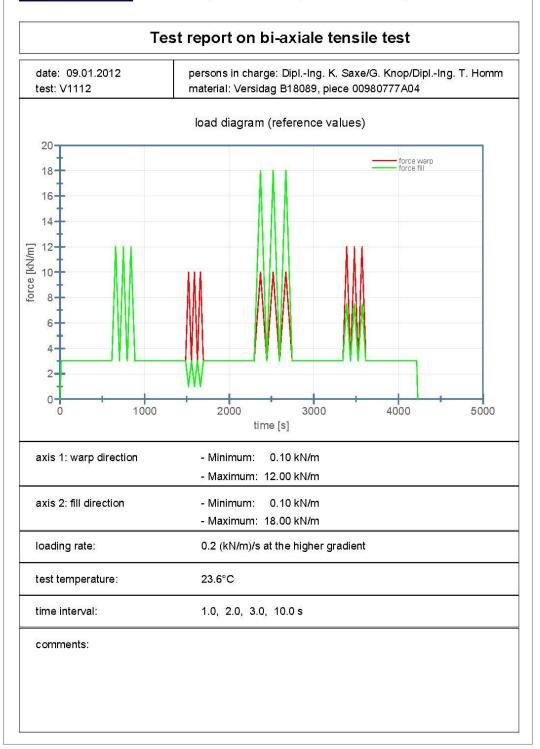


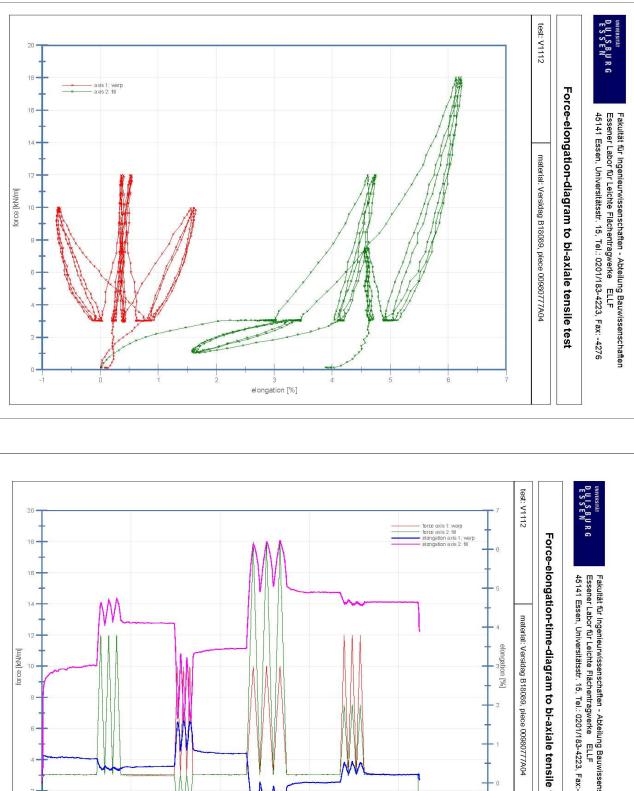


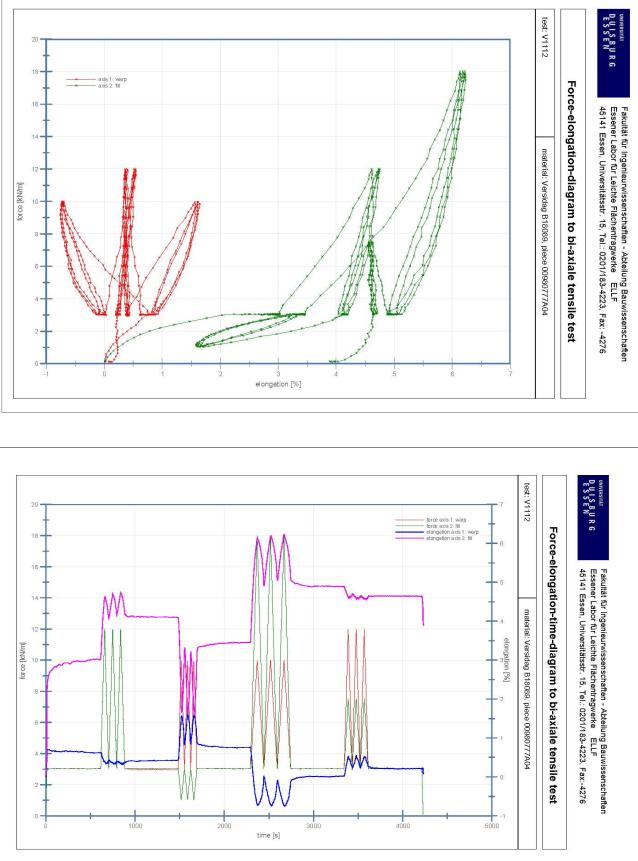
In this particular project, there are FOUR batch of material from Verseidag, so FOUR biaxial test is done. Extract here some pages from one of the test for information.



Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276





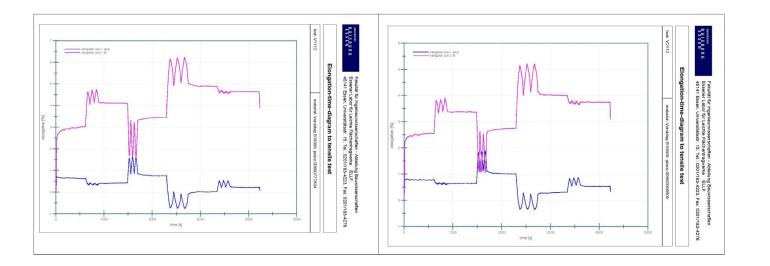


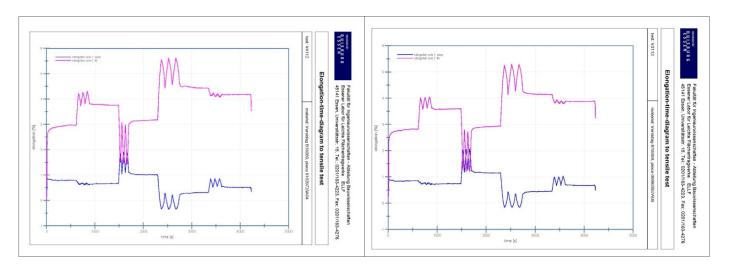


Anhalt University of Applied Sciences, Dessau 🛹

39

#### The elongation result of the 4 batch of material is summarized as follow;





As the result was based on higher wind speed as opposed to the design wind speed of 32m/s, when deciding a suitable value for compensation for cutting pattern, some reduction is considered from the tested result.

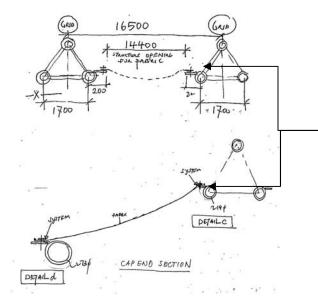
Based on past experience with Verseidag's PTFE material and the above result, we have used compensation value of 2.8% for the weft and 0.6% for the warp. Whereas the fixed side which is along the weft direction 1.2% is used instead of 2.8% as shrinkage is expected at welded seam for the keder pocket.

#### 8.7 CUTTING PATTERN

#### 8.7.1 FABRIC SYSTEM POINT

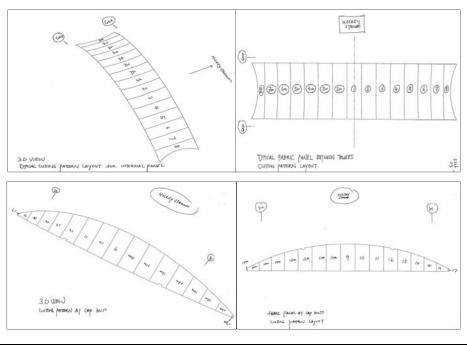
After the compensation value is established, some typical details ie. seam width, clamping detail, border cable pocket size are then finalized to prepared the cutting pattern. Also the roll width of the membrane is also known to decide how many strips of cutting pattern.

For fabric patterning, the system is different from the steel structure system, example the distance between 2 steel arch center is 16.5m, but fabric system is smaller than that and is 14.4m instead.

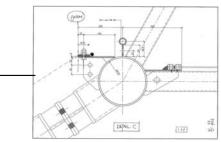


The width of B18089 is 4.7m, so maximum width of the patterning at system is 4.6m after deducting the overlapped seam of 80mm and trimming of 10mm on each side of the width of membrane.

So total nos of strip for internal panel is about 68m/4.6 = 15 and end panel 17 strip, and they are symmetrical about the centerline, so only 17 cutting pattern need to be done.



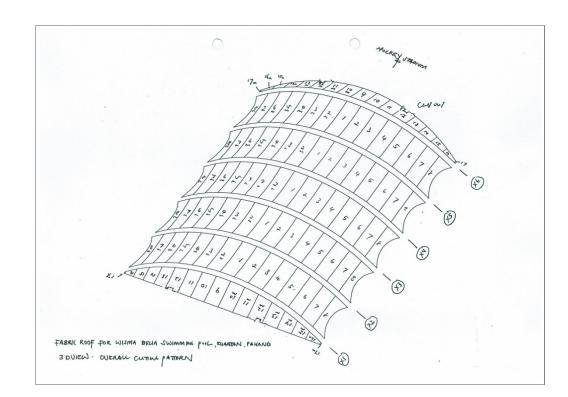


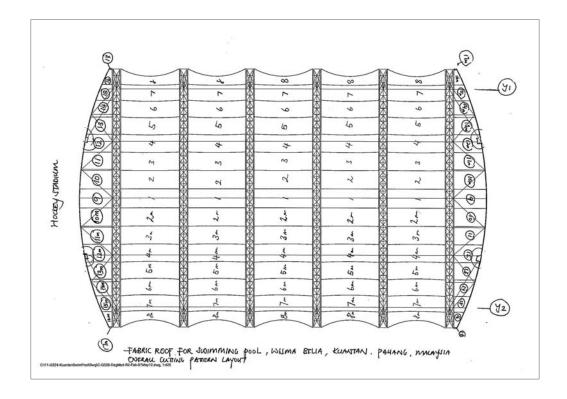


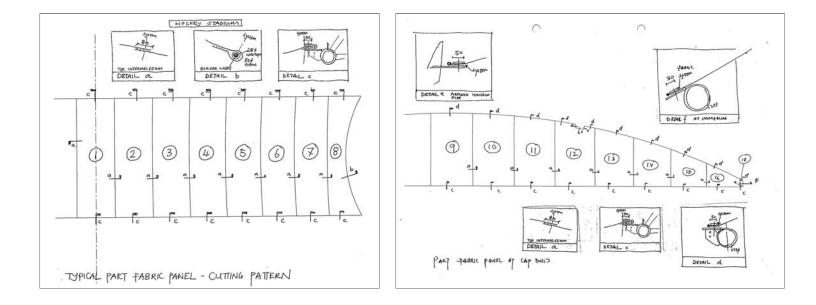
Anhalt University of Applied Sciences, Dessau 🦟

### 8.7.2 COMPENSATED CUTTING PATTERN

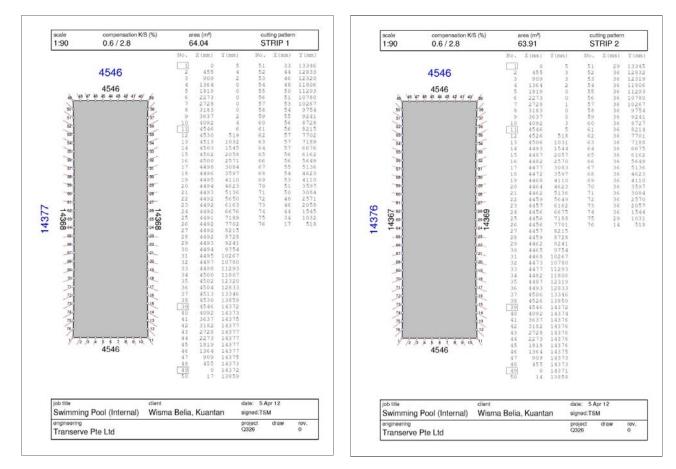
Therefore the overall cutting pattern for the swimming pool membrane roof are as follow;



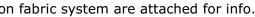


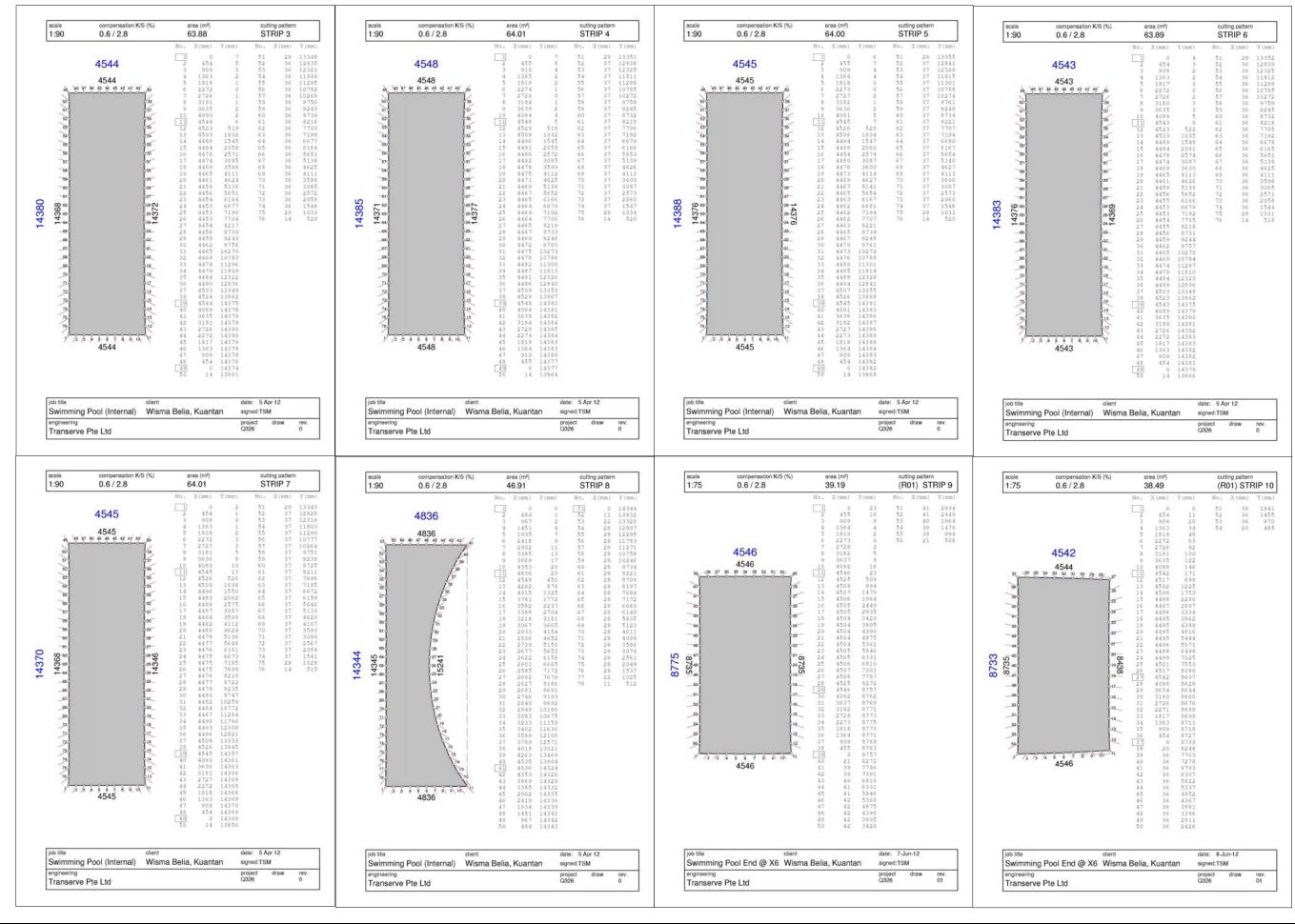


### The compensated cutting pattern Strip 1 to 17 based on fabric system are attached for info.









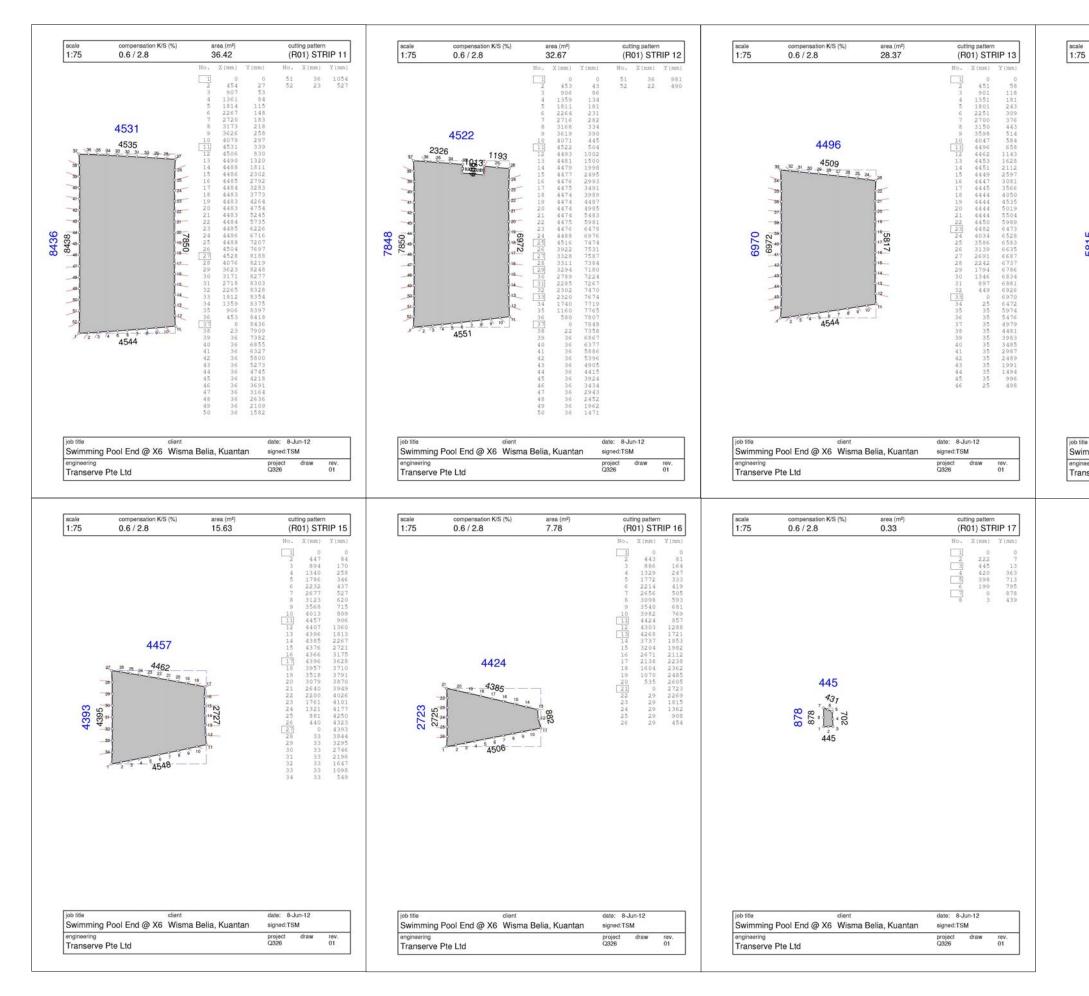
TAN SIEW MOI

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

Institute for Membrane and Shell Technologies



Anhalt University of Applied Sciences, Dessau 🛹

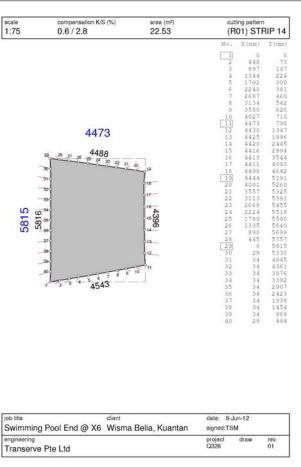


TAN SIEW MOI

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

Institute for Membrane and Shell Technologies



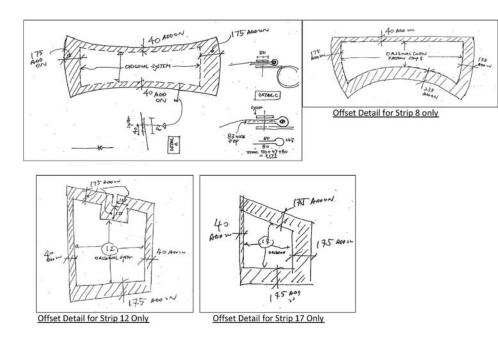


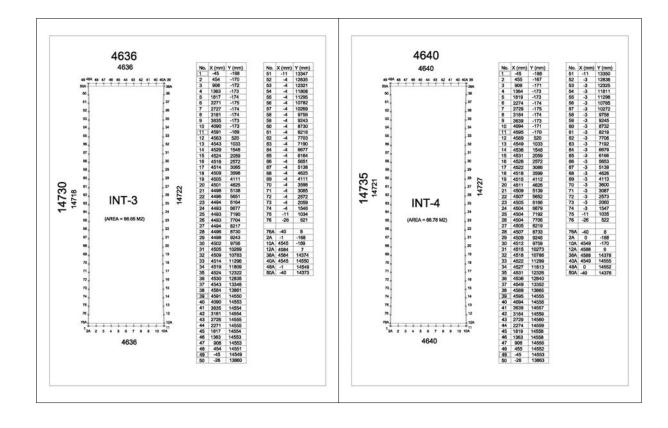
# 43

Anhalt University of Applied Sciences, Dessau

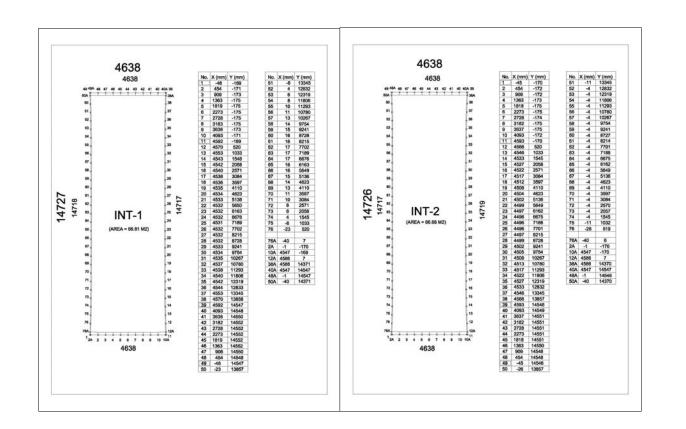
#### 8.7.3 OFFSET CUTTING PATTERN

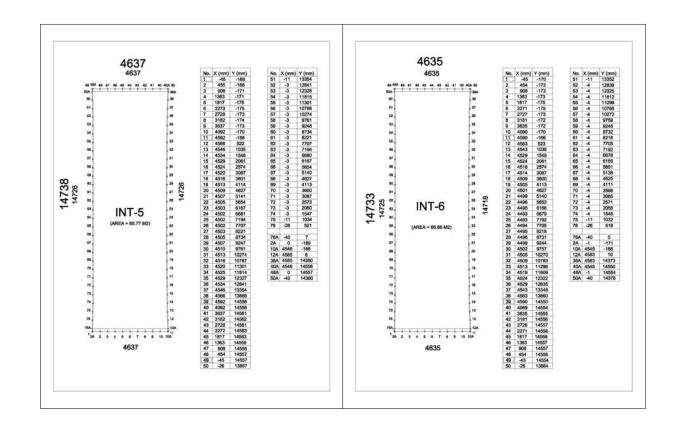
The cutting pattern based on fabric system are to be further process before actual cutting can be carried out. The tabulation of how much offset is is shown in the sketch below. The offsetting process is then done in autoucad.





After that a different set of cutting pattern data is then passed to factory for actual fabrication.

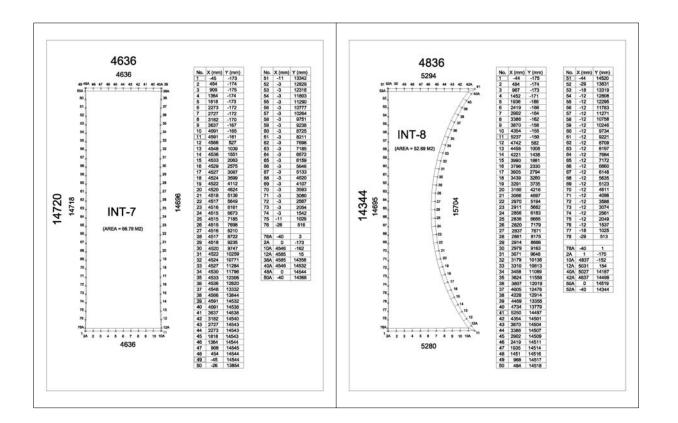


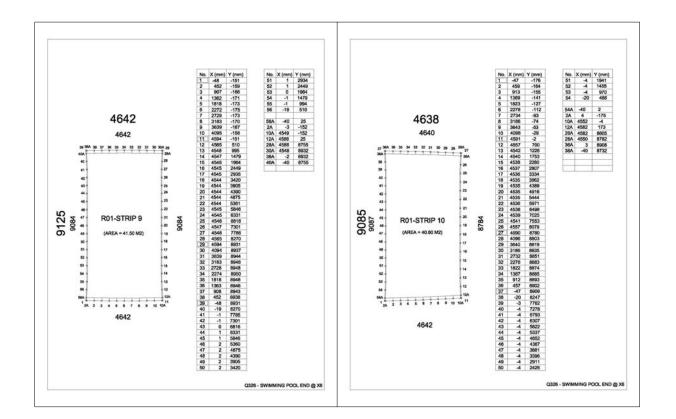


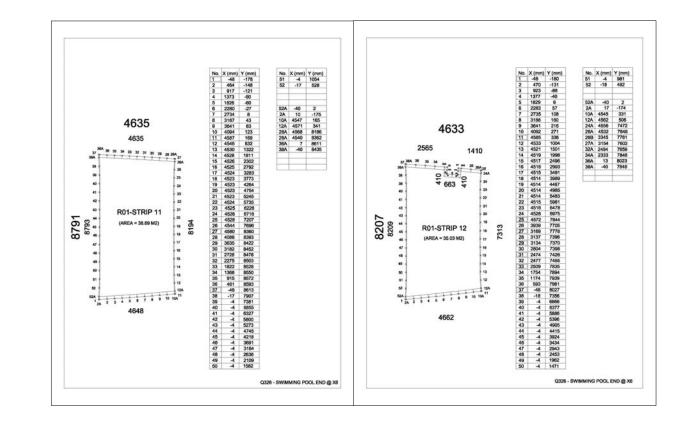
TAN SIEW MOI

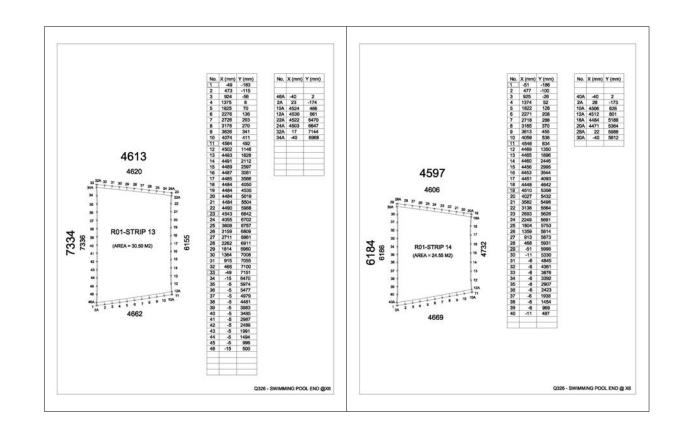


Anhalt University of Applied Sciences, Dessau



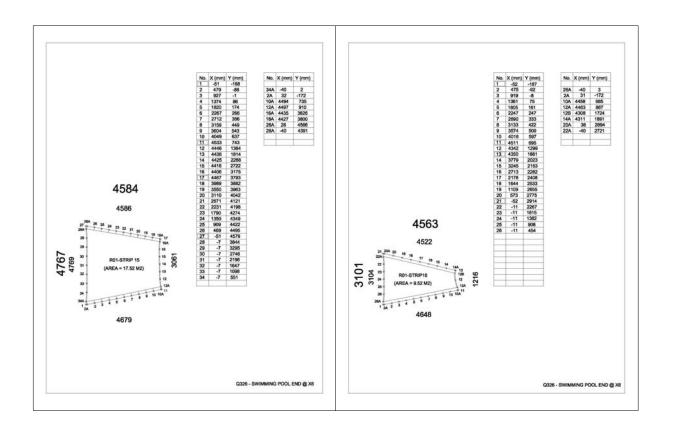


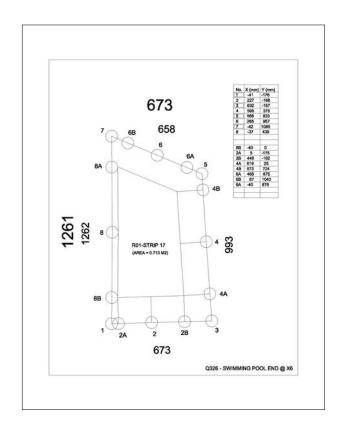






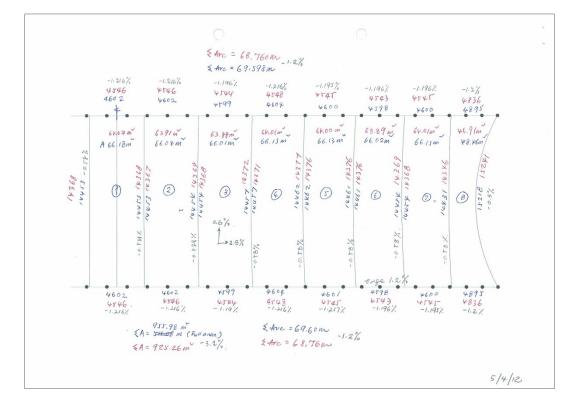
Anhalt University of Applied Sciences, Dessau



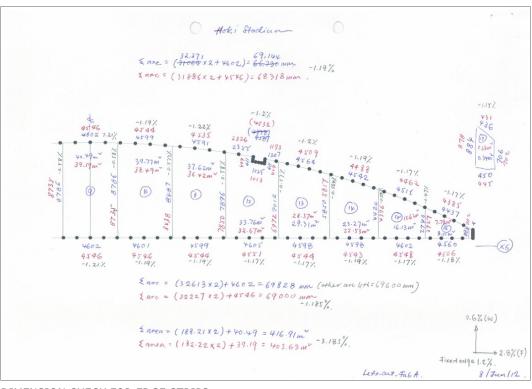


#### **8.7.4 DIMENSION CHECK**

As the cutting pattern is to be use 5 times for internal panel and 2 times for the end panel, extra measure is taken to make sure the compensated strips are done correctly, so dimension check of uncompensated length and area against the compensated length is done as shown.



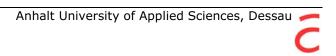
DIMENSION CHECK FOR INTERNAL STRIPS

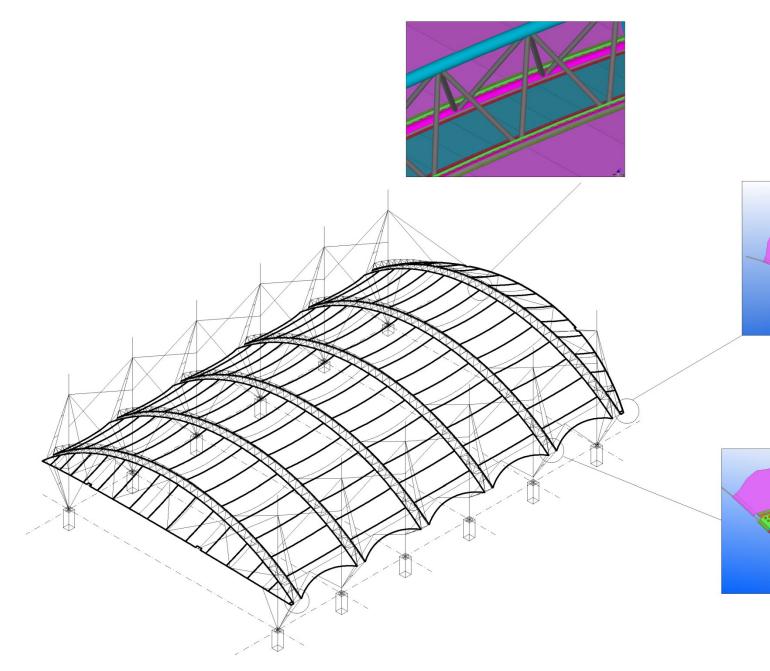


DIMENSION CHECK FOR EDGE STRIPS

TAN SIEW MOI

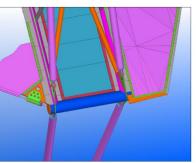


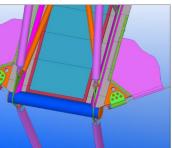


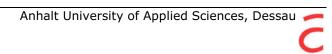












#### 9. STEEL ERECTION

#### 9.1 LIFTING CHECK

After site visit, noted that site access for crane only possible on the pavement beside the pool and also the access road leading to existing hostel beside the swimming pool. And the width of pool side pavement is 6.5m width of 250mm thick concrete slab, and so bigger tonnage crane are not possible to be used at site. And so not possible to erection the trusses in one single lift.



CRANE ACCESS BESIDE EXISTING HOSTEL BLOCK AT REAR OF SITE



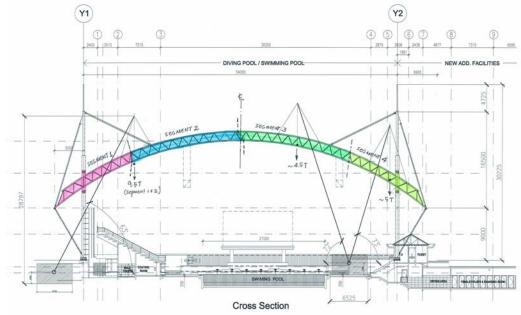
CRANE ACCESS BESIDE POOL

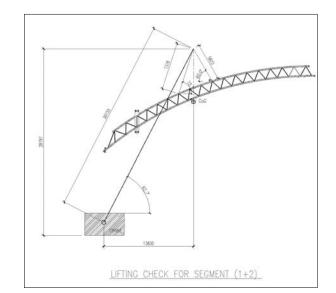
Due to these site access constrain, and preferably no welding work on site, proposed to use 35 ton hydraulic mobile crane. As such the 3D curved truss of approximately 68m span have to be fabricated in 4 segment to enable lifting by 35 tons crane and flange jointed to ensure the structural integrity and continuity of the trusses.

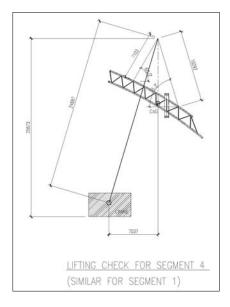
The truss is then subdivided further to 4t to 5t each so that they are possible to be lifted by the crane. And it is preferred that they are exactly oriented in final position when lifted and placed in position, so the center of gravity of these segment truss and correct length of lifting sling is important to the erector.

The Cog of these segmented truss is calculated with StaadPro software.

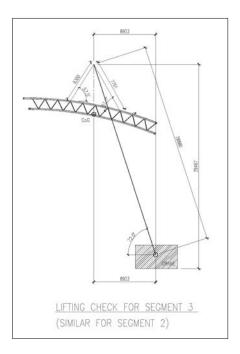
In the preliminary study of erection method, possibility of lifting truss segment 1 and segment 2 together from the rear access is also checked to minimize connection in the high air. But this option was not used at site later. It is attached for information.











48

#### 9.2 ERECTION SEQUENCE

The steel frame erection sequence is briefly describe below, a detail illustration of the erection process is refers to attachment in the appendix.

The erection will starts from gridline X1 near to Score Board and progressively to gridline X6.

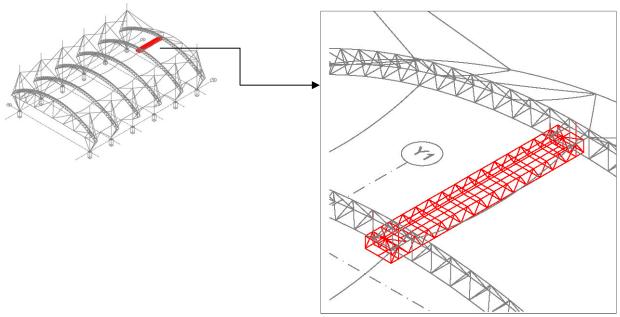
- 1) Firstly lift the lower column with base stump into correct position.
- 2) Then tie up at least 2 lower mast with the horizontal brace and cross bracing.
- 3) Then put in position Segment 1 truss on top and bolt up the flange joint.
- 4) With Segment 1 truss, the lower backstay can be fix up.
- 5) The step 1 to 4 can be repeated to the other side as well.
- 6) Then the upper mast with backstay and front hanger is connected placed on top
- 7) Then using 2 crane to lift the Segment 2 truss and also bolt the front hanger to stabilized the partly erected frame.
- 8) And a truss is completed when the opposite side Segment truss 3 is lifted and connected.
- 9) The same process will repeat for the second truss.
- 10) When the two truss are done, the 3 nos of curve tie beam can then be bolted on.
- 11) Same process repeat for the remaining truss until gridline X6.
- 12) Then the 2 end cap frame is erect with all its brace member until complete.
- 13) The 2 end front hanger is then bolted on.
- 14) Now the main structure is completed, the cross cable at the upper mast can then be install.
- 15) The catwalk hanging cage and walkway frame is then bolt on to the main roof structure.
- 16) So the roof is now ready to take on the fabric installation.

#### **10. MEMBRANE INSTALLATION**

#### **10.1 MEMBRANE HANDLING**

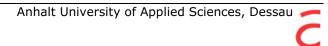
For lifting of fabric to the right level for installation, a temporary platform is proposed to be hung in-between 2 nos of 3D truss of 16.5m apart. This 3D platform is 18m in length, 2.4m width and 1.05m depth. It has to be lighted weight so not to impose too much load on to the steel structures. It is designed to be less than 2 tons and mainly welded from rectangular, square hollow section and angles.

4 nos of lifting padeye is provided at 4 corner, and 12mm thick plywood is fixed on top the platform. The platform will be placed slightly off center of the truss to avoid the center tie member , and it will be opened up at the center with the help of a crane with a spreader beam of as long as the width of the membrane 14m to one side and then to other side.



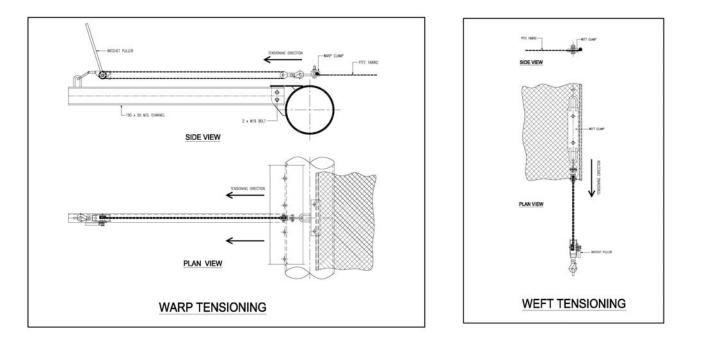


TEMPORARY PLATFORM



#### **10.2 MEMBRANE TENSIONING**

For installation of the membrane, some in-house tools are used. There are two type of tensioning tools used in this project; one for the warp and the other for the weft direction.





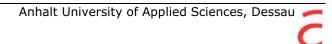
The membrane installation is starting from grid X1 outward to grid X6. The sequence is briefly description as follow;

- 1) Firstly lift the temporary platform to just underneath the 3D truss and then secured at four corner to the bottom chord of truss.
- 2) Then lift the fabric with a spreader beam and place it on to top of the platform.
- 3) After that, fix the nylon ropes at a constant distance of about 1.5m across the truss. And do all necessary preparation for securing fabric.
- 4) Then secure 2 corners of the fabric to the spreader beam and lift up slowly by crane.
- 5) As the fabric is slowly lifted up and move outward, the edge of the fabric is temporary secure with the warp tensioning tools.
- 6) So this process will continue until the fabric reaches the end of truss.
- 7) After all necessary temporary securing is done, the crane can release the fabric.
- 8) The same process will repeat for the other side of the fabric.
- 9) The remaining work is then time consuming and it will progress slowly to tension the warp and weft of the fabric.
- 10)The same sequence is repeated for internal panel 2 and until panel 5.
- 11)After all internal fabric is installed, then proceed for preparation work for edge fabric.
- 12)The erection process of the edge panel is similar to the internal fabric.
- 13)After all the fabric are installed, the tensioning and fixing of clamping edge work is still in progress until they are all fully tension and clamped.
- 14) A fully illustration of the sequence can refers to photo images in the Appendix.







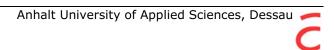






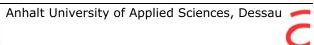
- **11. APPENDIX**
- **11.1 WORK PROGRAMME**
- **11.2 ENGINEERING DRAWINGS**
- **11.3 ERECTION SEQUENCE**
- **11.4 PHOTO IMAGES OF STEEL WORK**
- **11.5 PHOTO IMAGES OF FABRIC WORK**
- **11.6 PHOTO IMAGES OF COMPARISON BEFORE & AFTER ERECTION**
- **11.7 AERIAL VIEW PHASE 1 COMPLETION**
- **11.8 AERIAL VIEW PHASE 2 COMPLETION IMPRESSION**
- **11.9 NEWSPAPER ARTICLES BEFORE THE GAMES**
- **11.10 PHOTO IMAGES DURING THE GAMES**
- **11.11 BIAXIAL TEST REPORT**
- **11.12 DESIGN CALCULATION**





# **11.1 WORK PROGRAMME**





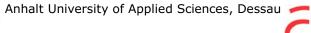
## PROJECT: PROPOSED TENSILE FABRIC ROOF SYSTEM AT KOMPLEKS KOLAM RENANG, WISMA BELIA INDERA MAHKOTA, KUANTAN, PAHANG DARUL MAKMUR, MALAYSIA

### PROPOSED WORK PROGRAMME

		1				20	11																2	012														
S/N	Schedule of Works	Date Start	Date Finish		Nov	9		Dec		J	an		F	eb		Mai	rch		Ap	ril		Ma	ay		Jur	ie		Ju	uly	Τ	A	ug	Т	Se	.p	Т	0	ct
				1	2 3	3 4	1	2 3	4	1 2	2 3	4	1 2	3	4 1	2	3 4	4 1	2	3	4 1	L 2	3	4 1	2	3	4 1	2	3	4		-	4 1	2	3	4 1	2	3 4
Α	Pre-Design & Form Finding Activities																										Т									T	$\square$	
1	Contract Award by Tri Arch to Sediabena	23-Nov-11	26-Nov-11																								Г			Т			Τ					
2	2 Meeting with Client and Consultant at Site	21-Nov-11	21-Nov-11																								Г						Τ					
3	3 Submission of Approval Final Roof Form Drawings	23-Nov-11	15-Dec-11																								Г									T	$\square$	
4	Submission of Reaction Forces of Columns	23-Nov-11	15-Dec-11																								Т						$\top$					
5	5 Technical Presentation	15-Dec-11	15-Dec-11																								Т									$\top$		
6	5 Submission of Revised Reaction Forces	15-Dec-11	23-Dec-11																											_	_	$\square$	$\mp$		—	$\bot$	$\square$	
В	Procurement of Long Lead Time Materials			+											+			╋						+			┢	۲	$\vdash$	+			+	-	+	╋	+	<u> </u>
7	Purchase of Fabric (Using Airfreight)	7-Dec-11	7-Mar-12																								Т			$\top$			$\top$		$\neg$	$\top$	$\square$	
	Purchase of Steel Materials	7-Dec-11	15-Apr-12																								Т									$\top$		
9	Purchase of Galvanised Cables	15-Dec-11	28-Apr-12																											$\mp$	_		十		_	Ŧ	$\square$	
с	Engineering & Design														+			╋		-				-			┢	+	$\vdash$	+			+	-	+	╋	+	
10	D Submission of Final Roof Dwgs	15-Dec-11	21-Jan-12																											1	_		$\mp$		_	T	$\square$	
D	Fabrication Works														+			+						-			┢	+	┝┼	+			+	-	+	+	+	<u> </u>
11	L Fabrication Of Steelworks	7-Jan-12	7-Jun-12																								Т						$\top$		-	+		
12	2 Fabrication of Fabric Works	15-Jan-12	15-Jun-12																											ゴ			十		_	t	$\square$	
E	Erection Works (Phase 1)	-		+											+			+		_				+			┢	+	$\vdash$	+	<u> </u>	<u> </u>	+	$\square$	+	╋	+	<u> </u>
13	Holding Down Bolts Installation for Columns	7-Jan-12	28-Feb-12																								╈	⊢					+		-	+	+	
	Frection of Steelworks	15-Apr-12	15-Jun-12																								╈	➡		+			+		+	+	+	
	Installation of Fabric	7-May-12	30-Jun-12															+										➡	H	+	+		+		+	+	+	
	Handing Over (Contract Finish Date)	, 30-Jun-12	30-Jun-12																											土			土		_	t		
F	SUKMA Games 2012	_		╉┼								-			+			╋						+			┢	+	$\vdash$	+	—	<u> </u>	+	$\vdash$	+	╋	+	<u> </u>
17	Aquatic Competitions	7-Jul-12	16-Jul-12																											1			十		$\pm$	T	$\square$	
G	Erection Works (Phase 2)			+					$\left  \right $			+			+			+			-			+		+	┢	-	$\vdash$	+		$\square$	╋	+	+	+	+	$\vdash$
	B Erection of Steelwork	1-Sep-12	14-Sep-12									+						+									╈			+					+	+	+	$\vdash$
_	P Installation of Fabric	7-Sep-12	21-Sep-12									+			+			+									╈			+	+				-	+	$\top$	
_	Post Tensioning Works of Fabrics		15-Oct-12									+			+			$\top$									╈			+			+					
	L Touching Up of Paints & Cables Tensioning		15-Oct-12									+			+						+						┢		H	+			+					
	2 Final Handing Over	15-Oct-12										+						$\top$									╈			+			+					
	č											+						+			$\top$						Т			+			+	$\square$	+	+		



Rev. 01 Date: 16 Jan 2012



# **11.2 ENGINEERING DRAWINGS**

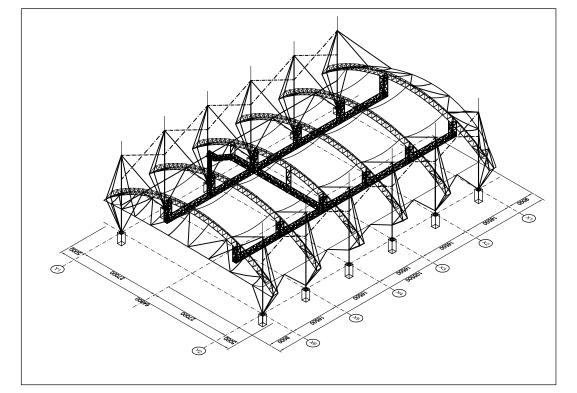








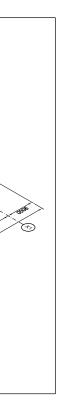
# PROPOSED TENSILE FABRIC ROOF SYSTEM AT KOMPLEKS KOLAM RENANG, WISMA BELIA INDERA MAHKOTA, KUANTAN, PAHANG DARUL MAKMUR. MALAYSIA.



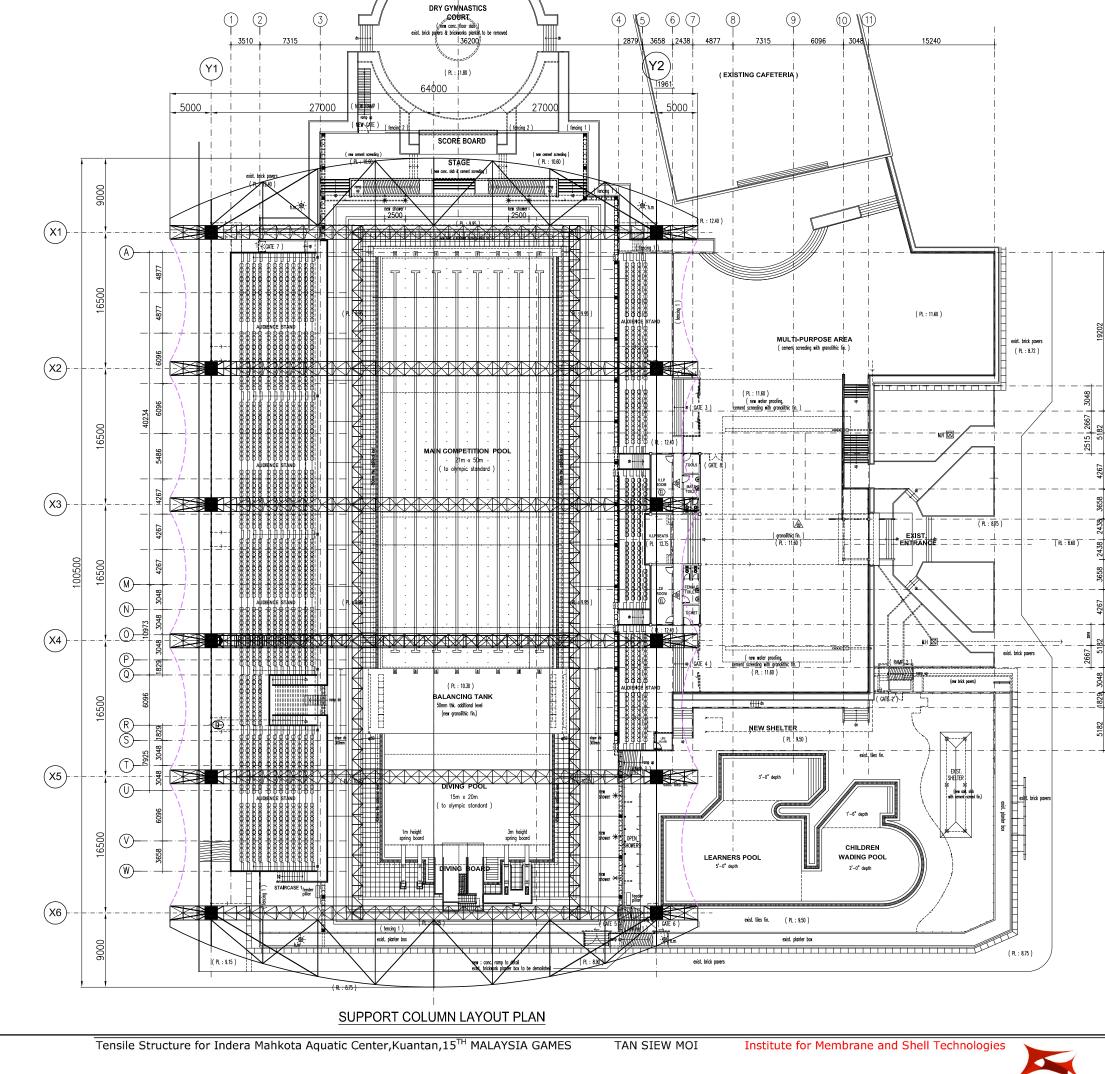
3D-VIEW OF STRUCTURE FRAMING

3D-VIEW OF STRUCTURE FRAMING + FABRIC





		Kom	pleks	Kolam F	Renang	
		NOTE :				55
			24.07.0040			
I۸		03 02	31.07.2012 20.04.2012		AS-BUILT GENERAL	
IA.		01	12.01.2012		GENERAL	
.,		REF	DATE		DESCRIPTION	
		OWNER : MAJ Jalan Pahar TEL : MAIN CON	LIS PE Tanah Putih ng Darul Mih 09–512155 VIRACTOR : SURAC 117–A, 15 JALAN MAI TEL :609–	RBANDAR A, 25100 Kuantu kmur, Malaysia. 5/666 FAKS HATI SD st. FLOOR, MI HKOTA, 25000 ARUL MAKMU	AN KUANTAN an, : 5130644 N. BHD. UIP BUILDING, D KUANTAN ,	
		0	Ŋ	SENDIRI B-26 Tingkat Sa	ATTES ARCENT AN BERHAD (74 atu, Jalan IM3/10 Vahkota Pahang Darul Makmur. 0 / 5738372 Fax: 09	5736443
		6	UNCTION WITH: SEE Ref. add Ref. a	7-1, JALAN 2/115 OFF JALAN KUC 58200 KUALA LU ETEL : 79812870 F. E-mail : triarch90 : : : : : : : : : : : : : : : : : : :	CH sdn. bhd. sa, Taman Pagaa Ruyoni Hai Liwa. Iweya. Ax : 78918210 Dig yahoo.com.my ENA schwarth Harry Strategy Strategy Strategy Strategy Strategy Strategy Strategy Strategy	Breat Agela a.com
			r's C&s and JU A-7 Jala Pahr	M&E: <b>RUNDING</b> 732, Tingkat Sc n Dato' Bahama ang Darul Makm	(G. sincerPorte 6092 2024 Emoil: sdee@transervet.co (HYH SDN. BH Hu, Kedai LKNP, n. 25200 Kuantan, ur. Faks : 09-560 1182	281 <sup>m.sg</sup>
		NO.C- 85 Jo Tel :	alan Loke•Ye 03-9200820	11, Menara Un w, 55200 Kuala 58 Fax : 03-	a Lumpur	
		KOLA BERK	ngan i M Ren (Aitan	di wisma	TA KERJA-KER	
		τιπιε : 3D	- View			
		DATE :	29.12.2011		DRAWN :	
		SCALE :	NTS		CHECKED :	
		DRAWING	NO. :			REVISION
		TA-	-Q326-	-01		03
Anhalt U	niversity of Applied S	Scien	ces, I	Dessau	2	1



	Kom	pleks	Kolam R	lenang	
	NOTE :				56
	03	31.07.2012	-	AS-BUILT	
	02 01	20.04.2012 12.01.2012		GENERAL GENERAL	
	ref	DATE		DESCRIPTION	
	OWNER :				
		Á	)		
	/				
	Ļ	Majlis Perja	andaran		
	<b>N</b>				
			RBANDAR	an kuantan	
	Pahan		kmur, Malaysia.	: 5130644	
		09-312133	137 000 FAK3	. 3130044	
	MAIN CON	TRACTOR :			
		suara	hati sdi	<b>N. BHD.</b>	
		117-A, 1st. Jalan Mahko	FLOOR, MUIP BUIL DTA, 25000 KUANT	DING, AN	
		PAHANG DAR	UL MAKMUR 15 2473, FAX : 6		
			.,		
	ARCHITECT	r's :			
			& ASSOC	UATES ARCHITI	ects
	d	7	SENDIRI	AN BERHAD (7	H200-P)
	4	<b>س</b> ال		atu, Jalan IM3/10 Jahkota Pahang Darul Makmur,	
		-	Tel: 09-573643	0/5736372 Fax: 09	5736443
	SPECIALIS		CLADDING CONTRAC		
	A			CH sdn. bhd. 54. TAMAN PAGAR RUYOI	NG
		y	OFF JALAN KUC 58200 KUALA LU TEL : 79812870 F	5A, TAMAN PAGAR RUYOI HAI LAMA, MPUR. AY : 78818210	
			E-mail : triarch9	D@yahoo.com.my	
	in conju	NCTION WITH	ŧ		
		SE	DIAB	ENA ann. an	D.
		No. 11, Jalan Tel : 903-7847		elutorg, 40150 Shah Alam, Selangor Devil Broan, Via e-mail tempiny@sectaber vetsita : www.sectaber	laysla. a.com
		(Lompany No	(1000(1941) &	vecete : www.sediader	e.com
	TRA	ICEPVE		CRVE PTE LI	'D
	39 P	ANDAN R	J ROAD, JURON	CRVE PTE L1 (co. Reg. Mol: 197702) G, SINGAPORE 6092 24 Email: sales@transervet.co	нзм) 281
					,
	ENGINEER	'S C&S and	M&E:		
	6			hyh sdn. Bh	id.
	7	A-7 Jala	732, Tingkat Sa In Dato' Bahama	tu, Kedai LKNP, m, 25200 Kuantan,	
		Pan	ang Darul Makm	ur. Faks : 09-560 1182	
	-				
	QUANTITY	SURVEYOR :			
	S	èP	en	DÎTA	
	N0.C-	9-9, Level	11, Menara Una	cang Emas,	
	85 Ja Tel :	lan Loke¶Y€ 03-920082	ew, 55200 Kuala 68 Fax : 03–	Lumpur	
	email:	info@pendi	ta.com.my we	bsite: pendita.com.my	
	PROJECT	:			
			MENAIK T		
				TA KERJA-KER	JA
			di Wisma Hkota, ki	uantan. Malan	ISIA.
	TITTLE :				
	SUP	PORT CO	olumn layo		
	301				
	DATE :	29.12.2011		DRAWN :	
	SCALE : DRAWING			CHECKED :	REVISION
			00		
	IA-	-Q326-	-02		03
plied 9	Scien	ces. I	Dessau	_	•
				-	

–(B) -C) -D -E -(F) -6 -(H)

-(A)

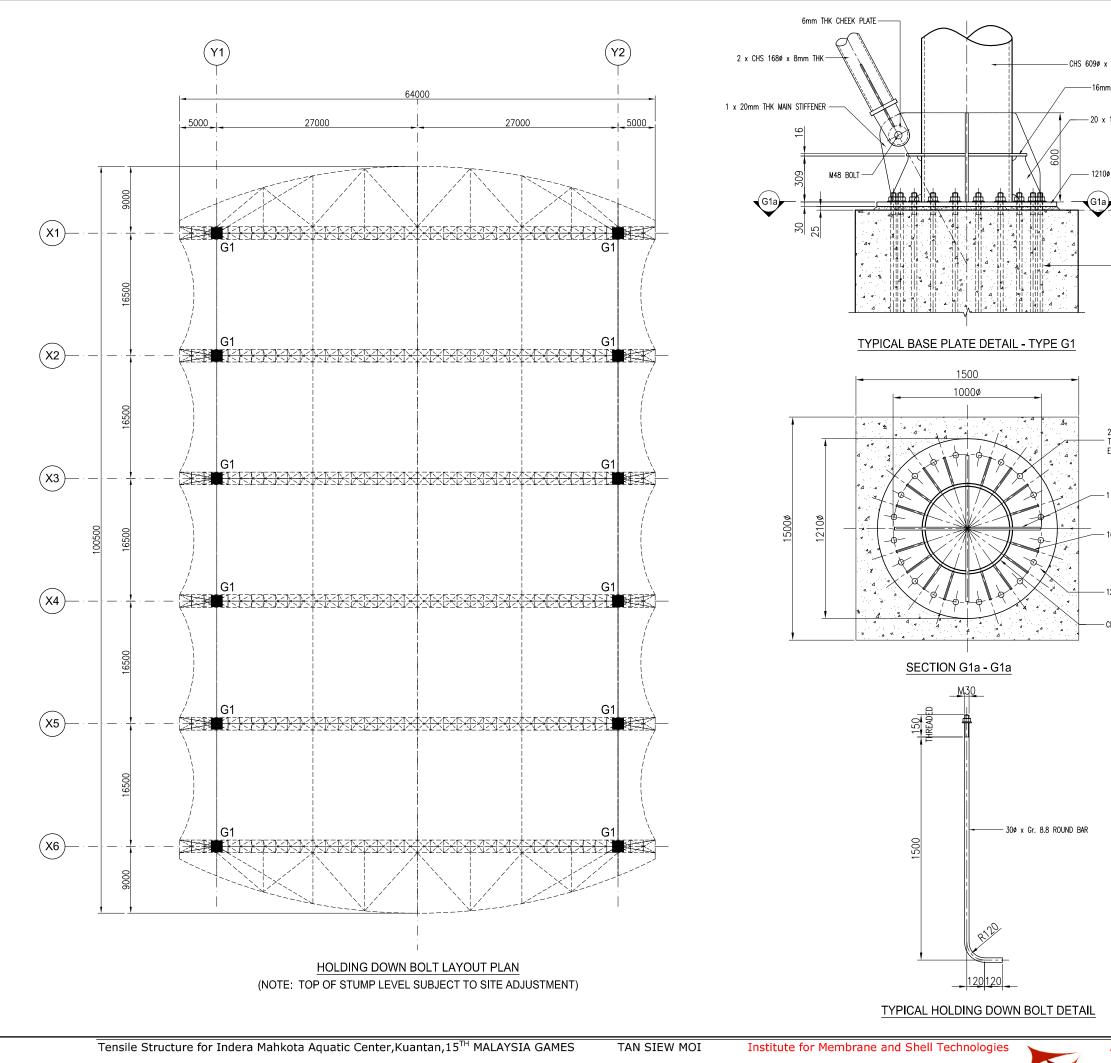
-(1)

-(J)

-(K)

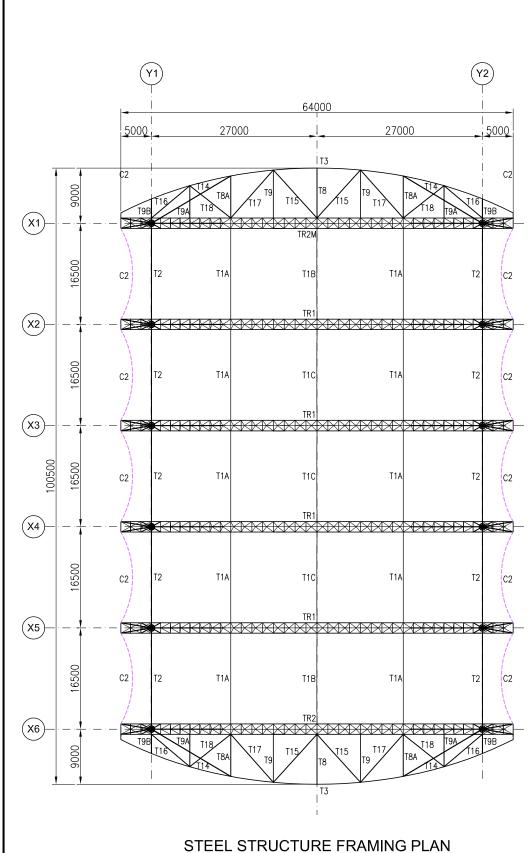
-(L)

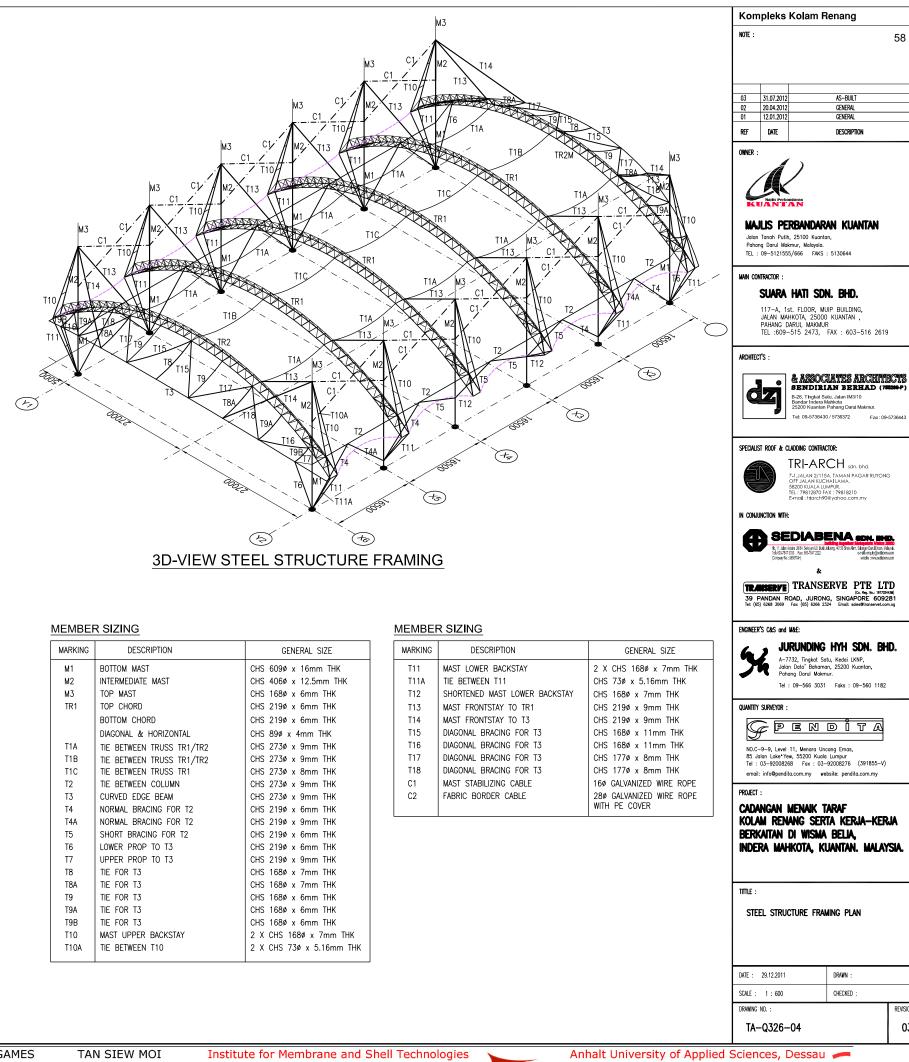
Anhalt University of App





	Kompleks Kolam Renang
16mm THK	
Ibmm IHK	
THK PLATE	03 31.07.2012 AS-BUILT 02 20.04.2012 GENERAL
12mm THK STIFFENER	01 12.01.2012 GENERAL
	REF DATE DESCRIPTION
	OWNER :
ø x 30mm THK BASE PLATE	
TOP OF STUMP	
	MAJLIS PERBANDARAN KUANTAN
	Jalan Tanah Putih, 25100 Kuantan, Pahang Darul Makmur, Malaysia. TEL : 09-5121555/666 FAKS : 5130644
20 x M30 HOLDING DOWN BOLT — THREADED AT TOP WITH MIN	WAIN CONTRACTOR :
EMBEDMENT 1500mm DEPTH	SUARA HATI SDN. BHD.
	117-A, 1st. FLOOR, MUIP BUILDING,
	JALAN MAHKOTA, 25000 KUANTAN , PAHANG DARUL MAKMUR TEL:609-515 2473, FAX : 603-516 2619
	ARCHITECT'S :
	& ASSOCIATES ARCHITECTS SENDIRIAN BERHAD (78220-P) B-26, Thgkat Satu, Jalan (M3/10
	Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.
	Tel: 09-5736430 / 5736372 Fax: 09-5736443
20 x M30 HOLDING DOWN BOLT THREADED AT TOP WITH MIN	SPECIALIST ROOF & CLADDING CONTRACTOR:
EMBEDMENT 1500mm DEPTH	
	7-1, JALAN 2/115A, TAMAN PAGAR RUYONG OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR. TEL: 79812870 FAX: 79818210
x 20mm THK MAIN STIFFENER	E-mail : triarch90@yahoo.com.my
	IN CONJUNCTION WITH:
16 x 12mm THK STIFFENER	<b>SEDIABENA con, pro.</b> N: 11. Markada UNIS Sanger Vi Balt Alary, 4719 San Att, Sanger Dal Esas, Mahri, erafi sen falkataria.
	14: 101-104 7 333 Fac: 101-114 7 222 e-seaf: engingised bencion (Corpory/No: 106076-4) webte: rowcostibion.com
	TRANSERVE TRANSERVE PTE LTD
1210ø x 30mm THK BASE PLATE	39 PANDAN ROAD, JURONG, SINGAPORE 609281 Tel: (65) 6268 3369 For: (65) 6266 2324 Email: sales@transervet.com.sg
CHS 609ø x 16mm THK	ENGINEER'S C&S and M&E:
	🖌 🍃 JURUNDING HYH SDN. BHD.
	A-7732, Tingkat Satu, Kedai LKNP, Jalan Dato' Bahaman, 25200 Kuantan, Pahang Darul Makmur.
	Tel : 09-566 3031 Faks : 09-560 1182
	QUANTITY SURVEYOR :
	<b>GPEND</b> ita
	NO.C-9-9, Level 11, Menara Uncang Emas, 85 Jalan Loke Yew, 55200 Kuala Lumpur
	Tel: 0.3-92008268 Fox: 0.3-9208276 (391855-V) email: info@pendita.com.my website: pendita.com.my
	PROJECT :
	CADANGAN MENAIK TARAF
	kolam renang serta kerja—kerja Berkaitan di Wisma Belia,
	INDERA MAHKOTA, KUANTAN, MALAYSIA.
	HOLDING DOWN BOLT LAYOUT PLAN
	& DETAILS
	DATE : 29.12.2011 DRAWN :
	DALE : 29.12.2011 DRAWN : SCALE : 1 : 500 / 1 : 20 CHECKED :
	DRAWING NO. : REVISION
	TA-Q326-03 03
	1 4020 00 1 00





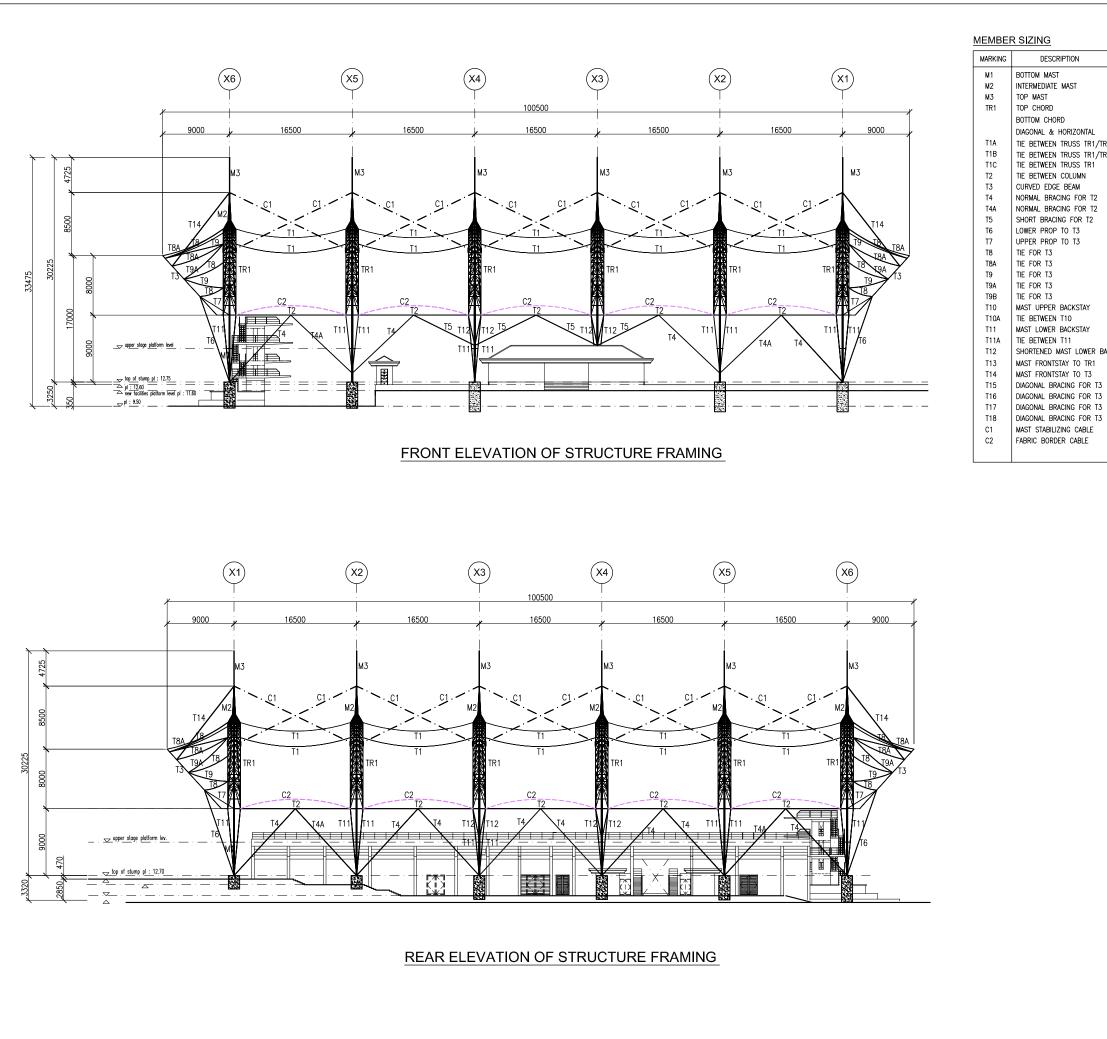
58

REVISION 03

MEMBER	R SIZING	
MARKING	DESCRIPTION	GENERAL SIZE
M1	BOTTOM MAST	CHS 609Ø x 16mm THK
M2	INTERMEDIATE MAST	CHS 406ø x 12.5mm THK
M3	TOP MAST	CHS 168Ø x 6mm THK
TR1	TOP CHORD	CHS 219ø x 6mm THK
	BOTTOM CHORD	CHS 219ø x 6mm THK
	DIAGONAL & HORIZONTAL	CHS 89ø x 4mm THK
T1A	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1B	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1C	TIE BETWEEN TRUSS TR1	CHS 273ø x 8mm THK
T2	TIE BETWEEN COLUMN	CHS 273ø x 9mm THK
T3	CURVED EDGE BEAM	CHS 273ø x 9mm THK
T4	NORMAL BRACING FOR T2	CHS 219ø x 6mm THK
T4A	NORMAL BRACING FOR T2	CHS 219ø x 9mm THK
T5	SHORT BRACING FOR T2	CHS 219ø x 6mm THK
T6	LOWER PROP TO T3	CHS 219ø x 6mm THK
T7	UPPER PROP TO T3	CHS 219ø x 9mm THK
T8	TIE FOR T3	CHS 168ø x 7mm THK
T8A	TIE FOR T3	CHS 168ø x 7mm THK
Т9	TIE FOR T3	CHS 168ø x 6mm THK
T9A	TIE FOR T3	CHS 168ø x 6mm THK
T9B	TIE FOR T3	CHS 168ø x 6mm THK
T10	MAST UPPER BACKSTAY	2 X CHS 168ø x 7mm THK
T10A	TIE BETWEEN T10	2 X CHS 73ø x 5.16mm THK

MARKING	DESCRIPTION
T11	MAST LOWER BACKSTAY
T11A	TIE BETWEEN T11
T12	SHORTENED MAST LOWER BACKST
T13	MAST FRONTSTAY TO TR1
T14	MAST FRONTSTAY TO T3
T15	DIAGONAL BRACING FOR T3
T16	DIAGONAL BRACING FOR T3
T17	DIAGONAL BRACING FOR T3
T18	DIAGONAL BRACING FOR T3
C1	MAST STABILIZING CABLE
C2	FABRIC BORDER CABLE







	GENERAL SIZE
	CHS 609ø x 16mm THK
	CHS 406ø x 12.5mm THK
	CHS 168ø x 6mm THK
	CHS 219Ø x 6mm THK
	CHS 219ø x 6mm THK
	CHS 89ø x 4mm THK
R2	CHS 273ø x 9mm THK
R2	CHS 273ø x 9mm THK
	CHS 273ø x 8mm THK
	CHS 273ø x 9mm THK
	CHS 273ø x 9mm THK
	CHS 219ø x 6mm THK
	CHS 219Ø x 9mm THK
	CHS 219Ø x 6mm THK
	CHS 219Ø x 6mm THK
	CHS 219ø x 9mm THK
	CHS 168ø x 7mm THK
	CHS 168ø x 7mm THK
	CHS 168ø x 6mm THK
	CHS 168Ø x 6mm THK
	CHS 168ø x 6mm THK
	2 X CHS 168Ø x 7mm THK
	2 X CHS 73ø x 5.16mm THK
	2 X CHS 168ø x 7mm THK
	CHS 73ø x 5.16mm THK
ACKSTAY	CHS 168Ø x 8mm THK
	CHS 219Ø x 9mm THK
	CHS 219Ø x 9mm THK
	CHS 168ø x 11mm THK
	CHS 168Ø x 11mm THK
	CHS 177ø x 8mm THK
	CHS 177ø x 8mm THK
	16ø GALVANIZED WIRE ROPE
	28ø GALVANIZED WIRE ROPE WITH PE COVER

Note :		Kolam Renang	59
03	31.07.2012	AS-BUILT	
02 01	20.04.2012	GENERAL GENERAL	
REF	DATE	DESCRIPTION	
Jalar Paho	n Tanah Putih	RBANDARAN KUANTAN , 25100 Kuantan, kmur, Malaysia. 5/666 FAKS : 5130644	
MAIN CC	117-A, 1s	HATI SDN. BHD. st. FLOOR, MUIP BUILDING, HKOTA, 25000 KUANTAN , ARUL MAKMUR -515 2473, FAX : 603-516 261!	9
	cr's :	& ASSOCIATES ARCENT SENDIALSIA BERHAD (7 5-25 Thyla Lalan 183/10 Bandar Indera Markota 25200 Kuantan Pahang Danu Makmur. Tek: 09-5738430 / 5738372 Fax: 08	
SPECIAL		LADDING CONTRACTOR: TRI-ARCH sdn. bhd. Z-Lualan 2/1154, Taman Pagar Ruyon	ic.
	UNCTION WITH: B B B B B B B B B B B B B B B B B B B	off JALAN KUCHA LAMA. Sobo KUALA UWHUR: Bend Hardwerk 798 200 Character 1998 200 Characte	аран Ануак акал акал ТДД 281
<b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b>	UNICTION WITH: SEE Mitting	S2000 KUALA LUMPUR, ETT: 7981/2010 KT: 7981/2010 Email: HanchP008 yahoo.com.my Email: HanchP008 yahoo.com.my etauWith Stever R. J. Market Market R. J. Market R. J. Market R. J. Market Market R. J. Market R. J.	ED Marka Assor HAM 281 mag
ENGINEE	UNICTION WITH: SEE Mitting	SB200 KUALA LUMPUR ETT-794 1220 YA: 794 12210 ETT-194 1220 YA: 794 1220 ETT-194 1200 YA: 794 1200 YA ETT-194 1200 YA	ED Marka Assor HAM 281 mag
	UNICTION WITH SEE THE SEA THE SEA T		ED Marka Assor HAM 281 mag
	UNICTION WITH: SEE SEE SEE SEE SEE SEE SEE SE		E CU Markin Mark
	UNICTION WITH: BEED SEE In Like I In Like I In Like I In Like I In Like I In Like I In Like I I I I I I I I I I I I I I		EL CONTRACTOR DE LA CON
	UNICTION WITH: B SE AT Light ACTION		EL CONTRACTOR DE LA CON
	UNICTION WITH:	SB202 KUALA LUMPUR ETT. 7981 2201 OK ETT. 7981 2201 OK AND	TD Wall Wall Hone TD TD.
	UNICTION WITH:	SB200 KUALA LUMPUR:           ETTORIZIO TALY 79818210           Email: HunchY09ydhoo.com.my           EDIABBENA gon, BD           MEDIABENA gon, BD           Mark UK Sueut B. Lakes MSS & dia Share a Share balanta Mark UK Sueut B. Lakes MSS & dia Share a Share balanta (Kangan a Share a Share a Share balanta (Kangan a Share a Share a Share balanta (Kangan a Share a Share balanta (Kangan a Share a Share balanta (Kangan a Share a Share a Share balanta (Kangan a Share a Share a Share balanta (Kangan a Share a Share a Share a Share balanta (Kangan a Share a Share a Share a Share a Share a Share a Share a Share a Share a Share a Share a Share a Share a (Kangan a Share	E CU Market Mark



T1A

T1B T1C T2

T3

T4

T4A

T5 T6 T7 T8 T8A T9 T9A T9B

T10

T10A

T11

T11A

T12

T13

T14

T15

T16 T17 T18 C1 C2 DIAGONAL & HORIZONTAL

TIE BETWEEN COLUMN

NORMAL BRACING FOR T2 NORMAL BRACING FOR T2 SHORT BRACING FOR T2 LOWER PROP TO T3 UPPER PROP TO T3

CURVED EDGE BEAM

TIE FOR T3 TIE FOR T3

TIE FOR T3

TIE FOR T3

TIE FOR T3

MAST UPPER BACKSTAY

MAST LOWER BACKSTAY

MAST FRONTSTAY TO TR1

MAST FRONTSTAY TO T3

DIAGONAL BRACING FOR T3

DIAGONAL BRACING FOR T3

DIAGONAL BRACING FOR T3 DIAGONAL BRACING FOR T3

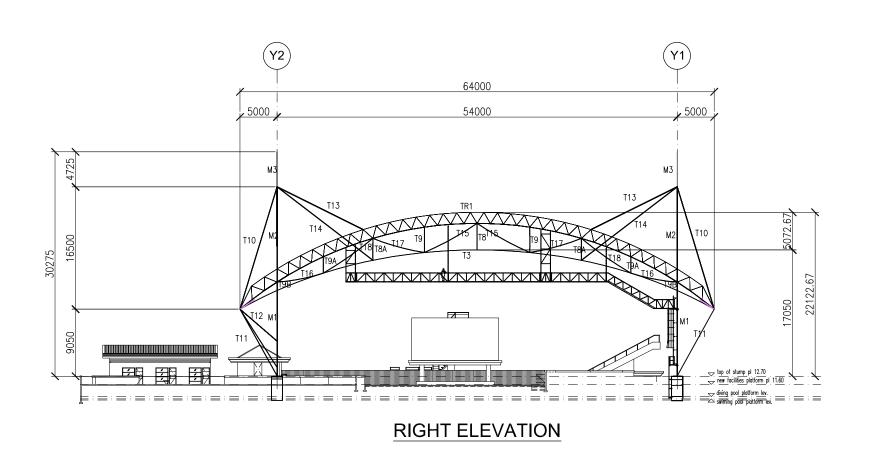
MAST STABILIZING CABLE FABRIC BORDER CABLE

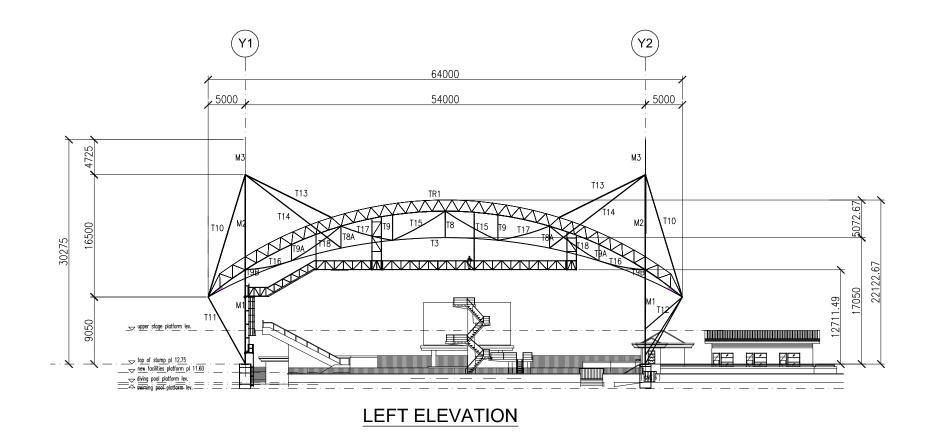
SHORTENED MAST LOWER BACK

TIE BETWEEN T10

TIE BETWEEN T11

TIE BETWEEN TRUSS TR1/TR2 TIE BETWEEN TRUSS TR1/TR2 TIE BETWEEN TRUSS TR1

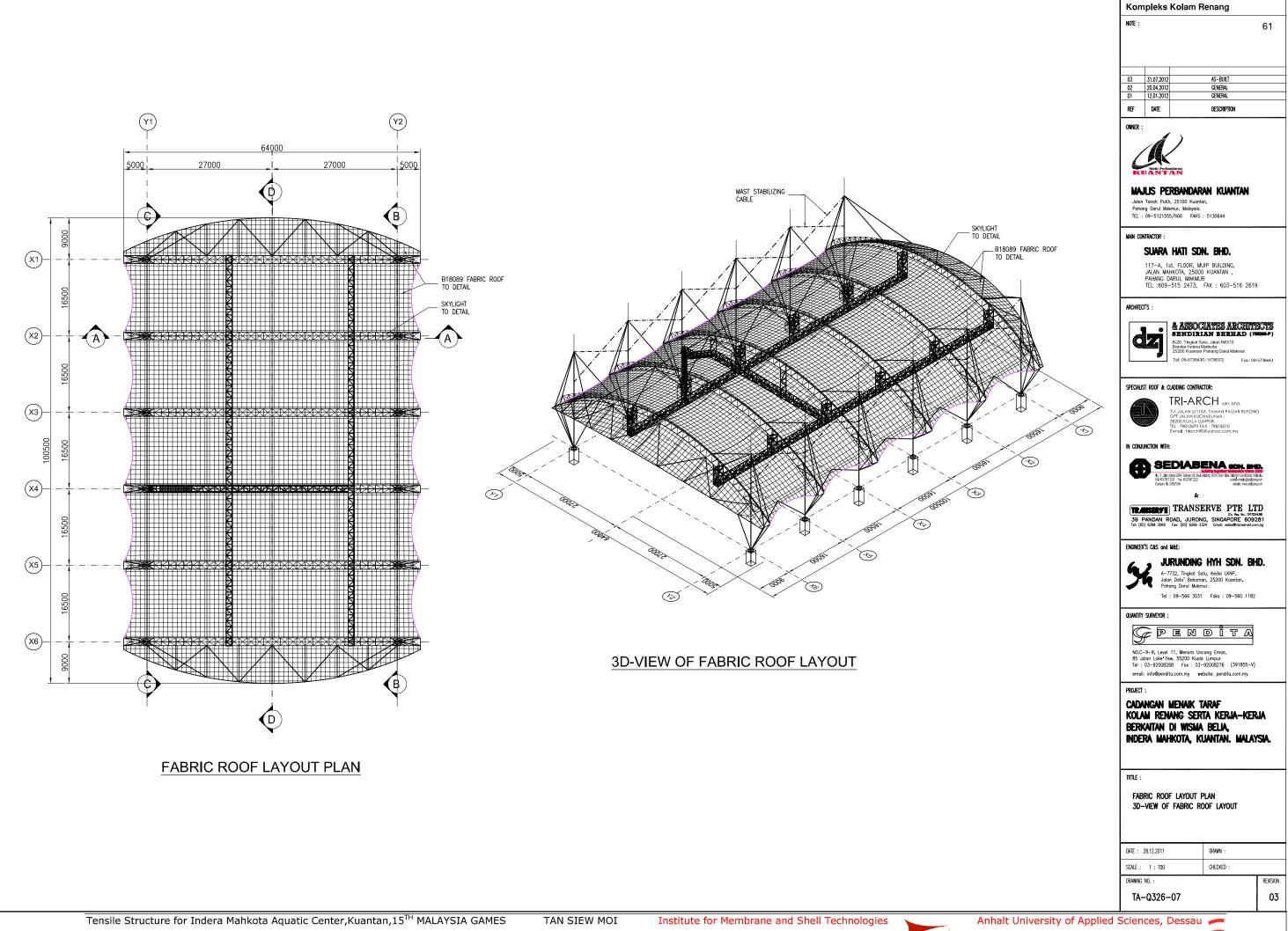




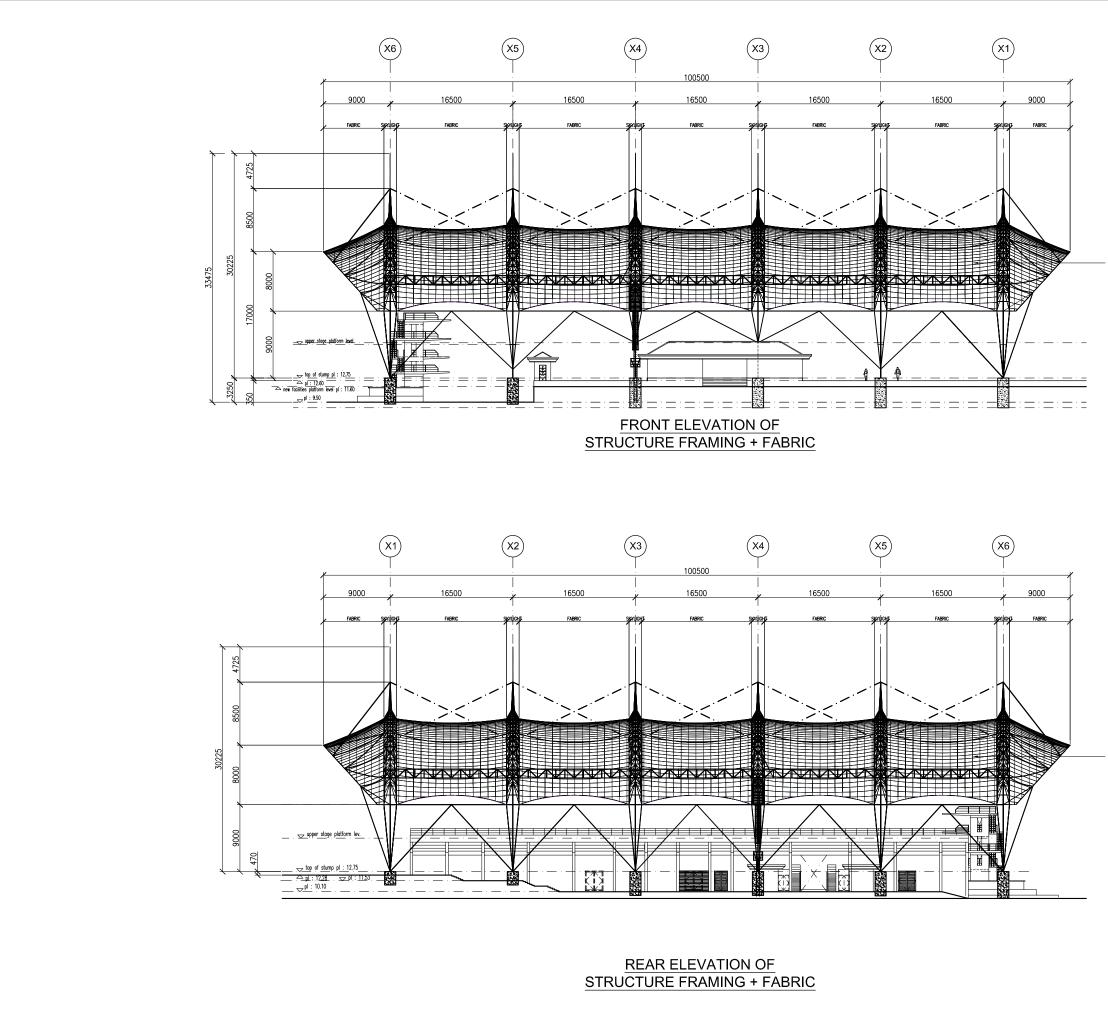


Anhalt University of Applied

NOTE :			
			60
03 02	31.07.2012 20.04.2012	AS-BUILT	
02	12.01.2012	GENERAL GENERAL	
ref	DATE	DESCRIPTION	
OWNER :			
	Â	)	
	K		
K		AN	
		RBANDARAN KUAN	TAN
Paha		, 25100 Kuantan, (mur, Malaysia. 5/666 FAKS : 5130644	
		,	
MAIN CO	NTRACTOR :		
		HATI SDN. BHD.	
	JALAN MA	st. FLOOR, MUIP BUILDING, HKOTA, 25000 KUANTAN , ARUL MAKMUR	
	TEL :609-	-515 2473, FAX : 603-5	16 2619
ARCHITEC	ct's :		
		& ASSOCIATES AR	CHIFECTE
		SENDIRIAN BERH. 8-26 Tindket Setu. Jalan 1M3(10)	AD (755269-P)
	<b>س</b>	Bandar Indera Mahkota 25200 Kuantan Pahang Darul Mal	kmur.
		Tel: 09-5736430 / 5736372	Fax: 09-5736443
SPECIALI	ST ROOF & C	LADDING CONTRACTOR:	
		TRI-ARCH sdn. bh	_
		7-1, JALAN 2/115A, TAMAN PAGA OFF JALAN KUCHAI LAMA.	
	J	58200 KUALA LUMPUR. TEL : 79812870 FAX : 79818210	
		E-mail: triarch90@vahoo.com.m	
IN CONJ	unction with:	E-mail : tifarch90@yahoo.com.m	У
in conj	unction with		
IN CONJ	<b>)</b> 8E		N. 840.
	<b>)</b> 8E	DIABENA co adulti Sieger (II. Jahr alorg 47/57 See Alm. See Satur State	N. 840.
Ð	R. 11, Jalan / Tel: KG-TAW (Company No:	DIABBENA co cal 1845 Segre II. Birl Auro, 2/17 Sen Min Sel Star 1845 March 2022 est March 2015 &	ya Dan Elwan Mahyak Jena ying Benda da Katala Jena ying Benda da Katala Marina Marina Mahaka katala Marina Mahaka Katala
	Na. 11, Jaho Na. 11, Jaho Tal roto Tor Company Na:	COLORENA CONSISTENT OF COLORENA CONSISTENT. OF COLORENA CONSISTENT OF COLORENA CONSISTENT OF COLORENA CONSISTENT. OF COLORENA CONSISTENT OF COLORENA CONSISTENT. OF COLORENA CONSISTENT OF COLORENA CONSISTENT. OF COLORENA COLORENA CONSISTENT. OF COLORENA CO	The sector of th
	Na. 11, Jaho Na. 11, Jaho Tal roto Tor Company Na:	CIABEENA co catalide Segre il dat dars e 19 Statich sign stat faits faits faits and statistic faits and catality k TRANSERVE PT GAD, JURONG, SINGAPOR	n and a state of the state of t
39 Tet: (62	A II Jaho It II Jaho I	COLOR STATES STA	no bulletare Malajat. retari fijimi detearan Mic versak detearan Mic uterak detearan Mic
39 Tet: (62	SEE H. I. And Id VISION (Contrary No: NISSERVE PANDAN R PANDAN R PANDAN R PANDAN R S C&S and JU	COLORS ENANCE OF COLORS OF	Andreas Mark Andreas Mark Michael Michael Mark Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Michael Mark Michael Michael Michael Michael Mark Michael M
39 Tet: (62	SEE It. 1. Jan. Id:05.367 (Carazer/HC: PANDAN R PANDAN R S) 6268 JOB9 R'S C&S and JU A-7 Join	COLOR LANGE AND	Andreas Mark Andreas Mark Michael Michael Mark Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Mark Michael Michael Michael Mark Michael Michael Michael Michael Mark Michael M
39 Tet: (62	SE It is in data (organy its: (organy its	COLORS ENANCE OF COLORS OF	2010 Bar Mark 2010 Bar Mark 42: Washington Bar 42: Washington Bar 19: E 6092 81 19: E
A 39 Tet (8) ENGINEER	SE It is in data (organy its: (organy its	COLOR STATES AND A	2010 Bar Mark 2010 Bar Mark 42: Washington Bar 42: Washington Bar 19: E 6092 81 19: E
ENCINEE	SEE It is the internet in the set of the internet internet PANDAN R PANDAN R PANDAN R PANDAN R PANDAN R PANDAN R J J J J J J J J J J J J J J J J J J J	COLORES CONTRACTOR OF CONTACTOR OF CON	2010 Bet Mark 2010 Bet Mark 1010 B
	SEE In the second In the second I	COLOR OF A Large delivery of the second of t	2010 Bet Mark 2010 Bet Mark 1010 B
	SEE SEE Second	COLOR OF A Large A large a ling stand and and a ling stand and a ling stand and a ling stan	2010 Bon Mark 2010 Bon Mark 2010 Bon Mark 2010 Bon Mark 2010 Bon 2010 B
	SEE SEE Second	COLORES AND A COLOR OF COLOR O	<b>21.2.2.5.</b> 21.2.2.5. <b>21.2.2.5.</b> <b>21.2.2.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.5.</b> <b>21.2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5</b>
ENCINEER COUNTER SUBJECTION	SEE Line In the li	COLORED ENCA detailing dear it start deriver deriver der detailing deriver der deriver der der der der TRANSERVE PTT (A. A. CAD, JURONG, SINGAPOR For: (s) 8266 2324 Erneit: edered MAE: RUNDING HYH SDI 732, Tingket Sotu, Kedei LKNP, n Doto' Behamon, 25200 Kunnt ng Darul Makmur. : 09–566 3031 Foks : 09–5 E N D I T 11. Venore Uncong Ernes, * 55200 Kunle Lumpur 8 Fax : 03–92008276 (39	<b>21.2.2.5.</b> 21.2.2.5. <b>21.2.2.5.</b> <b>21.2.2.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.5.</b> <b>21.2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5</b>
	SEE SEE SUBSERVE CONSTRUCTION CONSTRUCTI	COLOR DE CALL COLOR DE COLOR	<b>21.2.2.5.</b> 21.2.2.5. <b>21.2.2.5.</b> <b>21.2.2.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.</b> <b>21.2.5.5.5.</b> <b>21.2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5</b>
CUMPTER PROJECT CADA	SEE     S	COLORED ENCA detailing dear it start deriver deriver der detailing deriver der deriver der der der der TRANSERVE PTT (A. A. CAD, JURONG, SINGAPOR For: (s) 8266 2324 Erneit: edered MAE: RUNDING HYH SDI 732, Tingket Sotu, Kedei LKNP, n Doto' Behamon, 25200 Kunnt ng Darul Makmur. : 09–566 3031 Foks : 09–5 E N D I T 11. Venore Uncong Ernes, * 55200 Kunle Lumpur 8 Fax : 03–92008276 (39	2010/10-10-100 2010/10-10-100 4: Workshow 4: Workshow 5: Without 5: Big 1: Without 5: Big 1: Without 5: Big 1: Big
	SEE SEE SUBSERVIC CONTRACTOR CONTRACTOR SUBSERVIC CONTRACTOR SUBSERVIC	COLORS IN COLORS	2010 100 1400 2010 100 2010 201
	SEE SEE SUBSERVIC CONTRACTOR CONTRACTOR SUBSERVIC CONTRACTOR SUBSERVIC	COLOR DE LA Large d'Alfred de la Color de	2010 100 1400 2010 100 2010 201
	SEE SEE SUBSERVIC CONTRACTOR CONTRACTOR SUBSERVIC CONTRACTOR SUBSERVIC	COLORS IN COLORS	2010 100 1400 2010 100 2010 201
	SEE SEE SUBSERVIC CONTRACTOR CONTRACTOR SUBSERVIC CONTRACTOR SUBSERVIC	COLORS IN COLORS	2010 100 1400 2010 100 2010 201
	SEE	COLORES CONTRACTOR OF CONTRACT	2010 100 1400 2010 100 2010 201
	SEE SEE SUBSERVIC CONTRACTOR CONTRACTOR SUBSERVIC CONTRACTOR SUBSERVIC	COLORS CONTRACTORY CONTRACTOR	2010 100 1400 2010 100 2010 201
	SEE     S	COLORS CONTRACTORY CONTRACTOR	2010 100 1400 2010 100 2010 201
	SEE     S	COLORS CONTRACTORY CONTRACTOR	2010 100 1400 2010 100 2010 201
	SEE     S	COLORS CONTRACTORY CONTRACTOR	2010 100 1400 2010 100 2010 201
	SEE     S	COLOR STATES CONTRACT STATES STA	2010 100 1400 2010 100 2010 201
	SEE     S	CONCEPTION OF C	
	SEE     S	COLORES CONTRACTOR OF CONTRAC	2010 100 1400 2010 100 2010 201







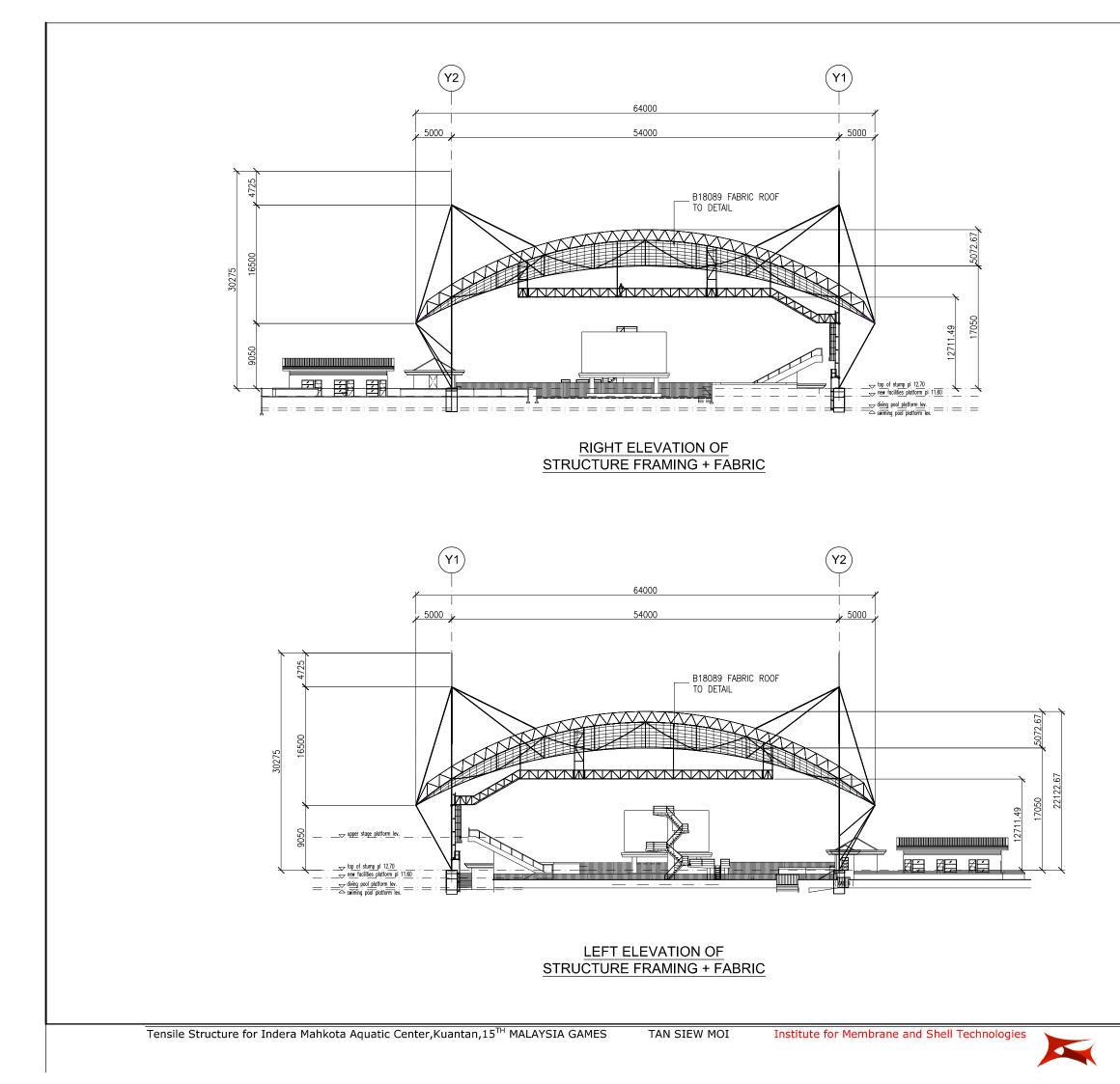


\_ B18089 FABRIC ROOF TO DETAIL

B18089 PTFE COATED FABRIC ROOF

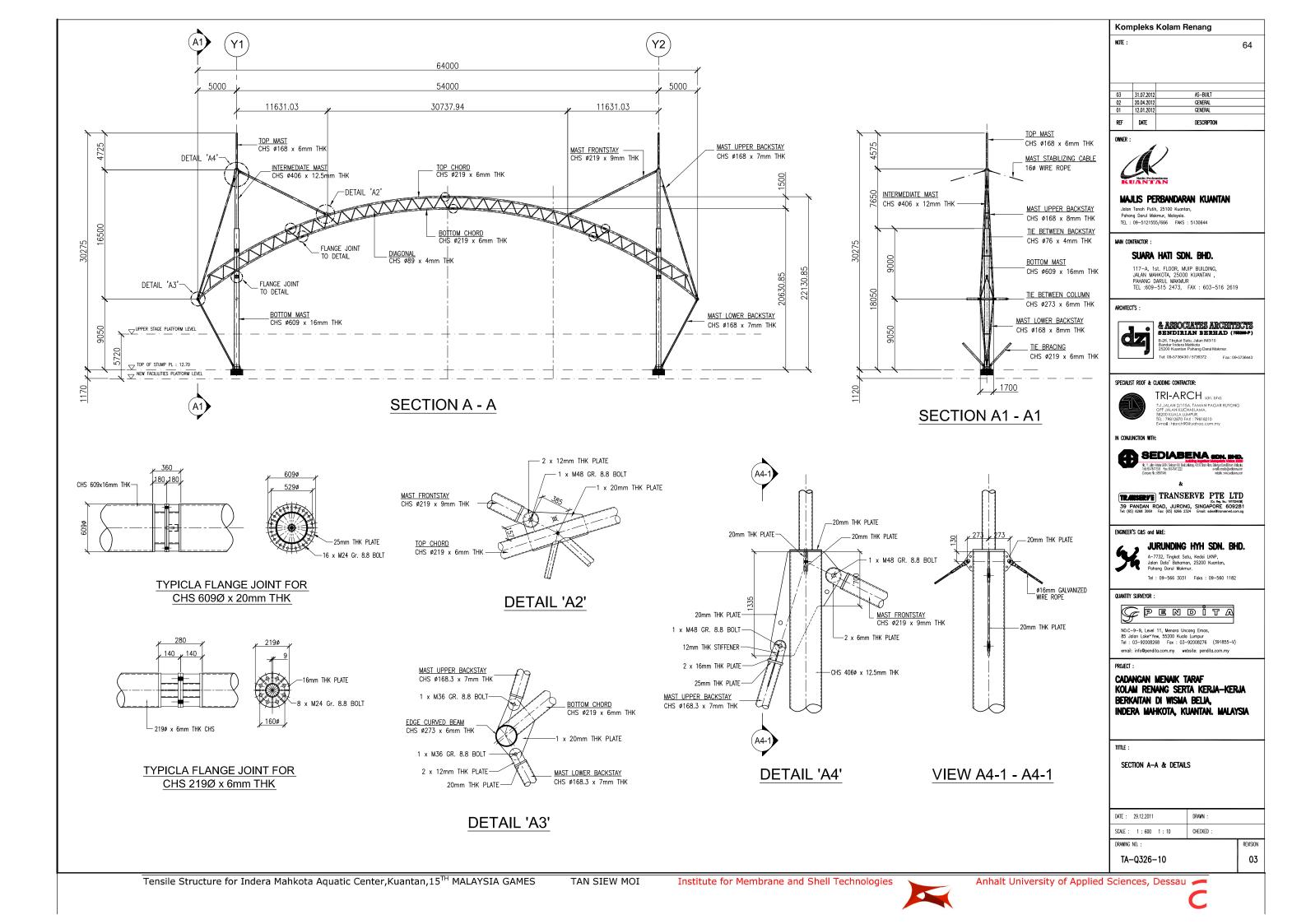
NOTE :		Kolam Renang	
			62
07	31 07 2012		
02 :	31.07.2012 20.04.2012	AS-BUILT GENERAL	
01 REF	12.01.2012 DATE	GENERAL	
OWNER :			
KU	Manilis Perine	undaran A N	
Jalan T Pahang	lanah Putih Darul Mal	RBANDARAN KUANTAN n, 25100 Kuantan, kmur, Malaysia.	
TEL : O	9-512155	5/666 FAKS : 5130644	
MAIN CONTI			
-		HATI SDN. BHD. st. floor, muip building,	
J P	ialan ma Pahang r	ST. FLOOR, MOIP BUILDING, HKOTA, 25000 KUANTAN , DARUL MAKMUR	
Ť	TEL :609-	-515 2473, FAX : 603-516 2619	
ARCHITECT'S	S :		
		& ASSOCIATES ARCHIT	ana Ana
		SENDIRIAN BERHAD (75	
	≝∦	B-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.	
L	-	Tel: 09-5736430 / 5736372 Fax: 09-	5736443
SPECIALIST		LADDING CONTRACTOR:	
A		TRI-ARCH sdn. bhd. 7-1. Jalan 2/115a, Taman Pagar Ruyong	3
Č	y	7-1, JALAN 2/115A, TAMAN PAGAR RUYONG OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR, TEL - 7091970 FAX - 70919210	-
		TEL : 79812870 FAX : 79818210 E-mail : triarch90@yahoo.com.my	
in conjun	iction with	:	
	) SE		D.
Ð	8E No. 11, Jaken Tel: 602-7547		aysta.
Ð		kelala U884, Seksyer U8, Bull, Heknong, 40161 Shah Hani, Selango Davi Elsan, Mal Solati, Faci, 803-1447 2222 e-mali, eng.hygosobbeno 18667344) websie : rww.sekabeno	aysta acom acom
e	No. 11, Jalan Tel: 603-7847 (Company No	ketala 1084: Seksyen UB, Bull Jahloog, 2019) Syat Han, Sahayon Davillensan Mal 3331 Fan, 463-3441 2222 (1957-344) website inverseducers 8657-344)	
39 PA	No.11, Jaker Tel: 5027447 (Company No ISERVIE	een USS Server U. Bal Alters 515 Sur Ha. Saryor Driffson Ha 300 Far 18547 (22) 880 FM & TRANSERVE PTE LT	'D
39 PA	No.11, Jaker Tel: 5027447 (Company No ISERVIE	etan USA Sayar (U. Bal Mare, SUS Sur An, Shyrr Erdifferer M Sus Francischer 222 sector and galaxies sector average and a superior of the su	'D
39 PA Tel: (65)	No.11, Jaker Tel: 5027447 (Company No ISERVIE	etat 1883. Steve II. Bal Mars, SISS an An Shryr Initizen 18 2007 in: 1000 2007 2007 2007 2007 2007 2007 2007	'D
39 PA Tel: (65)	With deal Interestion Concervite ISERVIE ANDAN R 6266 3069	etat 1883. Steve II. Bal Mars, SISS an An Shryr Initizen 18 2007 in: 1000 2007 2007 2007 2007 2007 2007 2007	<b>'D</b> 181 n.sg
39 PA Tel: (65)	No. 11. elec Tel: 8023957 (Carceny)/b SERRI/E NDAN R 6268 3069 5 C&S and 5 C&S and	Hen Was server at an Alexe, SIN See An Strong and Server at a serv	<b>'D</b> 181 n.sg
39 PA Tel: (65)	NIT SERVE	An USA Server at an Alexa, Salt See An School and Server at a School	<b>'D</b> 181 n.sg
39 PA Tel: (65)	NIT SERVE	An USA Sterrent and Allers All See An School and See Allers and School and Sc	<b>'D</b> 181 n.sg
39 PA Tel: (65)	NIT SERVE	And USE Steppen is an Allerge All See An Schopfungter Market 200704 200702 200700000000	<b>'D</b> 181 m.sg
39 PA Tel: (65)	W, 11, data Tat. 883-847 (Corpany)& SERV/E NADAN R 6268 3069 CddS and JU A-7 Jola Pah Tel	And Walk Steppen is an Allerg All See An Schopfungter Market 2007 Annotation and Allerge All See All Schopfungter Market 2007 Annotation and Allerge All See All S	<b>'D</b> 181 m.sg
	SERVE Coronyb SERVE SCORE 3009 Color 3000 Color 3000 Color 3000 Color 3000 Color 3000 Co	And USE Stephen is and Antern Schlörer and Schlörer Marken 2003 2003/41 2003/2003 2003/2003/2003/2003/2003/2003	<b>'D</b> 181 n.sg
39 PA Tet: (65) ENGINEER'S QUANTITY S NO.C-9 85 Join	M. 11. altr Intelexity of the Intelexity of the	AND	<b>'D</b> 181 m.sg
39 PA Tet: (65) ENCINEER'S QUANTITY S NO.C-9 85 Joid Tel : 0	H (Lide Lide Lide Lide Lide Lide Lide Lide	And USE Steppen is and Address of Silver And Steppen and Address of Silver Address o	<b>'D</b> 181 n.sg
39 PA Tet: (65) ENCINEER'S QUANTITY S QUANTITY S NO.C-9 85 Jolc Tel : 0 Tel : 0	H (Lide Lide Lide Lide Lide Lide Lide Lide	And USE Stephen is an Antere All See An Schopfungter M 200704 CC CC CC CC CC CC CC CC CC C	<b>'D</b> 181 n.sg
39 PA Tet: (65) ENGINEER'S QUANTITY S QUANTITY S NO.C-9 85 Jolo Tet : 0 email: PROJECT :	Fit (14) Fit (1	A Contraction of the state of the set of the state of the	<b>'D</b> 181 n.sg
39 PA Te: (65) ENGINEER'S QUANTITY S ROJECT : 0 email: i PROJECT : CADAN	ILLIGHT CONTROL OF CON	A Control of the second	D 81 n.ag
39 PA Tec (es) ENGINEER'S GUANTITY S NO.C-9 85 Joc Tel :: 0 CADAN KOLAI	It identifies and a second sec	A Contraction of the state of the set of the state of the	D 81 n.ag
30 PA Tec (es) ENGINEER'S CULINITY S S Jaile NO.C-9 Tet : 0 Tet : 0 PROJECT :: CADAM KOLAM BBERKJ	It identifies the second secon	A     A	20 2881 10.
30 PA Tec (es) ENGINEER'S CULINITY S S Jaile NO.C-9 Tet : 0 Tet : 0 PROJECT :: CADAM KOLAM BBERKJ	It identifies the second secon	the state of the set of the	20 2881 10.
30 PA Tet (65) ENGINEER'S OUWITTY S OUWITTY S	It identifies the second secon	the state of the set of the	Ъ 181 10.
30 PA Tec (es) ENGINEER'S CULINITY S S Jaile NO.C-9 Tet : 0 Tet : 0 PROJECT :: CADAM KOLAM BBERKJ	It identifies the second secon	the state of the set of the	Ъ 181 10.
	In Light And	the state of the set of the	"D 81 ID.
	In Light And	the state of	D 81 D.
	In Light And	the second	D 81 D.
	In Light And	the second	D 81 D.
	In Light And	the second	D 81 D.
	It takes It tak	A A A A A A A A A A A A A A A A A A A	D 81 D.
	ILLEVATION REPORTED TO THE ILLEVATION OF THE ILL	Control of the state of the set of the state of the	D 81 D.
	ILLEVATION REPORTED TO THE ILLEVATION OF THE ILL	the second	D BAI D. JA SIA. FABRIC

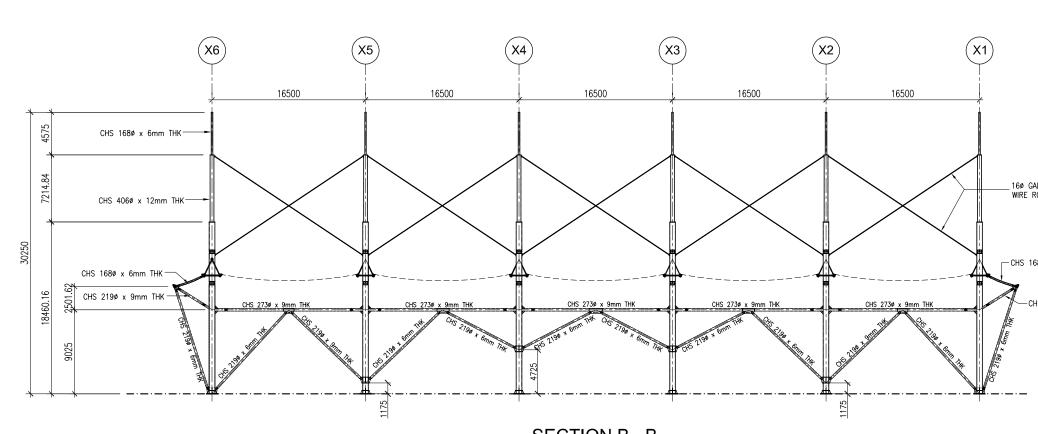
С



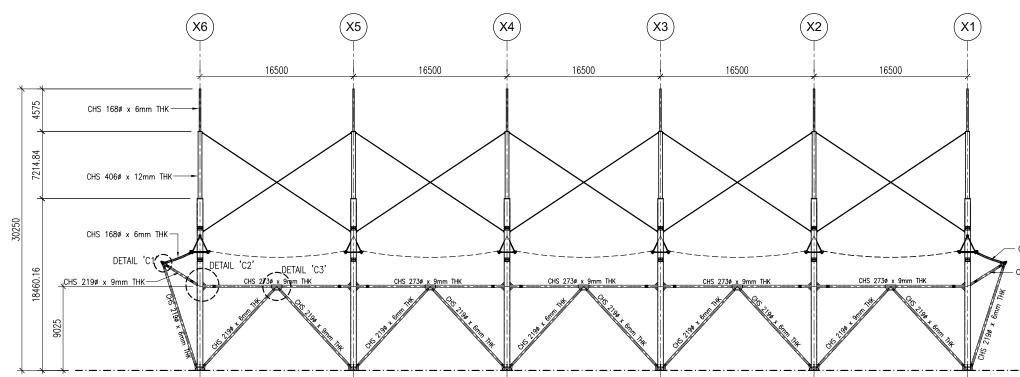
			6
03	31.07.2012	AS-BUILT	
02 01	20.04.2012 12.01.2012	GENERAL GENERAL	
REF	DATE	DESCRIPTION	
OWNER :			
		<b>`</b> )	
/	A.		
Ļ	Majlis Perba	indaran <b>A</b> N	
		RBANDARAN KUANTAN 1, 25100 Kuantan,	
Pahan		kmur, Malaysia.	
	itractor :		
		HATI SDN. BHD.	
	JALAN MA	st. FLOOR, MUIP BUILDING, HKOTA, 25000 KUANTAN , MRUL MAKMUR	
	TEL :609-	-515 2473, FAX : 603-516 2619	
ARCHITECT	r's :		
		& ASSOCIATES ARCHITE SENDIRIAN BERHAD (75	
		B-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.	
	9	Tel: 09-5736430 / 5736372 Fax: 09-	57364
SPECIALIS'	TROOF&C	LADDING CONTRACTOR:	
		TRI-ARCH sdn. bhd.	
a		7-1, JALAN 2/115A, TAMAN PAGAR RUYONO OFF JALAN KUCHAI LAMA,	3
	]	58200 KUALA LUMPUR. TEL : 79812870 FAX : 79818210	
		E-mail : triarch90@yahoo.com.my	
in conju	NCTION WITH:		
	) oe		_
8	SE No 11 Jake	DIABENA CON. DA	D.
9	<b>8</b> No. 11, Jaka A Tel: 803-7847 (Company No:	Indiana Department Managerine Vision 3 Istala U884, Seksyen U8, Buil Jelatong, 40151 Shah Alam, Selangor Dani Etsan, Ma 2021 - Exe Jell 14 (7 2021	aysta. Loom
æ	No. 11, John Tel: 803-7847 (Company No:	COLORED ENA CONLISION teta 034 Seven II, Bal Aldreg 405 Ser Mar, Sarvorbuletser M seven and nangester 200749 wede rewoodces	aysta acom acom
æ	No. 11, Jaka / Tel: 603-7847 (Company No:	etar 1985 Sever 18 aŭ letos 498 Sev 4an Servicio (1955 eta 301 - Fa: 1834 (222 1987 H) eta letos 498 Sev 4an Servicio (1956 H) eta le revestos 1987 H) eta letos 1990 - Sever	חי
	No. 11, Jaka / Tel: 603-7847 (Company No:	etar 1985 Sever 18 aŭ letos 498 Sev 4an Servicio (1955 eta 301 - Fa: 1834 (222 1987 H) eta letos 498 Sev 4an Servicio (1956 H) eta le revestos 1987 H) eta letos 1990 - Sever	חי
<b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b>	No. 11, Jaka / Tel: 603-7847 (Company No:	estat 1934: Selser UB, Ball Jeldon, 2015 Stat Alm, Selvico DordEnser Mal 300 Fin: 401347 222 4057744) estal Final Agenciene 4057744) estal Extension	חי
39 P Tel: (65)	No. 11, Jaka / Tel: 603-7847 (Company No:	etat 1883. Stoper et al. Aldres, 515 Ser An, Stoper Erilderer hi earter and automatication and an anti- earter and automatication and an anti- transference and anti- angle and anti- angle anti- anti- angle anti- anti- angle anti- anti- angle anti- a	חי
39 P Tel: (65)	K. 11, kite / rel: 8827847 (Carpany No: ANDAN R 0 6265 3069 S C&S and	eta USI Sano U Bal Aleg SISSe da Shyrinidada M Sano Shiron (2000) Sano Shiron (2000) Sano Shiron (2000) Sano Shiron (2000) TRANSERVE PTE LT (2000) Sano Shiron (2000) Sano Shiron (2000)	'D 434) 281 n.sg
39 P Tel: (65)	An 11, ker / Tel: 883-764T (Concenty No: Concenty No: Con	tet 1883 Store it all Alles Still an Antrophylicitation in Star 1980 Star 2012 Star 1980 Star 2012 Star 1980 Star 2012 TRANSERVE PTE LT (Ca Reg Tes	'D 434) 281 n.sg
39 P Tel: (65)	KITLANG TERSIST Companyle: ANDAN R 6268 3069 S C&S and S C&S and JU A-7 Jala	eta USI Sano U Bal Aleg SISSe da Shyrinidada M Sano Shiron (2000) Sano Shiron (2000) Sano Shiron (2000) Sano Shiron (2000) TRANSERVE PTE LT (2000) Sano Shiron (2000) Sano Shiron (2000)	'D 434) 281 n.sg
39 P Tel: (65)	RESERVE ANDAN R 6268 3069 'S C&S and JU A-7 Jala Pah	tet 1883. Store at Alex, Still See din Skryffelder M Store at Store at Sto	'D 434) 281 n.sg
39 P Tel: (65)	BSERVE ANDAN R 0 6268 3069 S C&S and JU ADDAN R 1 6268 3069 S C&S and JU A-7 Jula Paha Tel	tet 1883. Sayon ut an Alex, Still See An Shryfferlander M See Alexand See Alexandrow and See Alexandrow Carlos and See Alexandrow and See Alexandrow Carlos and See Alexandrow and See Alexandrow Carlos Alexandrow and See Alexandrow Fac (SS) 626 224 Enail selectrometer Runding Hymn Son. BH 732, Tingket Satu, Kedai LKNP, n Dato's Bohaman, 5200 Kuantan, ang Darul Makmur.	'D 434) 281 n.sg
39 P Tel: (65)	IN THE AREA THE AND	All 1985 Stephen at all Allers, Still See Alls, Stephen at all Allers, Still See Alls, Stephen at all all all all all all all all all	'D 434) 281 n.sg
39 P Tel: (65)	BSERVE ANDAN R 0 6268 3069 S C&S and JU ADDAN R 1 6268 3069 S C&S and JU A-7 Jula Paha Tel	tet 1883. Sayon ut an Alex, Still See An Shryfferlander M See Alexand See Alexandrow and See Alexandrow Carlos and See Alexandrow and See Alexandrow Carlos and See Alexandrow and See Alexandrow Carlos Alexandrow and See Alexandrow Fac (SS) 626 224 Enail selectrometer Runding Hymn Son. BH 732, Tingket Satu, Kedai LKNP, n Dato's Bohaman, 5200 Kuantan, ang Darul Makmur.	'D 434) 281 n.sg
	And Date of the second	the UBL Status of Mark Still See div Status diversed and Mark Still See diversed and Mark Still See diversed and Mark Still See diversed and Mark Status din Are Statu	'D 434) 281 n.sg
39 P Tel: (65) ENGINEER QUANTITY QUANTITY NO.C- 85 Ju	And Date of the second	An USA Same of an Alex, Shifter an School and an Alex School and Alex School Alex School Alex School Alex School Alex School and Alex School Alex Scho	'D 434) 281 n.sg
39 P Tel: (65) ENGINEER QUANTITY QUANTITY NO.C- 85 Jo Tel : 1	Autore and a set of the set of th	Att UBA Stature UI and Nature Still State Alls Stature UI and Nature Still State All State Still State All State Still State All State Sta	'D 434) 281 n.sg
39 P Tet: (65) Tet: (65) ENGINEER QUANTITY NO.C- S5 Ja S5 Ja S5 Ja	An adde Tel: Bisser VE Correny VE Corre	Att UBA Stature UI and Nature Still State Alls Stature UI and Nature Still State All State Still State All State Still State All State Sta	'D 434) 281 n.sg
39 P Tel: (65) ENGINEER QUANTITY NO.C- S5 Jo Tel : 1 email: PROJECT	Annaka A	All VARANCE AND A MARK AND AND A MARK AND A	'D 434) 281 n.sg
39 P Tel: (65) ENGINEER QUANTITY NO.C- S5 Jo Tel : 1 email: PROJECT CADA	An taken Teleboxic Intervention Intervent	Att 188 Statut at 189 Statut a	D (381) n.sg
39 P Tet (65) ENGINEER QUANTITY NO.C. S Jo DU.A. Tet :: email: PROJECT CADAN KOLA	An rate Television Intervent	All VALUE AND	D (381) n.sg
CUANTITY Free (65) COUNTITY COUNTITY COUNTITY COUNTITY PROJECT CADAA KOLA BERK	An advised to the second secon	All VIB Manue II and Marke Shiftse An Shape Inder M 20078 20078 TRANSERVE PTE LT Da Tage The WITTER CAD, JURONG, SINGAPORE 6092 Face (63) CEGE 232 REDUINE HYNH SDN. BH 732, Tingkat Satu, Kedai LKNP, n Dato' Beharman, 25200 Kuantan, ang Darul Makuru. 109–566 3031 Faks : 09–560 1182 II. Menara Uncang Emas, w, 55200 Kual Lumpur 85 Fax : 03–92008276 (391855–V) 8a.com.my website: pendila.com.my MERNAIK TARAF ANG SERTA KERJA-KER DI WISMA BELIA,	D (18) 181 10.
CUANTITY Free (65) COUNTITY COUNTITY COUNTITY COUNTITY PROJECT CADAA KOLA BERK	An advised to the second secon	All VALUE AND	D (18) 181 10.
CUANTITY Free (65) COUNTITY COUNTITY COUNTITY COUNTITY PROJECT CADAA KOLA BERK	An advised to the second secon	All VALUE AND	D (18) 181 10.
39 PT Tet (65) ENGINEER AUANTITY NO.C. NO.C. NO.C. NO.C. Tet :: email: email: email: ENGINEER FROJECT CADAN BERKK INDEF	An advised to the second secon	All VALUE AND	D (18) 181 10.
CUANTITY Free (65) COUNTITY COUNTITY COUNTITY COUNTITY PROJECT CADAA KOLA BERK	An advised to the second secon	All VALUE AND	D (18) 181 10.
	Annaka Intervention Interven	All VALUE AND	<sup>1</sup> D <sup>1,30</sup> 1D.
	Annoan R Survey As Annoan R Survey As Correspondent Survey As Survey As	Att 188 Statut of Bar Alex, Still See An Short Halfer M 20078 20078 2007 2007 2007 2007 2007 200	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>
	Annoan R Survey As Annoan R Survey As Correspondent Survey As Survey As	the UNIX Status of Marked Still Status of Marked Still Status of Marked Still Status Still Status of Marked	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>
	Annoan R Survey As Annoan R Survey As Correspondent Survey As Survey As	the UNIX Status of Marked Still Status of Marked Still Status of Marked Still Status Still Status of Marked	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>
	Annoan R Survey As Annoan R Survey As Correspondent Survey As Survey As	the UNIX Status of Marked Still Status of Marked Still Status of Marked Still Status Still Status of Marked	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>
	Annoan R Survey be: Correspondence Correspo	the value of the value of the set of the set of the value of the	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>
	Annoan R Annoan R Second Se	A Constructive framework of the standard of a constructive framework of the standard of the s	D AND AND AND AND AND AND AND AN
	Annoan R Annoan R Second Se	the last server at a large shiftser an shortender at a server	<sup>1</sup> D <sup>1</sup> 81 <sup>1</sup>

C









# SECTION C - C



		olam Renang
	NOTE :	65
	03 31.07.2012 02 20.04.2012	AS-BUILT GENERAL
	01 12.01.2012	GENERAL
	REF DATE	DESCRIPTION
	OWNER :	
		)
		ran
	KUANTA	N
D	MAJLIS PER	BANDARAN KUANTAN
	Jalan Tanah Putih, 2 Pahang Darul Makmi	
		666 FAKS : 5130644
	MAIN CONTRACTOR :	
		IATI SDN. BHD.
нк	JALAN MAHK	FLOOR, MUIP BUILDING, OTA, 25000 KUANTAN ,
	PAHANG DAR TEL :609-5	UL MAKMUR 15 2473, FAX : 603-516 2619
n THK		
r (r)dX	ARCHITECT'S :	
		ASSOCIATES ARCHITECTS
		ENDIRIAN BERHAD (755269-P) 26 Thokat Satu Jalan (M3/10
		-26, Tingkat Satu, Jalan IM3/10 andar Indera Mahkota 5200 Kuantan Pahang Darul Makmur.
		el: 09-5736430 / 5736372 Fax: 09-5736443
	specialist roof & clad	DING CONTRACTOR:
		RI-ARCH sdn. bhd.
		, JALAN 2/115A, TAMAN PAGAR RUYONG F JALAN KUCHAI LAMA, 200 KUALA LUMPUR.
	58: TEL E-r	200 KUALA LUMPUR. : 79812870 FAX : 79818210 na1 : triarch90@yahoo.com.my
	IN CONJUNCTION WITH:	
		NABENA COL PHD.
	No. 11., Jaker Astalia Tel: 600-7147 3333 Al Cremanic March 2005	U884, Seksyen U8, Buit Jekitorg, 40191 Shari Alan, Silançor Danil Etxan, Mahyaka Fas: 463:1447 2222 e-endil: engli Gyataka com 1441 webste : www.sedabiena.com
	(Company No: 0656	1241) webste : www.sedabena.com &
		TRANSERVE PTE LTD (ca. Rep. No: 1977024330)
	39 PANDAN ROA	(c. Re, No: 197703430) D, JURONG, SINGAPORE 609281 x: (65) 6266 2324 Email: sales@transervet.com.sg
	Tel: (65) 6268 3069 Fa	κ: (οວ) 6266 2324 Email: sales@transervet.com.sg
	ENGINEER'S C&S and M&	£
		- Unding Hyh SDN. BHD.
	A-773	2, Tingkat Satu, Kedai LKNP,
	Jalan i	)ata' Bahaman, 25200 Kuantan, Darul Makmur.
		9–566 3031 Faks : 09–560 1182
	Tel : C	
	quantity surveyor :	<u>0</u>
	quantity surveyor :	ENDÍTA
	QUANTITY SURVEYOR :	ENDITA
	QUANTITY SURVEYOR :	, Menara Uncang Emas, 55200 Kuala Lumpur
	QUANTITY SURVEYOR : 	, Menara Uncang Emas, 55200 Kuala Lumpur
НК	QUANTITY SURVEYOR : 	, Menara Uncang Emas, 55200 Kuala Lumpur Fax : 03-92008276 (391855-V)
	QUMITY SURFOR : Definition of the second se	, Menara Uncang Emas, 55200 Kuala Lumpur Fax: 0.3-2008276 (391855-V) om.my website: pendita.com.my
	QUMITY SURFOR : 	, Menara Uncang Emas, 55200 Kuala Lumpur Fax: 0.3-2008276 (391855-V) om.my website: pendita.com.my
	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 Joint Lover Yew, Tel : 03-92008268 emoit: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKATAN DI	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
(	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 Joint Lover Yew, Tel : 03-92008268 emoit: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKATAN DI	Menara Uncang Emas, 55200 Kuda Lumpur Fax: 0.3-9208276 (391855-V) om.my website: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA
	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 Joint Lover Yew, Tel : 03-92008268 emoit: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKATAN DI	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 Joint Lover Yew, Tel : 03-92008268 emoit: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKATAN DI	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 Joint Lover Yew, Tel : 03-92008268 emoit: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKATAN DI	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : WO-C-9-9, Level 11 85 John Lover Yee, Tel : 03-92008268 erroli: into@pendita.c PROJECT : CADANGAN MI KOLAM RENAU BERKAITAN DO INDERA MAHK	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUMITIY SURVEYOR : 	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : WO.C-9-9, Level 11 85 Jalon Loke Tex, Tel : 03-9200228 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK 11TTLE : SECTION B-B	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
тнк тнк	QUANTITY SURVEYOR : WO.C-9-9, Level 11 85 Jalon Loke Tex, Tel : 03-9200228 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK 11TTLE : SECTION B-B	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : NO.C-9-9, Level 11 85 Jalon Loke Yew, Tel : 0-32003268 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK TITLE : SECTION B-B SECTION C-C	Menaro Uncang Ernas, 55200 Kulo Lumpur Fox : 03-92008276 (391855-v) om.my website: pendita.com.my ENAIK TARAF KG SERTA KERJA-KERJA WISMA BELIA, OTA, KUANTAN, MALAYSIA.
	QUANTITY SURVEYOR : WO.C-9-9, Level 11 85 Jalon Loke Tex, Tel : 03-9200228 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK 11TTLE : SECTION B-B	Merare Uncang Emas, 55200 Kulo Lumpur Fax : 03-92008276 (391855-V) om.my websile: pendita.com.my ENAIK TARAF IG SERTA KERJA-KERJA WISMA BELIA,
	QUANTITY SURVEYOR : NO.C-9-9, Level 11 85 Jalon Loke Yew, Tel : 0-32003268 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK TITLE : SECTION B-B SECTION C-C	Menaro Uncang Ernas, 55200 Kulo Lumpur Fox : 03-92008276 (391855-v) om.my website: pendita.com.my ENAIK TARAF KG SERTA KERJA-KERJA WISMA BELIA, OTA, KUANTAN, MALAYSIA.
	QUANTITY SURVEYOR : WO C-9-9, Level 11 85 Jalon Loke Yew, Tel : 03-2000288 email: info@pendita.c PROJECT : CADANGAN MI KOLAM RENAI BERKAITAN DI INDERA MAHK ITTLE : SECTION B-B SECTION C-C	DRAWN :
	QUANTITY SURVEYOR : NO.C-9-9, Level 11 85.3000 Loker Yee, Tel : 03-92008268 emoil: info@pendita. PROJECT : CADANGAN MI KOLAM RENAU BERKAITAN DO INDERA MAHK TITLE : SECTION B-B SECTION B-B SECTION C-C DATE : 29.12.2011 SCALE : 1 : 400 DRAWING NO. :	Merrare Uncang Ernas,         Sizolo Kuloi Lumpur         Fax: 0.3-92008276 (391855-V)         om.my       websile: pendita.com.my         ENAIK TARAF         KG SERTA KERJA-KERJA         WISMA BELIA,         OTA, KUANTAN. MALAYSIA.         DRAIN :         CHECKED :         REVISION
	QUANTITY SURVEYOR :	Merrare Uncang Ernas,         Sizolo Kuloi Lumpur         Fax: 0.3-92008276 (391855-V)         om.my       websile: pendita.com.my         ENAIK TARAF         KG SERTA KERJA-KERJA         WISMA BELIA,         OTA, KUANTAN. MALAYSIA.         DRAIN :         CHECKED :         REVISION

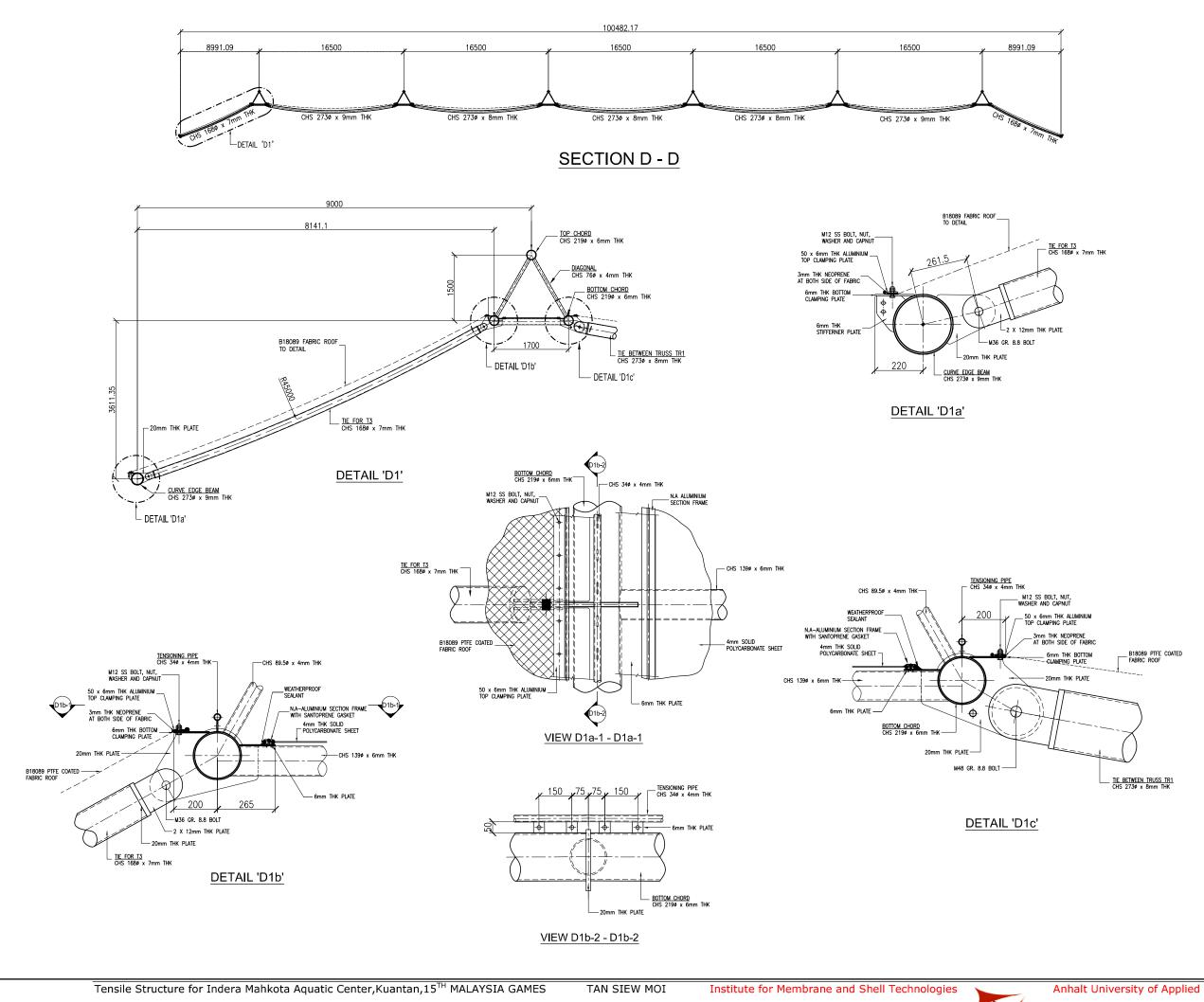
\_ 16ø GALVANIZED WIRE ROPE

CHS 168Ø x 6mm THK

-CHS 219ø x 9mm THK

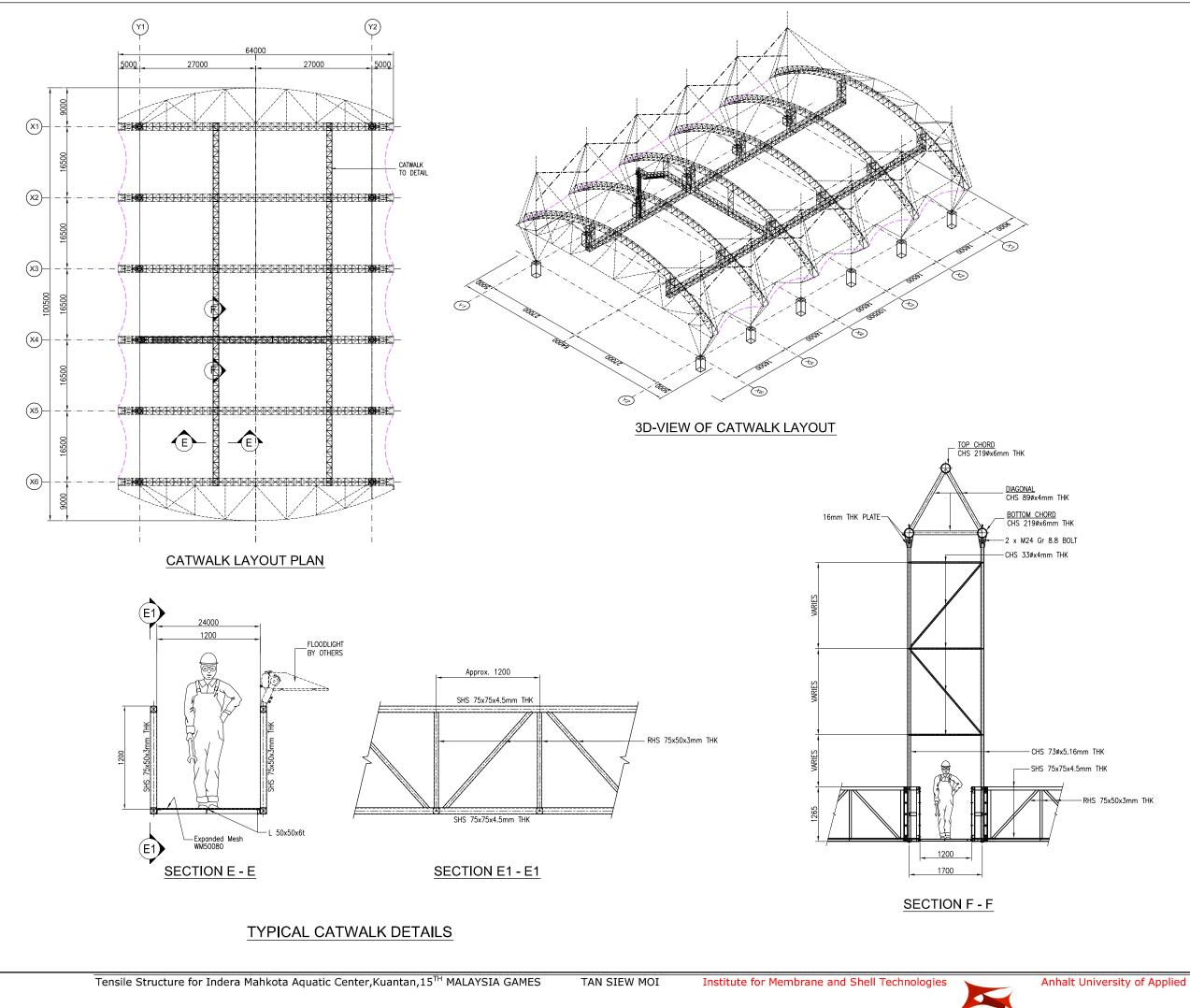
- CHS 168ø x 6mm THK

– CHS 219ø x 9mm THK



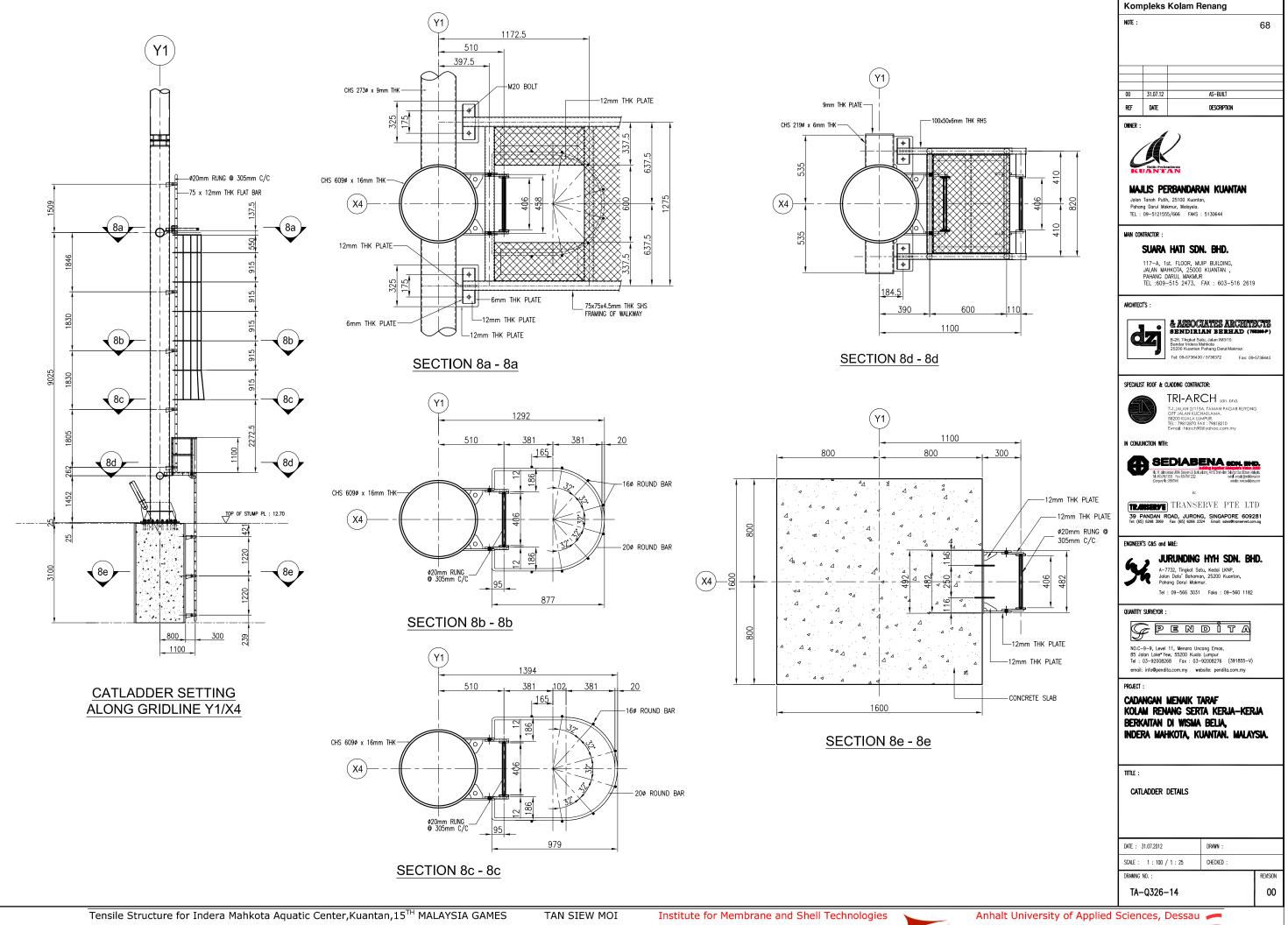


NOTE :	-	Kolam Renang 66
07	71.07.0010	ас рішт
03 02	31.07.2012 20.04.2012	AS-BUILT GENERAL
01	12.01.2012	GENERAL
ref	DATE	DESCRIPTION
OWNER :		
4	Manilis Pertin	uduran
		RBANDARAN KUANTAN , 25100 Kuantan,
Paha		mur, Malaysia.
MAIN CO	NTRACTOR :	
	SUARA	hati son. Bhd.
		t. Floor, Muip Building,
	JALAN MAH	IKOTA, 25000 KUANTAN ,
	TEL :609-	ARUL MAKMUR 515 2473, FAX : 603-516 2619
ARCHITEC	TTS :	
		& ASSOCIATES ARCHITECTS SENDIRIAN BERHAD (788289-7) B-26, Thgkat Satu, Jalan IM3/10
		B-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.
L	-	Tel: 09-5736430 / 5736372 Fax: 09-5736443
0000		
SPECIALI		ADDING CONTRACTOR:
ß		TRI-ARCH sdn. bhd. 7-1. Jalan 2/115a, taman Pagar Ruyong
		7-1, JALAN 2/115A, TAMAN PAGAR RUYONG OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR.
4		TEL : 79812870 FAX : 79818210 E-mail : triarch90@yahoo.com.my
in conji	unction with:	
	<b>SE</b>	
Ę	No. 11, Jake A	DIABENA CON. BHD. Sala 1894. Seager Lik, Balt, Halory, 4715 Stat Mar, Salarger David Bart, Mahyak.
Ð	No. 11, Jalan A Tel: 403-78473 (Company No:	sala 1994, Selayen IB, Buri Jelliong, Artisi Salat Alam, Salaroo Dan Elisan Malayak. 1331 - Far: 633-7447 2222 - e-rail: engal rigitadona.com 195679-41 - widale: +www.selablea.com
E	No. 11, Jalan A Tel : 003-7847 (Company No:	saar 1994, Seesen UE Bart Velang, 40151 Sati Kan Sakarat Druben. Malyak 1311 - Far: HST4VT 2022 e-talf insubrigitablana.com 18267749 witche: www.sakkena.com
	No. 11, Jalan A Tel : 003/34/1 (Company No:	Instanting Store in Start Store And
<b>1</b> 39 Tel: (65	No. 11, Jalan A Tel : 003/34/1 (Company No:	saar 1994, Seesen UE Bart Velang, 40151 Sati Kan Sakarat Druben. Malyak 1311 - Far: HST4VT 2022 e-talf insubrigitablana.com 18267749 witche: www.sakkena.com
	H, 11, Han A Td : 803-3477 (Corpany He Corpany He Corpa	An URA Sour II. SALANG SUB AN Shrip hards have SUB 29 100 201 201 201 201 201 201 201 201 201
	Hitta Handright Hitta Hitta Hi	And URAN Storen in A stations of the Start in March Index Advances of the Start Index A
	N. 11, Mar A Tel: 6023407 (Corpany No: Corpany No: Co	AND A STATE AND A
	No. 11. Jain A. Horsen VIE Researcher PANDAN R. PANDAN R. S C&S and JU Julian A77 Julian	And URAN Storen in A stations of the Start in March Index Advances of the Start Index A
	North Jahr Andrew States (Corport House Stat	AND
	National States and St	An URA Source it as a Leans of Sour in Sharp in Libra Mark Mark Source it as a Leans of Sour in Sharp in Libra Mark Mark Source it as a Leans of Source in Sharp in Libra DAD, JURONG, SINCADOR E GO2261 Face (16) 6266 2324 Endt Source in Source
	R: reader H:Board H:Board Margay H: AnDAN R: PANDAN R: SCAS and SCAS and JU A-7 Jolan Paho Tel : SURVEYOR :	AND
	National States and St	An URA Source it as a Leans of Sour in Sharp in Libra Mark Mark Source it as a Leans of Sour in Sharp in Libra Mark Mark Source it as a Leans of Source in Sharp in Libra DAD, JURONG, SINCADOR E GO2261 Face (16) 6266 2324 Endt Source in Source
	An Table Mit Cost Rereavie: Carpevie	AND
	In table to the table to the table to the table to the table	AND
	INSERVE ANDAN R ANDAN R AND	AND
	In taken In taken	AND
	INSERVE ALL SALE ALL SALE ANDAN R PANDAN R	Barbanan, 2520     Barbanan
	INSERVE ANDAN R ANDAN R AND	Bernark Tarafy Bernark tarafy Bernark States Bernark States B
	AnDAN R SUBJECT SUB	A Constraints of the second s
	AnDAN R SUBJECT SUB	Bernark Tarafy Bernark tarafy Bernark States Bernark States B
	AnDAN R SUBJECT SUB	A Constraints of the second s
	AnDAN R SUBJECT SUB	A Constraints of the second s
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	ALL CONTRACTOR OF CONTRACTOR O
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	A Constraints of the second s
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	ALL CONTRACTOR OF CONTRACTOR O
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	ALL CONTRACTOR OF CONTRACTOR O
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	A TRANSERVE PTE LID A A TRANSERVE PTE LID A A A TRANSERVE PTE LID A A A A A A A A A A A A A A A A A A A
	AnDAN R An Electronic Action An Electronic Action AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R AnDAN R And And And And And And And And	ALL CONTRACTOR OF CONTRACTOR O
	In addet In addet	A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSERVE AGAIL  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSER
	the set of the se	A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics with several detection  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSERVE AGAIL  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSERVE PTE LID Logistics  A TRANSERVE AGAIL  A TRANSER
	the set of the se	Bit States         Sta
	INSERVE ANDAN R ANDAN R AND	Bit States         Sta
	In adder In adder	Bit States         Sta

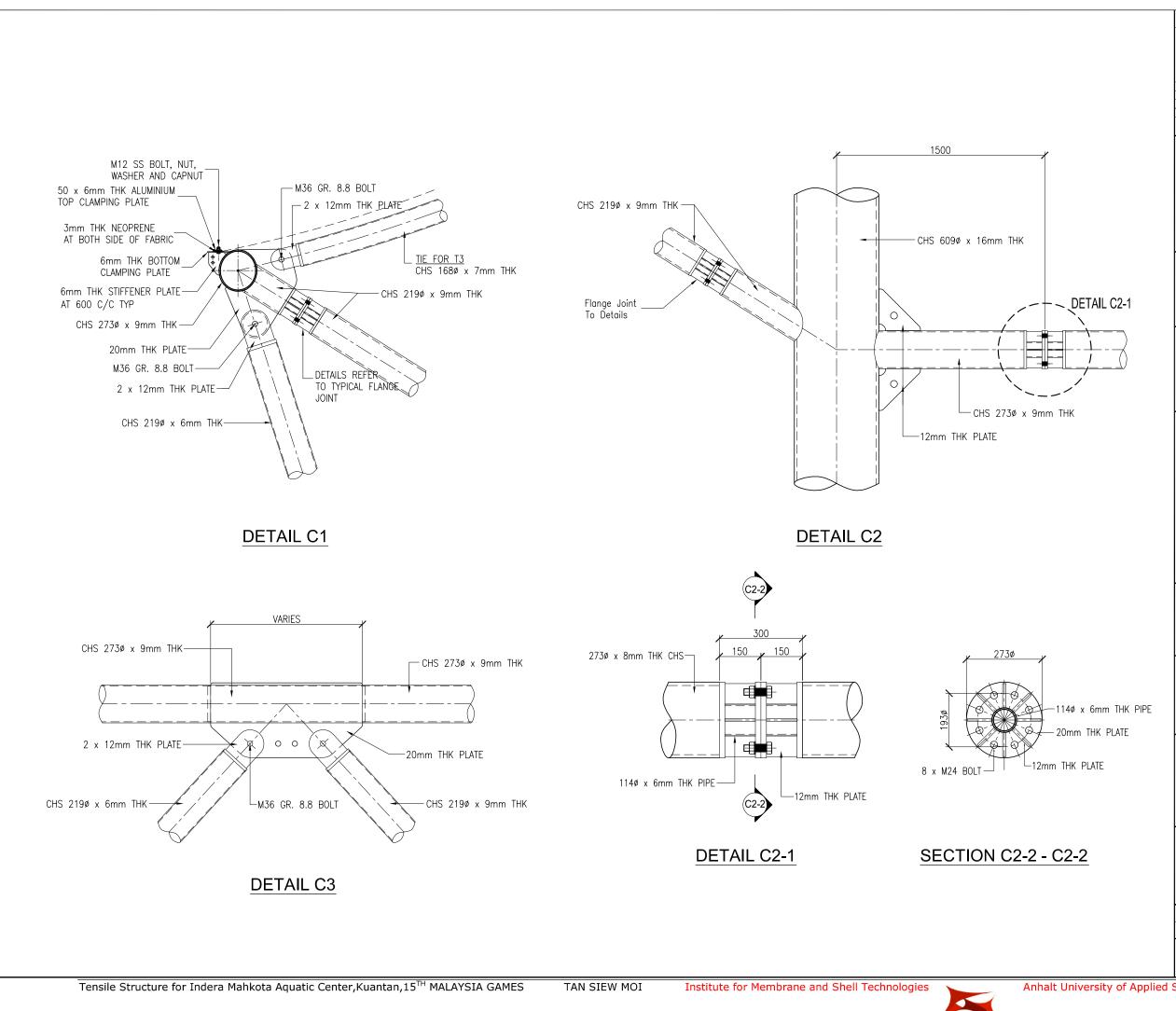


Kon	npleks	Kolam Renang	
NOTE :			67
03	31.07.2012	AS-BUILT General	
02 01	20.04.2012	GENERAL	
REF	DATE	DESCRIPTION	
OWNER :			
	Á	)	
	Majlis Perba	ndaran AN	
		rbandaran kuantan	
Jalar	Tanah Putik	n, 25100 Kuantan,	
	ng Darul Mal 09-512155	kmur, Malaysia. 5/666 FAKS : 5130644	
MAIN CO	NTRACTOR :		
		HATI SDN. BHD.	
	JALAN MA	st. FLOOR, MUIP BUILDING, HKOTA, 25000 KUANTAN , MRUL MAKMUR	
	TEL :609-	ARUL MAKMUR -515 2473, FAX : 603-516 2619	9
ARCHITEC	TS .		
		& ASSOCIATES ARCHIT SENDIRIAN BERHAD (7	
	77	B-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.	
	9		-5736443
Speciali		LADDING CONTRACTOR:	
ß		TRI-ARCH sdn. bhd.	
	)	7-1, JALAN 2/115A, TAMAN PAGAR RUYON OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR.	G
		TEL : 79812870 FAX : 79818210 E-mail : triarch90@yahoo.com.my	
in conj	unction with	:	
	) se		D.
	No. 11, Jalar / Tel : 803-7647	Luking together Mislengthan Vielan stabia U814, Seksyen U8, Bult Jelating, 4015) Shah Alam, Salangor Daral Ethan, Mi 4033 Fax: 603-7447 2222 e-Hall: angult gilosobati 1856/7441 webate: www.sedate	daysta ta.com
	(contrar) in	800000000 modelet modelet	
TR/	IISER/E	TRANSERVE PTE LT	D
<b>39</b> Tel: (6	PANDAN R 5) 6268 3069	OAD, JURONG, SINGAPORE 6092 Fax: (65) 6266 2324 Email: sales@transervet.co	2 <b>81</b> <sup>m.sg</sup>
ENGINEEI	R'S C&S and		
6		RUNDING HYH SDN. BH	ID.
7	Jala Pah	732, Tingkat Satu, Kedai LKNP, n Dato' Bahaman, 25200 Kuantan, ang Darul Makmur.	
-	Tel	: 09-566 3031 Faks : 09-560 1182	
QUANTIT	surveyor :		
	2 P	ENDÍTA	
	ኇዸ		
85 J	alan Loke•Ye	11, Menara Uncang Emas, w, 55200 Kuala Lumpur	
	03-920082 i: info@pendi		
PROJECT	:		
		MENAIK TARAF	
		ang serta kerja-ker	<b>JA</b>
		di Wisma Belia,	
INDE	ra mał	ikota, kuantan. Malan	<b>SIA</b> .
TITLE :			
	WAL 12		
	WALK LA	YOUT & SECTION	
DATE -	29.12.2011	DRAWN :	
SCALE :			
DRAWING		I. JU UREUNEU :	REVISION
		13	
	-Q326-	· IJ	03
Scien	ices, I	Dessau 🛹	

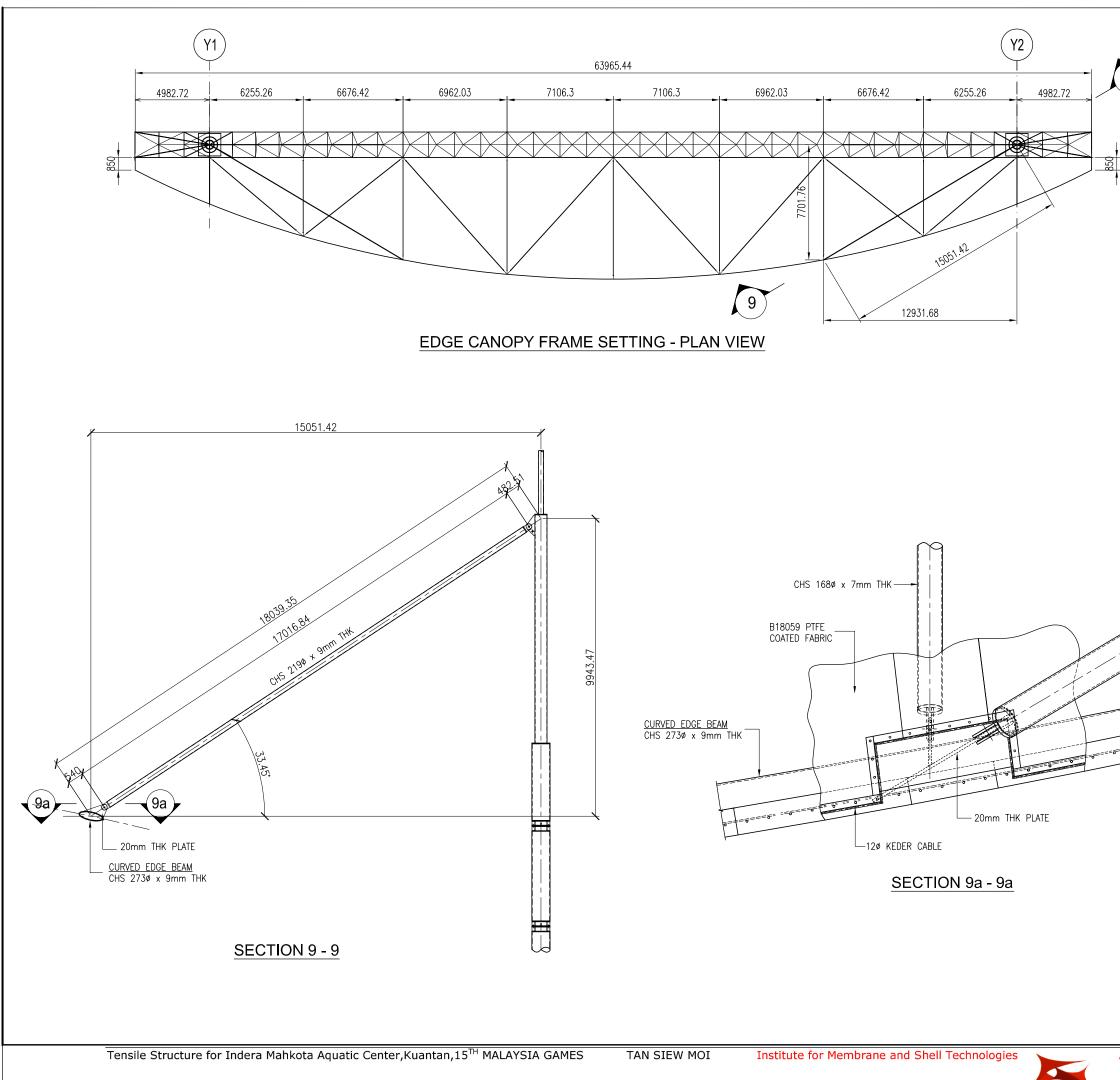
C



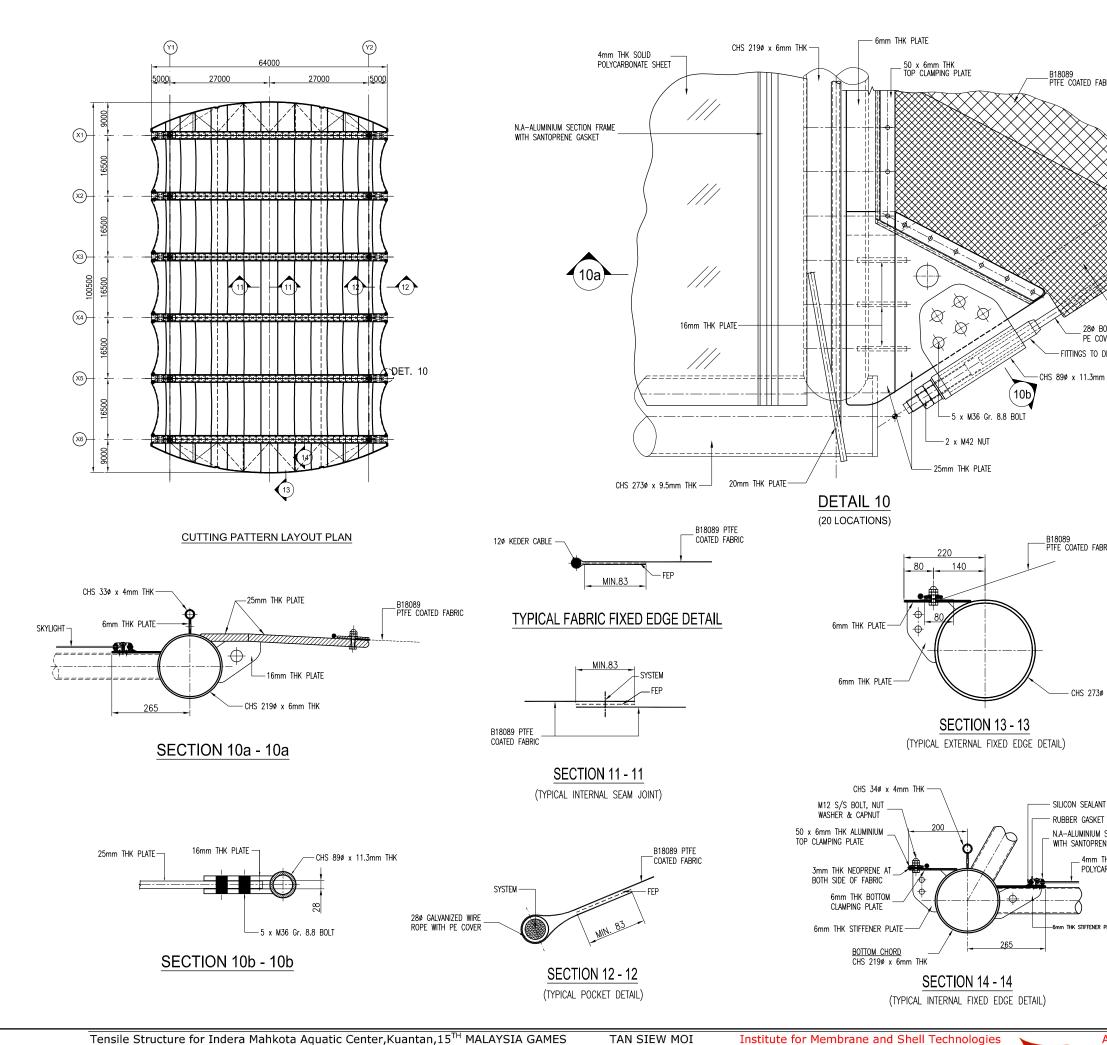




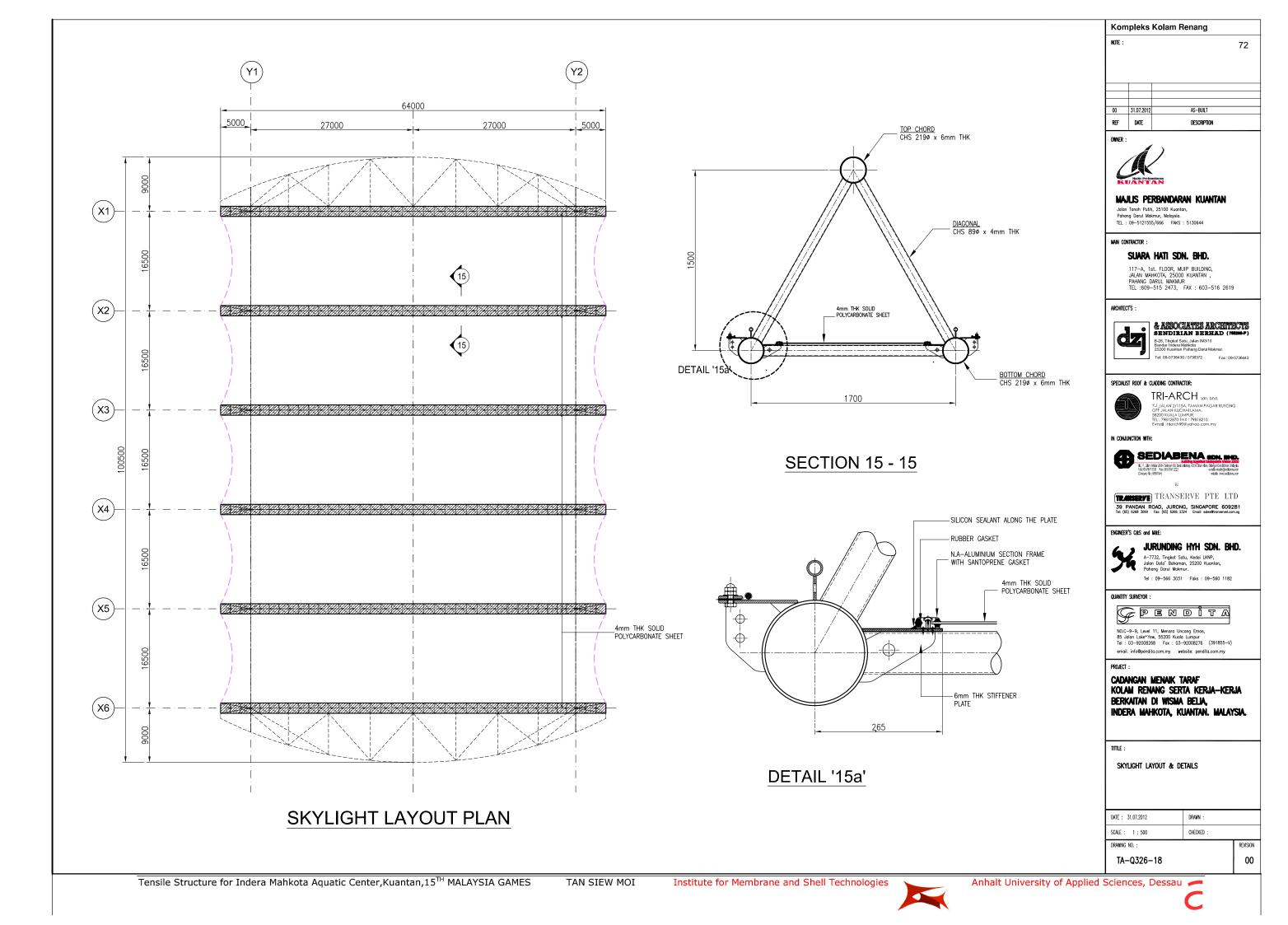
Kom	pleks	Kolam F	lenang	
NOTE :				69
00	31.07.2012		AS-BUILT	
ref	DATE		DESCRIPTION	
OWNER :		<pre>// .</pre>		
	Â	)		
	X			
KI	Majlis Perba			
			an kuantan	
Pahan	ig Darul Mal	n, 25100 Kuanta kmur, Malaysia.		
TEL :	09-512155	5/666 FAKS	: 5130644	
MAIN CON	TRACTOR :			
:	suara	hati sdi	N. BHD.	
	117-A, 1: JALAN MA	st. FLOOR, MU HKOTA, 25000	JIP BUILDING, KUANTAN	
	PAHANG D TEL :609-	DARUL MAKMUI	FAX : 603-516 2619	
ARCHITEC	r's :			
			IATES ARCHITI an berhad (74	
	4		<b>AN BERHAD (7</b> itu, Jalan 1M3/10 tahkota Pahang Darul Makmur.	
	J	25200 Kuantan Tel: 09-573643		-5736443
SPECIALIS	troof & C	LADDING CONTRAC	TOR:	
A			CH sdn. bhd.	
	S	58200 KUALA LU	A, TAMAN PAGAR RUYON HAI LAMA, MPUR.	3
ų	,	TEL: 79812870 F/	X : 79818210 @yahoo.com.my	
in conju	NCTION WITH	:		
А	SE		ENA adm. am	<b>n</b> .
	No. 11, John J Tel: 603-7047	Astaka USIB4, Seksyen UB, Bukt . 3333 Fax: 603-7647 2222	ektorg, 40150 Shah Alam, Selangor Danil Ersan, Ma e-rail: engulny@setlaber wetsila : www.setlaber	aysta. a.com
	foor deal and	н., &	intered , which could be	a2011
TR/	ISERVE	TRANSE		
39 P Tel: (65)	ANDAN R 6268 3069	OAD, JURON Fax: (65) 6266 23	G, SINGAPORE 6092 24 Email: sales@transervet.co	281 <sup>m.sg</sup>
-				
ENGINEER	'S C&S and			
6	A-7	732. Tinakat Sa	<b>HYH SDN. BH</b> tu, Kedai LKNP,	IV.
~	Jala Pah	n Dato' Bahama ang Darul Makm	n, 25200 Kuantan, ur.	
	Tel	: 09-566 3031	Faks : 09-560 1182	
QUANTITY	surveyor :			
C	è P	en	DÎTA	
	-9 Lavel	11 Manara Ila	rana Emar	
85 Ja	-9–9, Level Ian Loke Ye 03–9200821	11, Menara Un ew, 55200 Kuala 68 Fax : 03-	Lumpur	
	info@pendi		bsite: pendita.com.my	
PROJECT	:			
		MENAIK T		
		ang ser Di Wisma	TA KERJA-KER	JA
			JANTAN, MALAY	ISIA.
	-	•		
TITTLE :				
DET/	NLS			
D/	74 07 7		001001	
	31.07.2012		DRAWN :	
SCALE :	1:25		CHECKED :	
DRAWING				REVISION
TA-	Q326-	-15		00
Scien	ces. I	Dessau	-	
. croit	, 1			



	Kompleks Kolam Renang
	NOTE : 70
~	
9	
	00 31.07.2012 AS-BUILT
	REF DATE DESCRIPTION
	OWNER : WINDER PERMANANAN WAALUS PERBANDARAN KUANTAN Jalan Tanah Putih, 25100 Kuantan, Pahang Darul Makmur, Maloysia.
	TEL : 09-5121555/666 FAKS : 5130644
	MAIN CONTRACTOR :
	SUARA HATI SDN. BHD. 117-A, 1st. FLOOR, MUIP BUILDING, JALAN MAHKOTA, 25000 KUANTAN , PAHANG DARUL MAKMUR TEL :609-515 2473, FAX : 603-516 2619
	ARCHIECT'S : & ASSOCIATES ARCENTECTS SENDICAL AND BERLAD (19828-P) Description Mathematical Description Mathematical Description Dearl Mathematical Tet: 09-5736430 / 5736372 Fax: 09-5738443
	SPECIALIST ROOF & CLADDING CONTINCTOR: TRI-ARCH sdn.bnd. 7.17.JALAN 27/15A, TAMAH PAGAR RUYONG 7.17.JALAN 21/15A, TAMAH PAGAR RUYONG
<u>MAST_FRONTSTAY</u> CHS_219ø_x_9mm_THK	N CONJUCTION WITH: SEDEABEENA cont. articl. It that deal USE date of 3.4 Along 45% Se Mr. Sing 2.4 Bits that the SW1000 Sectors 2004 Manage 45% Se Mr. Sing 2.4 Bits that the SW1000 Sectors 2004 Manage 45% Se Mr. Sing 2.4 Bits that the SW1000 Sectors 2004 Manage 45% Se Mr. Sing 2.4 Bits that the SW1000 Sectors 2004 Manage 45% Se Mr. Sing 2.4 Bits that the SW1000 Sectors 2004 Manage 45% Sectors 2004 Manage
	39 PANDAN ROAD, JURONG, SINGAPORE 609281 Tet: (65) 6266 3069 Fac: (65) 6266 2324 Email: sales@transervet.com.sg
	ENGINEER'S CatS and Mate: SSA JURUNDING HYH SDN. BHD. A-7732, Tingkat Satu, Kedai LKNP, Jalan Data' Bahaman, 25200 Kuantan, Pahang Darul Wakmur. Tel : 09–566 3031 Faks : 09–560 1182
	quantity surveyor :
	C PENDITA
=======================================	N0.C-9-9, Level 11, Menaro Uncang Ernos, 85 Jolan Loker Yew, 55200 Kualo Lumpur Tel: 03-92008268 Fax: 03-92008276 (391855-V) email: info@pendita.com.rny vebsite: pendita.com.rny
6mm THK TOP CLAMPING PLATE	project : Cadangan menaik taraf Kolam renang serta kerja-kerja Berkaitan di Wisma Belia, Indera Mahkota, kuantan. Malaysia.
	TITLE : EDGE CANOPY FRAME SETTING & DETAILS
	DATE : 31.07.2012 DRAWN :
	SCALE : 1 : 250 CHECKED :
	JOHLE . T. 200 OHLONED .
	DRAWING NO. : REVISIO



	Korr	pleks	Kolam Renang	
	NOTE :			71
	00	12 01 2012	AC. DINIT	
	REF	12.01.2012 DATE	AS-BUILT Description	
	OWNER :			
$\geq$			)	
$\sim$		A		
$\times$	K	Majlis Peris	andaran A N	
	MA	ilis pe	rbandaran kuantai	١
			n, 25100 Kuantan, kmur, Malaysia.	
	TEL :	09-512155	5/666 FAKS : 5130644	
	MAIN CO	NTRACTOR :		
10a		SUARA	hati SDN. Bhd.	
DOUBLE LAYERED		JALAN MA	st. FLOOR, MUIP BUILDING, HKOTA, 25000 KUANTAN ,	
CABLE WITH			DARUL MAKMUR -515 2473, FAX : 603-516	2619
UNDLE WIIT	ARCHITEC	T'S :		
			& ASSOCIATES ARCE	ITECTS
			SENDIRIAN BERHAD B-26 Thokat Satu Jalan M3/10	(755289-P)
			Bandar Indera Mahkota 25200 Kuantan Pahang Darul Makmur.	x: 09-5736443
	SPECIALIS	ST ROOF & C	LADDING CONTRACTOR:	
	G		TRI-ARCH sdn. bhd.	IYONG
		Y	7-1, JALAN 2/115A, TAMAN PAGAR RL OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR. TEL : 79812870 FAX : 79818210	
	IN CON1		E-mail : triarch90@yahoo.com.my	
	IN CON	JNCTION WITH		
	l e		EDIABENA con. Atala URA, Selayer UR, Bull, Halong, 4015 Shah Alan, Salancer Davi 3337 Fac: 603-7447 2222 enail: engaly	Fisar Malaysia
		(Company No	333 Fail (0.544) 2222 e-fail ( 1908) (0.55734) website: w/	ĝsedabena.com visedabena.com
	TRA	<b>IISERV</b> E	TRANSERVE PTE	LTD
	39 F Tel: (65	PANDAN R	OAD, JURONG, SINGAPORE ( Fax: (65) 6266 2324 Email: soles@transer	509281 rvet.com.sg
	ENGINEER	'S C&S and	M&F:	
			irunding hyh son.	BHD.
	9	A-7 Jala	732, Tingkat Satu, Kedai LKNP, n Dato' Bahaman, 25200 Kuantan,	
		Pah	ang Darul Makmur. : 09–566 3031 Faks : 09–560	1182
5mm THK		SURVEYOR :		
			•	
				7
	85 Je	-9-9, Level alan Loke Ye 03-920082	11, Menara Uncang Emas, w, 55200 Kuala Lumpur 68 Fax : 03-92008276 (39185)	5-V)
			ta.com.my website: pendita.com.m	
	PROJECT			
NG THE PLATE			menaik taraf Ang serta kerja—1	(FR.IA
	BERK	KAITAN	di wisma Belia,	
n Frame Sket	INDE	ra mał	ikota, kuantan. Ma	LAYSIA.
LID				
NTE SHEET	TITLE :			
	сл	ting pat	itern layout & details	
	<u> </u>			
		31.07.2012	DRAWN :	
	SCALE : DRAWING	1 : 500 NO ·	CHECKED :	REVISI
			47	
	1 14	-Q326-		1 0

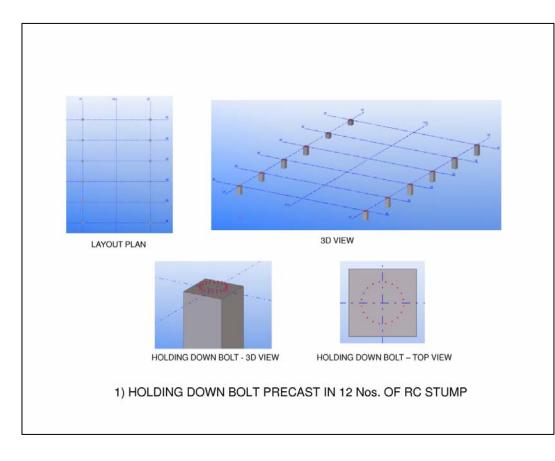


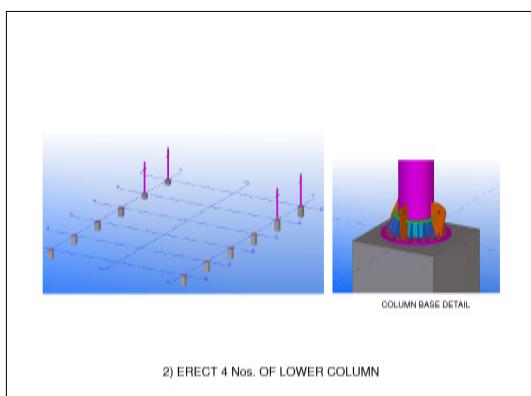
# **11.3 ERECTION SEQUENCE**

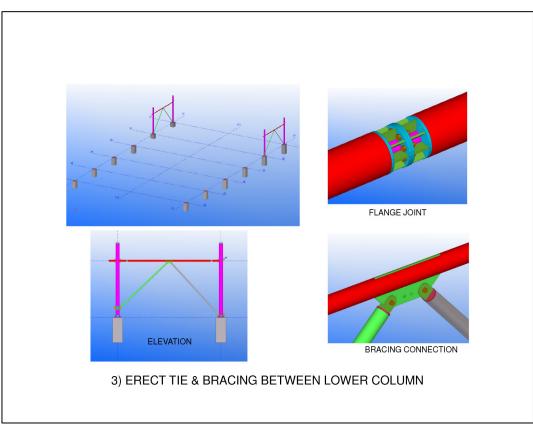


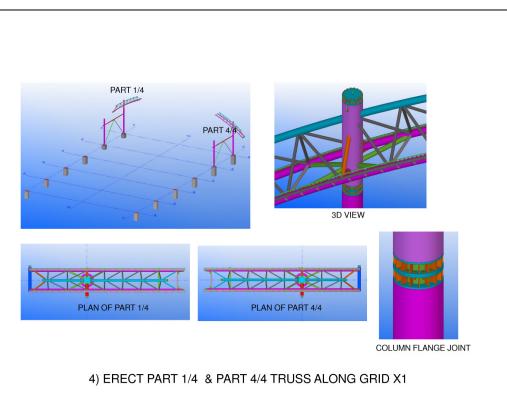






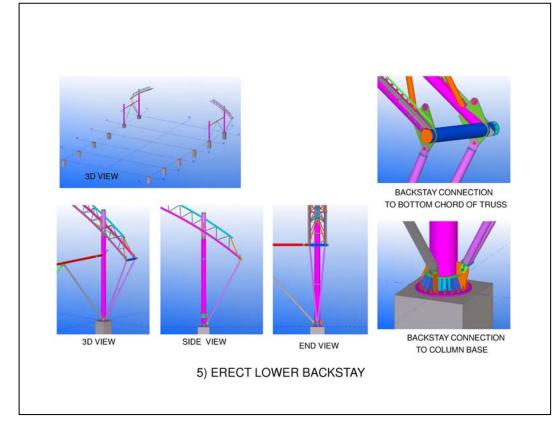


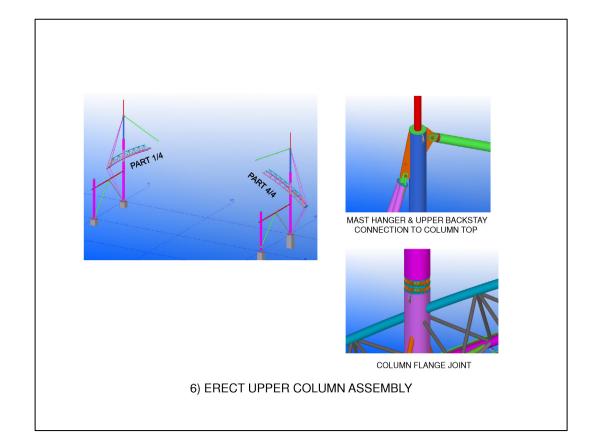


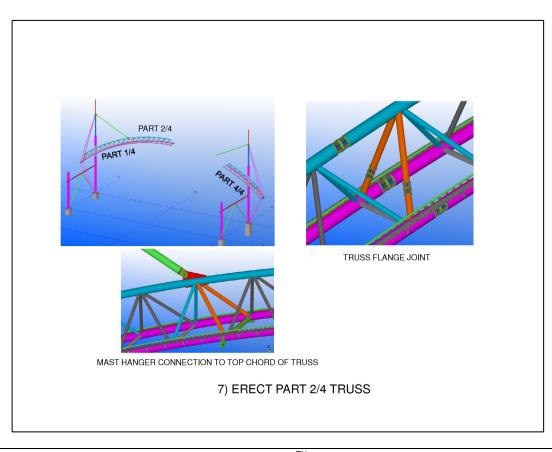


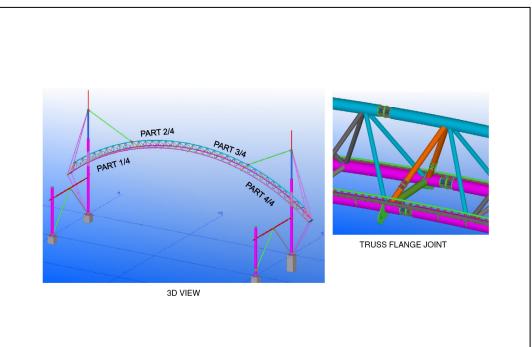








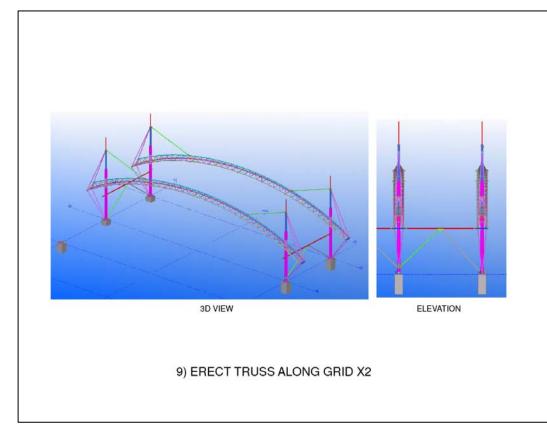


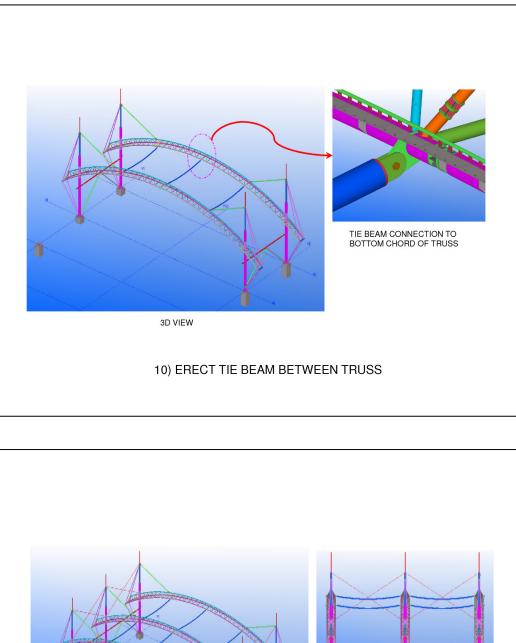


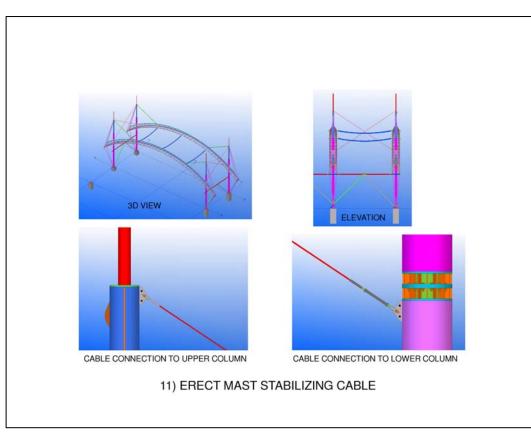
8) ERECT PART 3/4 TRUSS

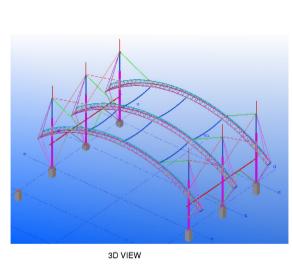












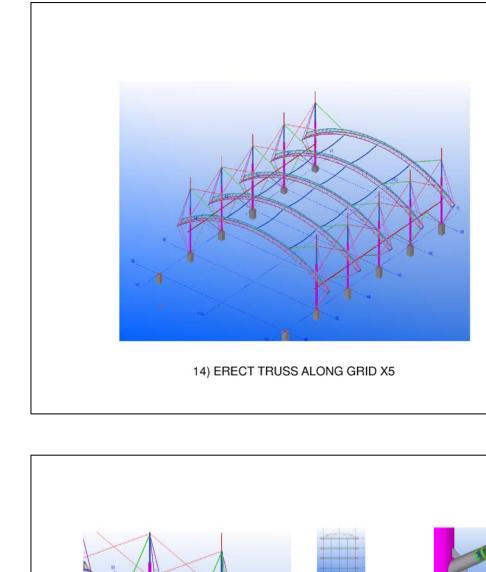
12) ERECT TRUSS ALONG GRID X3

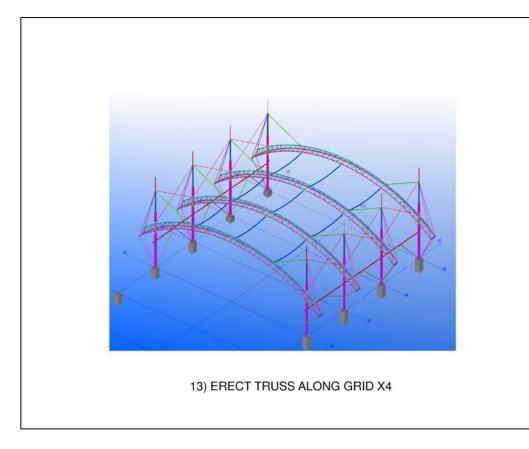


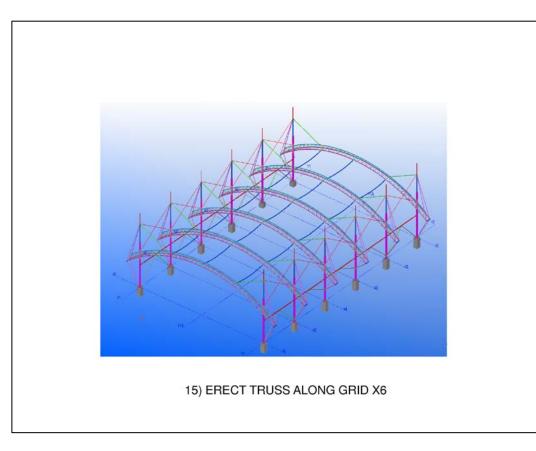
ELEVATION

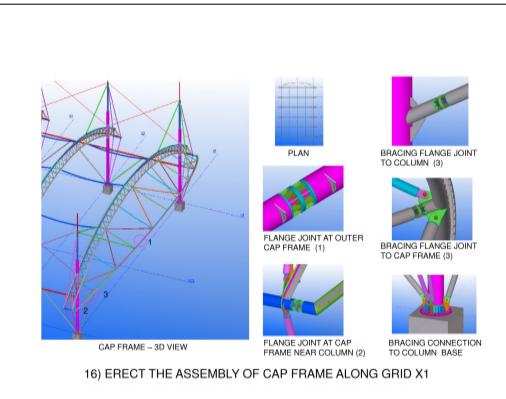






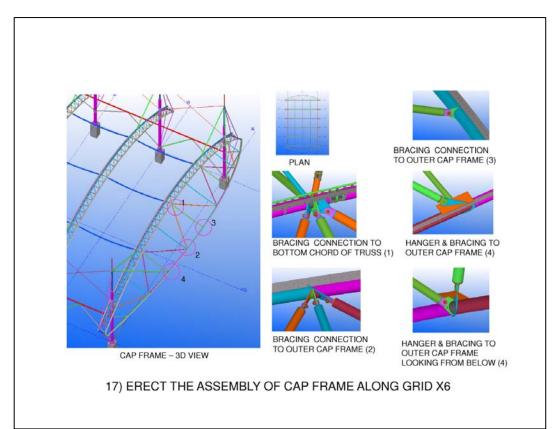


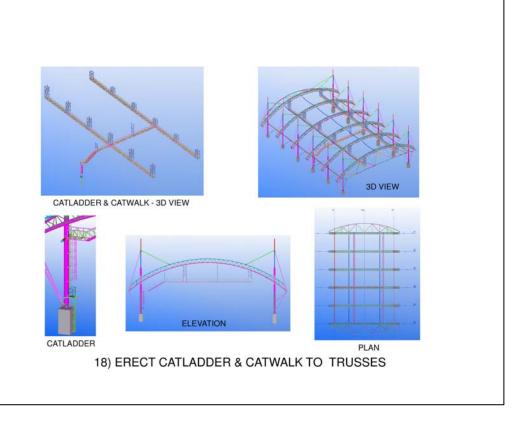


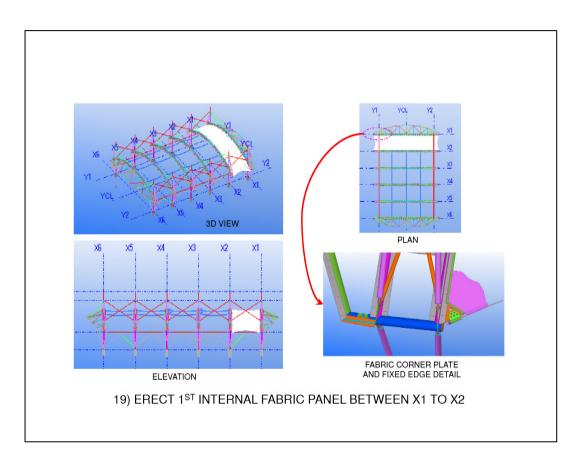


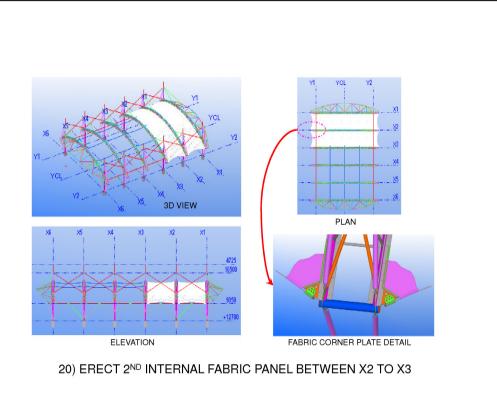






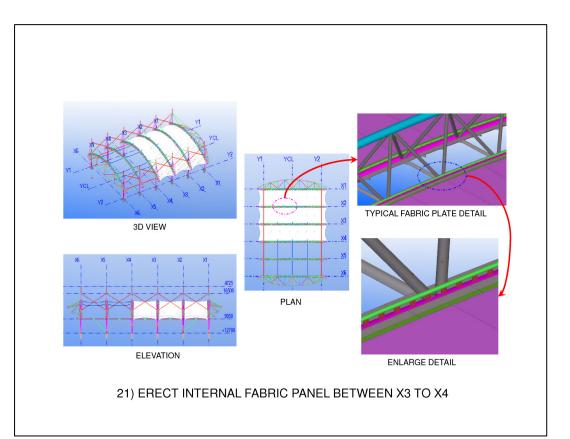


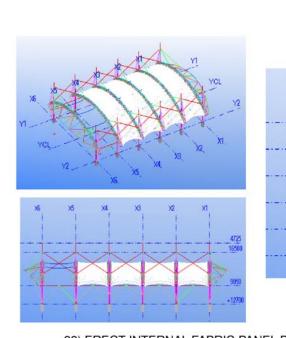


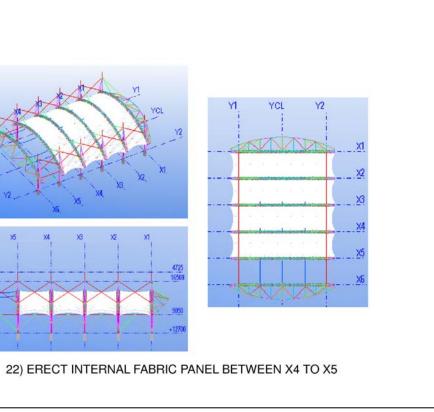


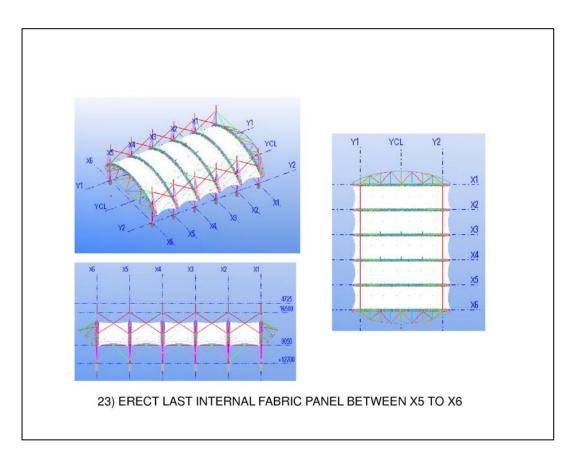
TAN SIEW MOI

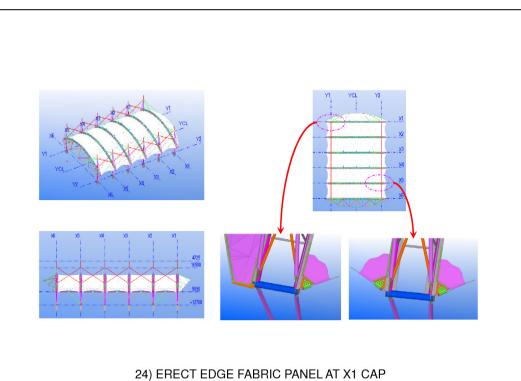


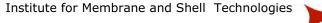




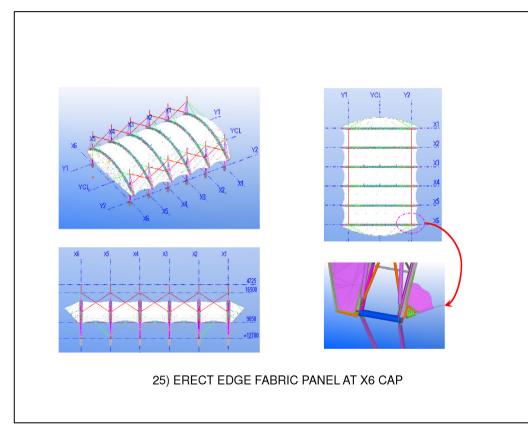


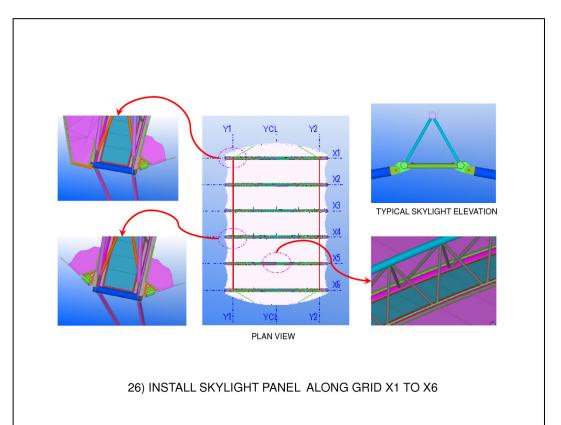


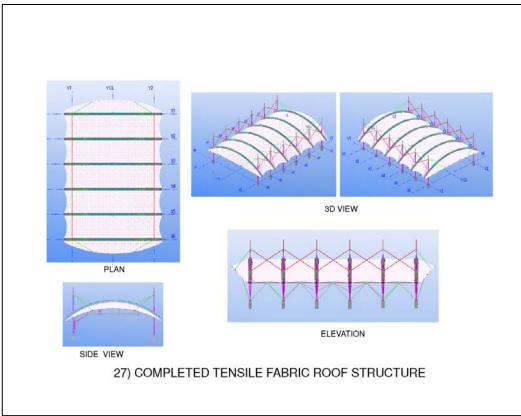












Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES TAN SIEW MOI





# **11.4 PHOTO IMAGES OF STEEL WORK**







#### PHOTO IMAGES – STEEL WORKS (1 OF 6)



TAPAH FACTORY, MALAYSIA



TAPAH FACTORY, MALAYSIA



TRUSS FABRICATION

COLUMN BASE

CLAMPING PLATE



TRUSS & COLUMN FABRICATION



COLUMN FLANGE



TRUSS FABRICATION



WELDING WORK





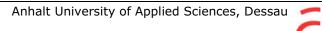
TRUSS FABRICATION



TRUSS WITH COLUMN



CLAMPING PLATE



#### PHOTO IMAGES – STEEL WORKS (2 OF 6)



TRUSS FLANGE JOINT



TRUSS DIAGONALS



ROLLED & WELDED COLUMN



BEFORE SANDBLASTING



AFTER SANDBLASTING



PAINTED TRUSS







PAINTED COLUMN

COLUMN DELIVERY

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES TAN SIEW MOI I





WELDING PREPARATION FOR COLUMN



PAINTED TIE



COLUMN STORAGE

## PHOTO IMAGES – STEEL WORKS (3 OF 6)



TRUSS DELIVERY



UNLOADING OF TRUSS



TRUSS STORAGE



INSTALL HD BOLT



COMPLETED STUMP



ERECT LOWER COLUMN



ERECT LOWER COLUMN



ERECT COLUMN TIE



ERECT COLUMN TIE



Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES TAN SIEW MOI

Institute for Membrane and Shell Technologies



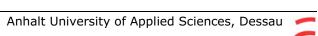
TRUSS STORAGE AT SITE



COLUMN BASE



ERECTED COLUMN TIE



## PHOTO IMAGES – STEEL WORKS (4 OF 6)



ERECT 1/4 TRUSS @ X1



ERECT UPPER COLUMN



ERECT 2/4 TRUSS @ X1



ERECT UPPER COLUMN



ERECT 3/4 TRUSS @ X1



ERECT 2/4 TRUSS @ X2



ERECTED TRUSS @ X3



ERECTED TRUSS @ X2



TAN SIEW MOI

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

ERECTING TRUSS @ X3

Institute for Membrane and Shell Technologies





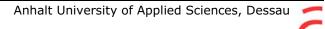
ERECT 4/4 TRUSS @ X1



ERECT 3/4 TRUSS @ X2



ERECTING TRUSS @ X4



## PHOTO IMAGES – STEEL WORKS (5 OF 6)



ERECTED TRUSS @ X4



ERECTING TRUSS @ X5



ERECTED TRUSS @ X6



TRUSS FLANGE CONNECTION



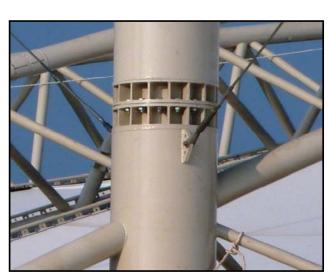
TRUSS FLANGE & TIE JOINT



FRONTSTAY CONNECTION



COLUMN BASE



COLUMN FLANGE JOINT



TRUSS END CONNECTION





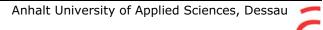
ERECTING CATWALK



COLUMN TOP CONNECTION



COLUMN BRACING CONNECTION



## PHOTO IMAGES – STEEL WORKS (6 OF 6)



ERECTED TRUSS @ X1



ERECTED TRUSS @ X2



ERECTED TRUSS @ X3



ERECTED TRUSS @ X5



ERECTED TRUSS @ X6



CATWALK IN PROGRESS





ERECTED TRUSS @ X4



COMPLETED CATWALK

# **11.5 PHOTO IMAGES OF FABRIC WORK**







#### PHOTO IMAGES – FABRIC WORKS (1 OF 6)



VERSEIDAG FABRIC IN SINGAPORE



FABRIC DELIVERY



TRANSPORT TO TAPAH



FABRIC INSPECTION



FEP DELIVERY



FEP MATERIAL



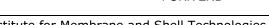
FORK END



28Ø BORDER CABLE



STABILISING CABLE







FABRIC PACKING



NEOPRENE



COMALONG



#### PHOTO IMAGES – FABRIC WORKS (2 OF 6)



FIXED EDGE PREPARATION



TACKING



TACKING



COOLING



SEAMING



EDGE PANEL WITH POCKET



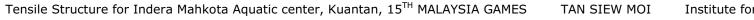
TRIAL FIT EDGE CABLE



TEMPERATURE CONTROL



CORNER PREPARATION







TEMPERATURE CONTROL



INTERNAL PANEL



CORNER PREPARATION





#### PHOTO IMAGES – FABRIC WORKS (3 OF 6)



PREPARE TENSIONING TOOL



CLAMPING TOOL (WARP)



CLAMPING TOOL (WEFT)



TENSIONING ANGLE

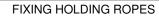


FABRIC PANEL AT SITE



FABRIC ERECTION PLATFORM







LIFTING 1<sup>ST</sup> FABRIC PANEL







RATCHET PULLER



FIX PLATFORM



OPENING FABRIC TO Y2



#### PHOTO IMAGES – FABRIC WORKS (4 OF 6)



OPENING FABRIC TO Y2



**OPENING FABRIC TO Y1** 







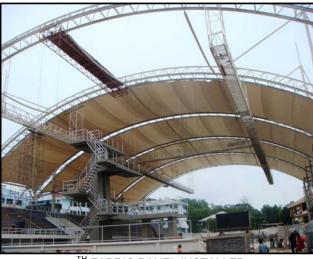
INSTALLING 2<sup>ND</sup> FABRIC PANEL



**OPENING FABRIC TO Y1** 



**OPENING FABRIC TO Y1** 







2<sup>ND</sup> FABRIC PANEL INSTALLED









1<sup>S1</sup> FABRIC PANEL INSTALLED



**OPENING FABRIC TO Y1** 



5<sup>TH</sup> FABRIC PANEL INSTALLED



#### PHOTO IMAGES – FABRIC WORKS (5 OF 6)



FABRIC TENSIONING



FABRIC TENSIONING



FABRIC TENSIONING



WARP TENSIONING



WARP TENSIONING



WARP TENSIONING







WARP TENSIONING



FABRIC TENSIONING





WEFT TENSIONING



FABRIC TENSIONING



WARP TENSIONING



#### PHOTO IMAGES – FABRIC WORKS (6 OF 6)



FIXING FASTENER



FIXING FASTENER



TIE BEAM CLEARANCE



CORNER PLATE



WEFT TENSIONING AT CORNER



FIXED EDGE



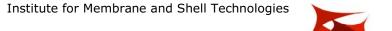
CORNER PLATE



CORNER PLATE



CORNER PLATE







EDGE FIXED



FIXED EDGE



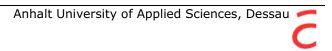
CABLE EDGE



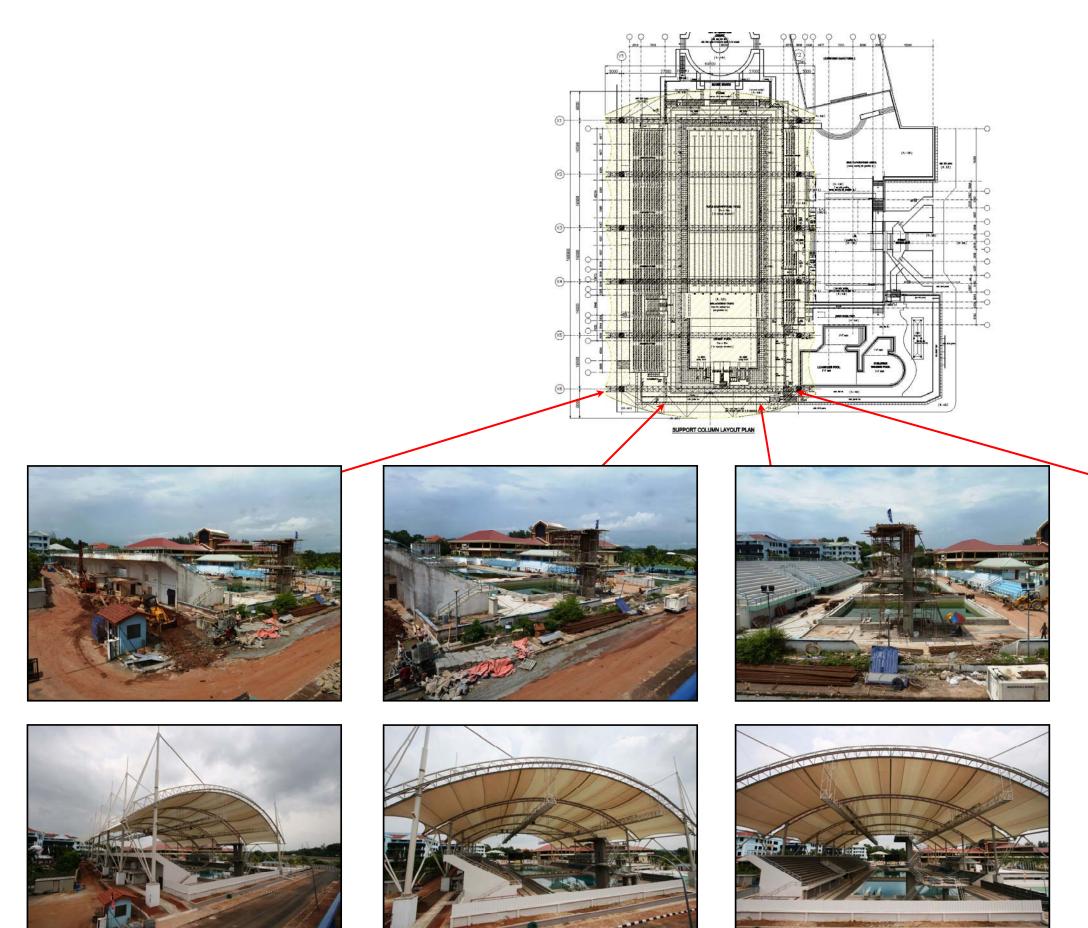
# **11.6 PHOTO IMAGES OF COMPARISON BEFORE & AFTER ERECTION**





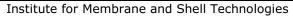


#### **PHOTO IMAGE COMPARISON BEFORE & AFTER ERECTION**



Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

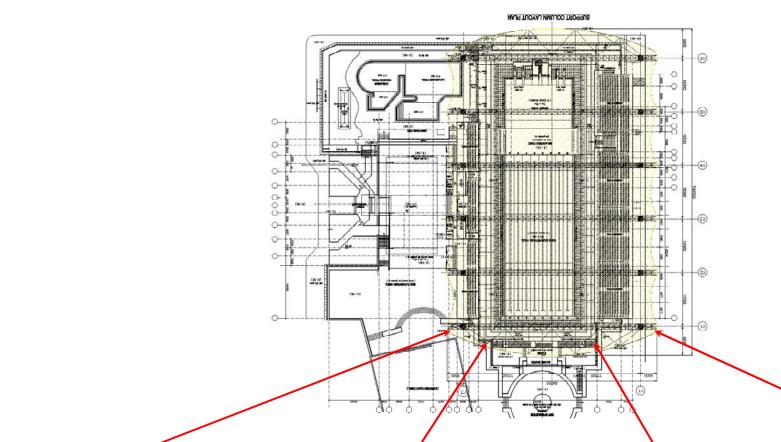
TAN SIEW MOI Institu







#### **PHOTO IMAGE COMPARISON BEFORE & AFTER ERECTION**

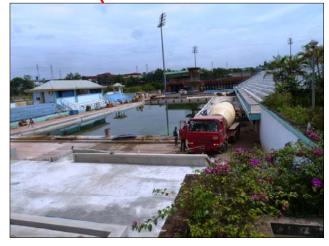








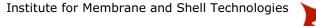






Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

TAN SIEW MOI Institute f





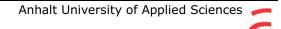




# **11.7 AERIAL VIEW PHASE1 COMPLETION**

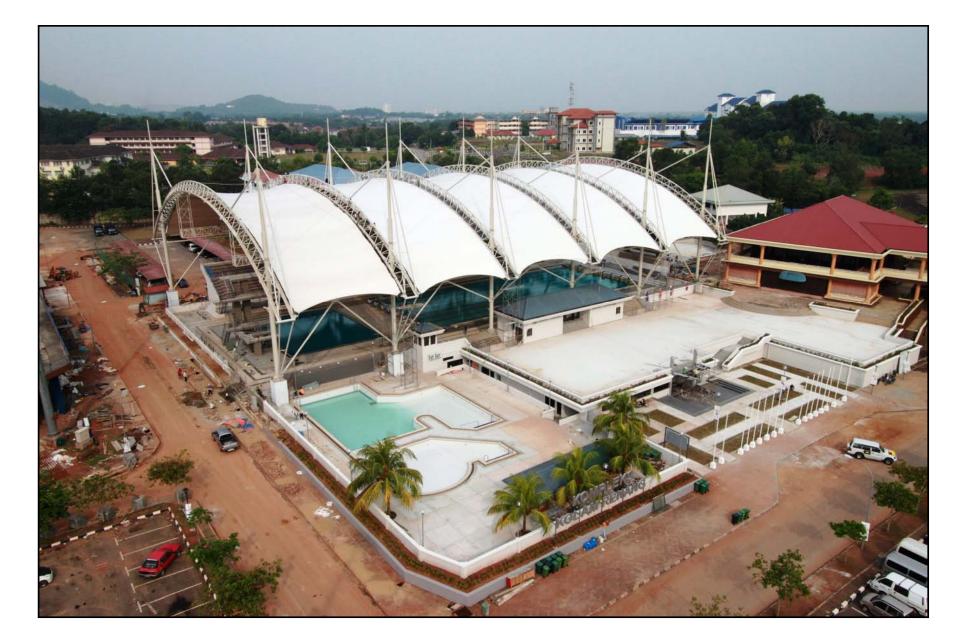








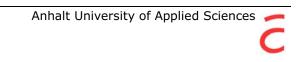
**INTERNAL VIEW** 



HANDOVER CEREMONY

#### **AERIAL VIEW – PHASE 1 COMPLETION**





## **11.8 AERIAL VIEW PHASE2 COMPLETION - IMPRESSION**







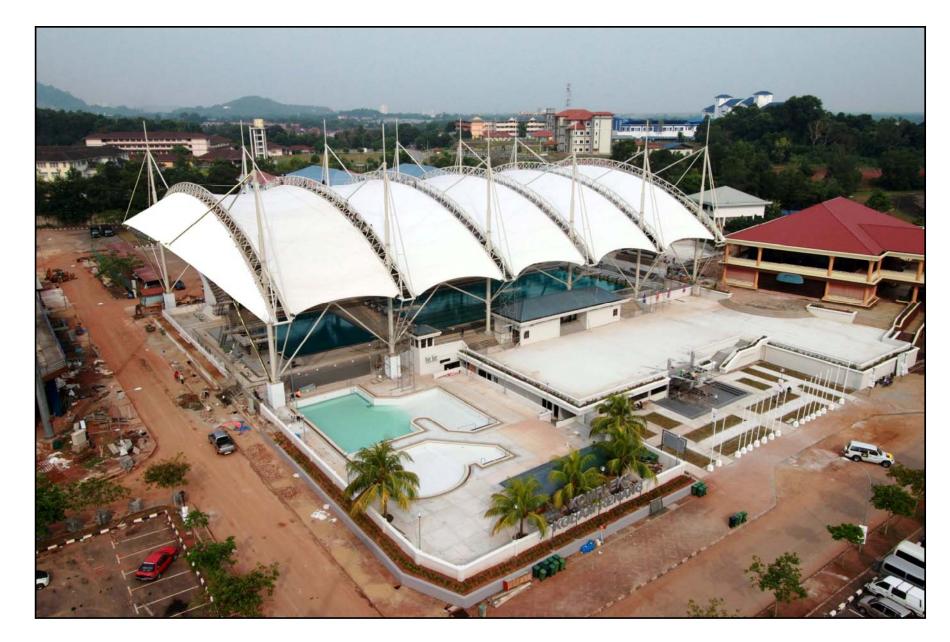






**INTERNAL VIEW** 





#### **AERIAL VIEW – PHASE 2 COMPLETION - IMPRESSION**





# **11.9 NEWSPAPER ARTICLES BEFORE THE GAMES**





#### **NEWSPAPER ARTICLES – BEFORE THE GAMES**

## All systems go

AFTER a month's delay, upgrading works for the 15th Malaysia Games swimming pool in Kuantan were finally completed and it was officially handed over to the organising committee yesterday. Since it was the last venue to be

Since it was the last venue to be completed, Games chief executive officer Ahmad Hairl Hussin made a 'splashing' gimmick when he jumped into the Olympic-size swimming pool from a springboard after making a final inspection on the facility which utilised the latest technology from Germany.

Hairi said he was relieved the pool was ready for the Games.

The RM21 million upgrading works were supposed to be completed on May 30. He said upgrading works and construction of new venues — costing about RM238 million — had already been completed, including the Darulmakmur stadium where the

opening ceremony will be officiated by Sultan Ahmad Shah of Pahang on Saturday and closed by Prime Minister Datuk Seri Najib Razak on July 16.

renovated at a cost of RM21 million, which will be the venue for aquatic events. Pic by Halim Mat Ali

chief executive officer Ahmad Hairi Hussin looks satisfied with the swimming pool,

UTIL ATTE

A ST THE

ted Some 7,000 athletes and officials will participate in the Games which offer 377 gold, 377 silver and 453 bronze medals. By M. Hamzah Jamaludin

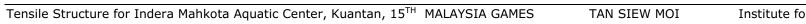




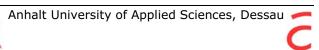




# **11.10 PHOTO IMAGES DURING THE GAMES**







## **PHOTO IMAGES – DURING THE GAMES**



Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

TAN SIEW MOI

Institute for Membrane and Shell Technologies



Anhalt University of Applied Sciences, Dessau 🦛

С

# **11.11 BIAXIAL TEST REPORT**





-

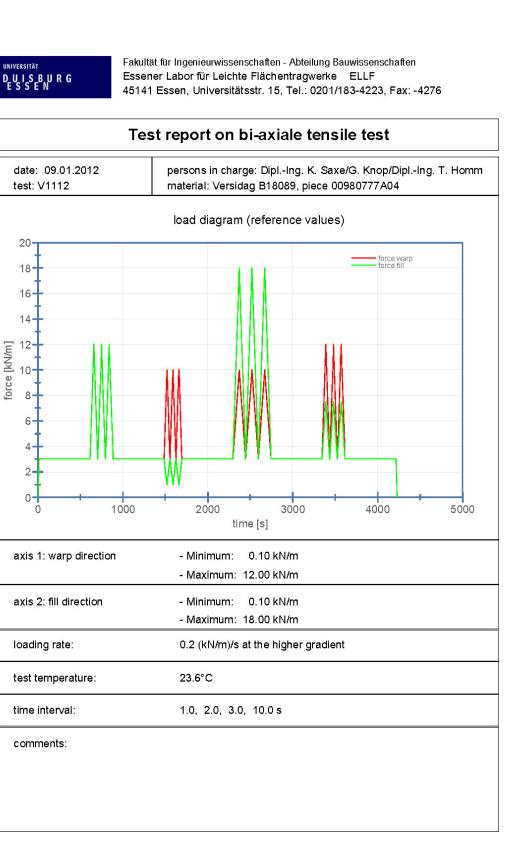


#### NIVERSITÄT D U I S B U R G E S S E N

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

persons in charge: DiplIng.	K. Saxe/G. Knop/DiplIng. T. Homm date: 09.0	date: 09.01.2012
ocation: V15R00H01		
customer:	Verseidag Indutex GmbH Industriestr. 56 47803 Krefeld	
subject of order:	biaxiale test on technical membranes for the project: Swimming Pool, Wisma Belia, Malaysia	Kuantan,
test procedure:	according to specifications by: A.W. Lam	
material:	Versidag B18089, piece 00980777A04	
test:	V1112	
comments:		



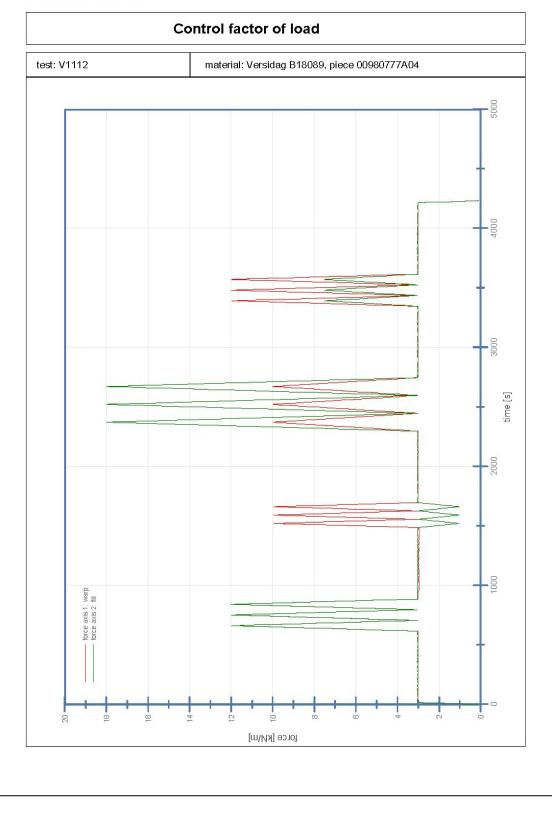


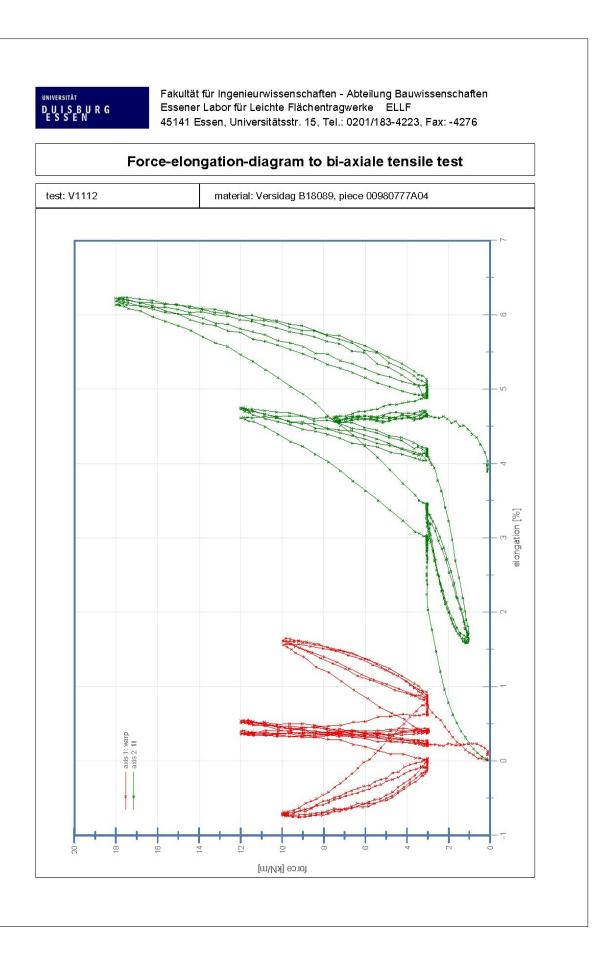






Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax:-4276





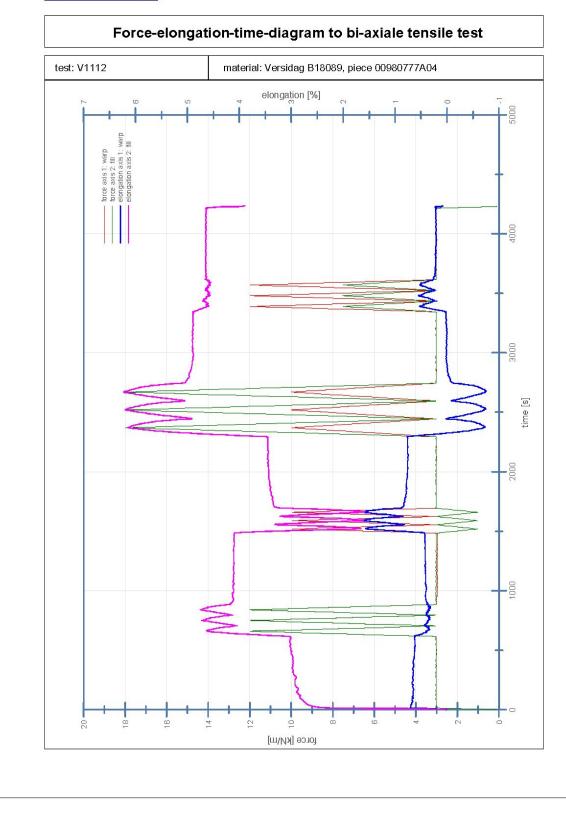


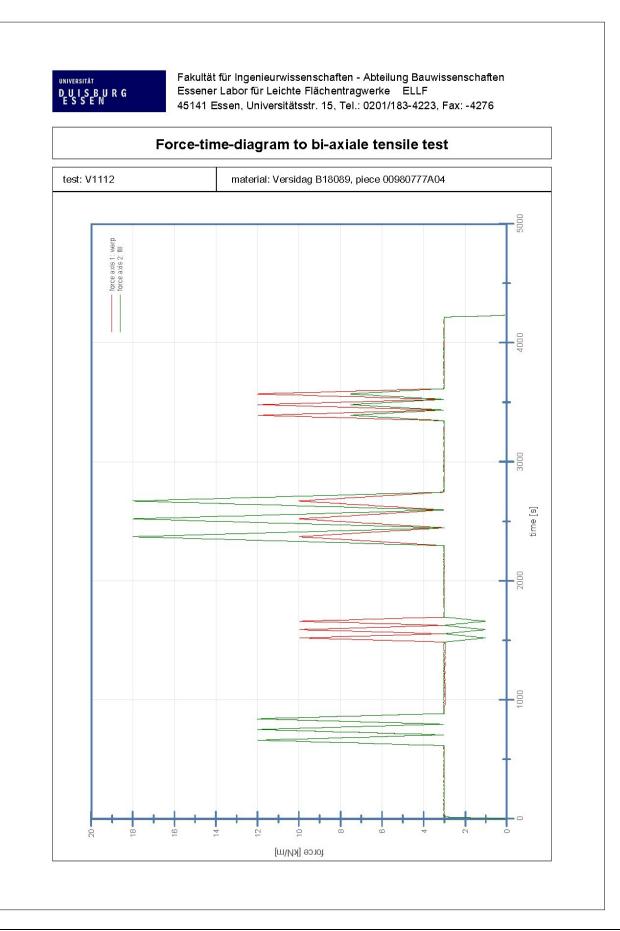






Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax:-4276





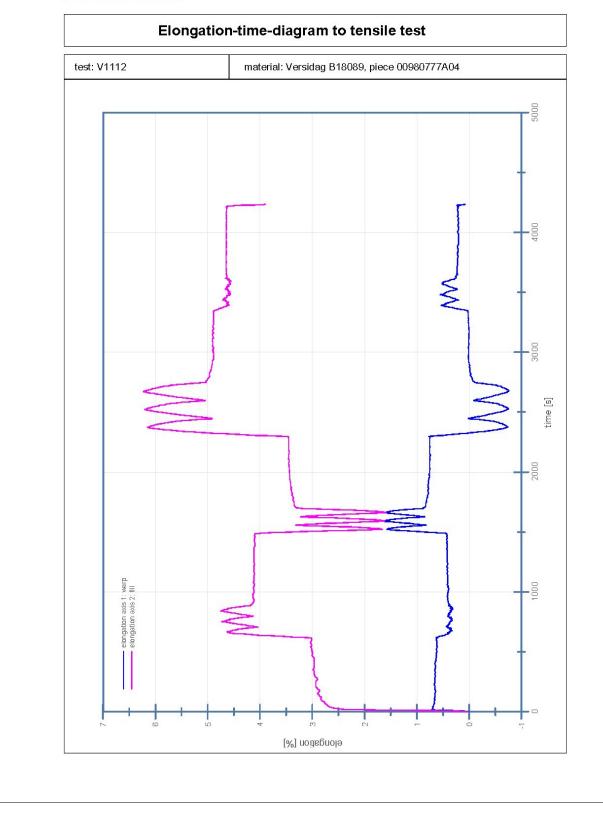
TAN SIEW MOI







Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: 0201/183-4276



DUISBUI	RG

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

test: V1	112		material: V	/ersidag B18	089, piece (	00980777	A04		page: 3
time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elon gatio [%] fill
1518.0	9.55 9.76 9.95		1.50 1.53 1.56	1.90	1660.0	9.95 9.82 9.62	1.03	1.62	1.62 1.59 1.59 1.59
1518.0 1519.0	9.76	1.15 1.07	1.53	1.81	1661.0 1662.0 1663.0	9.82	1.06	1.65	1.59
1520.0	9.95	1.03	1.56	1.71	1662.0	9.62	1.14	1.64	1.59
1521.0	9.81	1.07	1.57	1.67	1663.0	9.42	1.18	1.62	1.59
1522.0 1523.0	9.61 9.42	1.13	1.57	1.66 1.67	1664.0 1665.0	9.22 9.02	1.25 1.30	1.61	1.60
1524.0	9.21	1.25	1.56 1.57 1.54	1.69	1668.0	8.43	1.45	1.56	1.61
1527.0	8.62	1.44	1.54	1.72	1671.0	7.82	1.64	1.53	1.75
1530.0	8.03	1.60	1.51	1.79	1674.0	7.23	1.80	1.49	1.84
1533.0	7.43	1.76	1.48	1.90	1677.0	6.63	1.99	1.45	1.99 2.11 2.28
1536.0	6.83	1.95	1.42	2.00	1680.0	6.03	2.16	1.37	2.11
1539.0	6.23	2.11	1.37	2.13	1683.0	5.44	2.33	1.31	2.28
1542.0 1545.0	5.64 5.04	2.27	1.29	2.29 2.48	1686.0 1689.0	4.84	2.51 2.68	1.24	2.50
1548.0	4.44	2.40	1.22	2.70	1692.0	3.64	2.86	1.04	2.94
1551.0	3.84	2.79	1.02	2.95	1692.0 1693.0	3.64 3.45	2.91	1.01	2.99
1552.0	3.64	2.86	1.14 1.02 0.98	3.04	1694.0	3.25	2.97	0.94	3.09
1553.0	3.44	2.91	0.93	3.12	1695.0	3.05	3.03	0.93	3 15
1554.0	3.25 3.04	2.97 3.02	0.90	3.19	1696.0	3.02	3.03	0.88	3.21
1554.0 1555.0 1556.0	3.04	3.02	0.83	3.19 3.29 3.32	1698.0 1700.0	3.02 3.03	3.04 3.03	0.87	3.25
1557.0	3.19 3.39	2.98 2.92	0.82	3.32	1702.0	3.03	3.03	0.88	3.21 3.25 3.27 3.29
1558.0	3.57	2.32	0.87	3.30	1702.0	3.02	3.04	0.86	3.31
1558.0 1559.0	3.57 3.77	2.89 2.84	0.87 0.88	3.30 3.26	1704.0 1710.0	3.02 3.02	3.03 3.02	0.86	3.31 3.33
1560.0	3.98	2.75	0.91	3.22	1720.0	3.01	3.03	0.83	3.34
1563.0	4.57	2.58	0.95	3.13	1730.0	3.01	3.03	0.83	3.35
1566.0	5.18	2.41	1.03	3.01	1740.0	3.01	3.02	0.83	3.35
1569.0 1572.0	5.77 6.36	2.23 2.07	1.09	2.87 2.72	1750.0 1760.0	3.01 3.02	3.02 3.02	0.81	3.35 3.36
1575.0	6.96	1.88	1.14	2.55	1770.0	3.02	3.02	0.82	3.37
1578.0	7.56	1.73	1.31	2.39	1780.0	3.02	3.03	0.81	3 36
1581.0	8.16	1.56	1.38	2.19	1790.0	3.01	3.03	0.79	3.36 3.38 3.39 3.38
1584.0	8.76	1.38	1.47	2.04	1800.0	3.01	3.02	0.80	3.38
1587.0	9.35 9.55	1.22 1.16	1.54	1.85	1810.0	3.01	3.04	0.79	3.39
1588.0 1589.0	9.55	1.16	1.57 1.61	1.78	1820.0 1830.0	3.02 3.03	3.04 3.03	0.78	3.30
1590.0	9.95	1.04	1.61	1.65	1840.0	3.03	3.03	0.78	3.39 3.40
1591.0	9.82	1.07	1.61	1.61	1850.0	3.02	3.03	0.79	3.40
1592.0	9.95 9.82 9.62	1.13	1.61	1.61	1860.0	3.02 3.02	3.02	0.77	3.41
1593.0	9.42	1.19	1.60	1.63	1870.0	3.02	3.01	0.79	3.39
1594.0	9.23	1.25	1.62	1.64	1880.0	3.01	3.03	0.78	3.41
1596.0 1599.0	8.82 8.24	1.37	1.60 1.57	1.65	1890.0 1900.0	3.01 3.02	3.03 3.04	0.79	3.41 3.41
1602.0	7.63	1.72	1.50	1.81	1910.0	3.02	3.03	0.78	3.41
1605.0	7.04	1.88	1.47	1.92 2.05	1920.0	3.01	3.04	0.78	3.42
1608.0	6.43	2.07	1.42	2.05	1930.0	3.02	3.04	0.78	3.42
1611.0	5.84	2.21	1.36	2.19	1940.0	3.02	3.03	0.77	3.43
1614.0	5.23	2.39	1.26	2.38	1950.0	3.02	3.01	0.77	3.43
1617.0 1620.0	4.63	2.57 2.74	1.17	2.57 2.82	1960.0 1970.0	3.01 3.03	3.04 3.03	0.76	3.43 3.43
1622.0	3.63	2.74	0.99	2.94	1980.0	3.03	3.03	0.78	3.43
1623.0	3.44	2.91	0.96	3.06	1990.0	3.02	3.02	0.76	3.43
1623.0 1624.0	3.24	2.91 2.96	0.96 0.93	3.06 3.13	1990.0 2000.0	3.02 3.01	3.02 3.03	0.76	3.44
1625.0 1626.0 1627.0	3.04	3.03	0.88	3.20 3.22 3.20	2010.0 2020.0	3.01	3.04	0.76	3.43
1626.0	3.18	2.99 2.93	0.85	3.22	2020.0	3.03	3.03	0.76	3.44
1627.0	3.38	2.93	0.88	3.20 3.18	2030.0 2040.0	3.01 3.01	3.02 3.03	0.75	3.44
1629.0	3.78	2.87	0.88	3.19	2040.0	3.03	3.03	0.76	3.44
1632.0	4.37	2.64	0.90	3.09	2060.0	3.02	3.04	0.76	3.44
1635.0	4.97	2.48	1.03	2.96	2070.0	3.01	3.03	0.76	3.45
1638.0	5.58	2.31	1.09	2.85	2080.0	3.02	3.03	0.76	3.45
1641.0	6.18	2.12	1.16	2.70 2.53	2090.0	3.01	3.02	0.76	3.44
1644.0	6.77	1.96	1.24	2.53	2100.0	3.00	3.04	0.75	3.44
1647.0 1650.0	7.37	1.78	1.33	2.36 2.20	2110.0 2120.0	3.02 3.02	3.03	0.75	3.46
1653.0	8.56	1.62	1.40	2.05	2130.0	3.02	3.03	0.75	3.45
1656.0	9.15	1.27	1.52	1.87	2140.0	3.01	3.03	0.74	3.45
1657.0	9.36	1.20	1.54	1.78	2150.0	3.02	3.02	0.76	3.45
1658.0	9.36 9.56	1.13	1.57	1.74	2160.0	3.02	3.04	0.76	3.44
1659.0	9.75	1.09	1.59	1.69	2170.0	3.02	3.02	0.76	3.44



# Measured data of bi-axiale tensile test



UNIVERSITÄT D U I S B U R G E S S E N

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

test: V1	112		material: V	ersidag B18	089, piece (	00980777	A04		page:
time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongati [%] fill
750.0	11.98	11.99	0.37	4.73	970.0	2.95	3.02	0.41	4.13
751.0 752.0	11.84	11.83 11.66	0.36	4.73 4.72	980.0	2.96	3.05 3.02	0.41	4.14
753.0 756.0	11.43	11.46 10.85	0.36	4.71	1000.0	2.95 2.96 2.95	3.03 3.04	0.40	4.1
758.0	10.84	10.85	0.33	4.66 4.63	1020.0	2.96	3.04	0.39	4.1
762.0	9.64	9.65	0.33	4.64	1030.0	2.97	3.04	0.39	4.13
765.0 768.0	9.03	9.05 8.45	0.34	4.64 4.57	1040.0 1050.0	2.96	3.02 3.03	0.41	4.1:
771.0	7.84	7.85	0.35	4.58	1060.0	2.96	3.02	0.42	4.10
774.0 777.0	7.25	7.27	0.33	4.54 4.47	1070.0 1080.0	2.97	3.03 3.04	0.41	4.12
780.0	6.03	6.03	0.36	4.45	1090.0	2.96	3.02	0.41	4.1*
783.0 786.0	5.44	5.45 4.85	0.37	4.41 4.35	1100.0	2.97	3.03	0.41	4.12
789.0	4.26	4.25	0.38	4.31	1120.0	2.97	3.04	0.41	4.11
792.0 793.0	3.64	3.66	0.39	4.20 4.22	1130.0 1140.0	2.96	3.03 3.02	0.41	4.12
794.0	3.24	3.46	0.39	4.19	1140.0	2.98	3.02	0.42	4.1
795.0	3.05	3.06	0.40	4.14	1160.0	2.97 2.96	3.02	0.42	4.11
796.0 797.0	3.18	3.20 3.39	0.39	4.14 4.13	1170.0 1180.0	2.96	3.04	0.41	4.11
798.0 801.0	3.58	3.60	0.41	4.15	1190.0	2.97 2.98	3.02	0.42	4.11
801.0	4.18	4.19	0.40	4.20	1200.0	2.98	3.04 3.02	0.41	4.12
807.0	5.38 5.98	5.43	0.38	4.24 4.27	1210.0 1220.0	2.97 2.98 2.96 2.98	3.03	0.42	4.1*
810.0 813.0	5.98 6.58	6.02 6.60	0.38	4.33 4.37	1230.0 1240.0	2.96	3.02 3.05	0.41	4.10
816.0	7.18	7.19	0.37	4.41	1250.0	2.97	3.03	0.42	4.11
819.0 822.0	7.77 8.37	7.78	0.39	4.46	1260.0 1270.0	2.97	3.02 3.03	0.42	4.1
825.0	8.97	9.00	0.38	4.56	1280.0	2.97	3.02	0.42	4.11
828.0 831.0	9.57 10.19	9.61 10.21	0.38	4.55 4.62	1290.0 1300.0	2.96	3.03 3.02	0.42	4.11
834.0	10.78	10.82	0.34	4.66	1310.0	2.96	3.03	0.42	4.11
837.0 838.0	11.37	11.41	0.34	4.70	1320.0	2.97	3.03 3.04	0.42	4.11
839.0	11.58	11.61 11.80	0.36	4.72	1330.0 1340.0	2.97	3.03	0.42	4.11
840.0 841.0	11.97	12.01	0.36	4.75 4.75	1350.0	2.96	3.02 3.03	0.42	4.11
842.0	11.63	11.86 11.67	0.35	4.73	1360.0 1370.0	2.96 2.97	3.03	0.43	4.1
843.0	11.43	11.46	0.35	4.73	1380.0	2.97	3.03	0.42	4.10
846.0 849.0	10.84	10.84 10.27	0.36	4.71 4.69	1390.0	2.96	3.03 3.02	0.42	4.10
849.0 852.0 855.0	9.64	9.65	0.33	4.68	1410.0	2.96	3.02	0.43	4.10
855.U 858.0	9.03	9.06 8.47	0.32	4.64 4.60	1420.0 1430.0	2.96	3.03 3.03	0.42	4.1
861.0	7.84	7.86	0.34	4.62	1440.0	2.96 2.96	3.03	0.43	4.1*
864.0 867.0	7.24	7.26	0.36	4.55 4.55	1450.0 1460.0	2.96	3.03 3.03	0.42	4.10
870.0	6.02	6.05	0.33	4.48	1470.0	2.96	3.03	0.42	4.11
873.0 876.0	5.43	5.46 4.86	0.35 0.36	4.45 4.37	1476.0 1478.0	2.97 2.96	3.01 3.02	0.43	4.10
879.0 882.0	4.25 3.65	4.27	0.35	4.35 4.28	1480.0	2.96	3.04	0.43	4.10
882.0 883.0	3.65 3.45	3.66 3.46	0.36	4.28 4.24	1482.0 1484.0	2.96 2.97	3.03 3.03	0.43	4.10
884.0	3.25	3.26	0.37	4.22	1486.0	3.14	2.97	0.44	4.05
885.0 886.0	3.05	3.07 3.02	0.39	4.20 4.20	1487.0 1488.0	3.34	2.91 2.85	0.43	4.05
888.0	3.01	3.03	0.39	4.17	1489.0	3.53 3.71	2.80	0.47	3.98
890.0 892.0	3.00	3.03 3.02	0.38	4.18 4.16	1491.0 1494.0	4.11 4.71	2.68 2.52 2.34	0.56	3.94 3.77
894.0	3.01	3.02	0.37	4.17	1497.0	5.30	2.34	0.72	3.63
900.0	3.03	3.03	0.38	4.15	1500.0	5.89	2.16	0.84	3.41
910.0 920.0	3.00	3.03 3.04	0.40	4.13 4.12	1503.0 1506.0	6.54 7.15	2.00 1.83	0.95	3.22
930.0	3.00	3.02	0.41	4.11	1509.0	7.75	1.67	1.19	2.65
940.0 950.0	3.02	3.04 3.02	0.41	4.12 4.13	1512.0 1515.0	8.35	1.49	1.26	2.46
960.0	2.96	3.04	0.42	4.13	1517.0	8.95 9.36	1.20	1.45	2.01

_			1	14	-	
D	U	s s	_B_	U	R	6

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

test: V11	112	1	material: V	ersidag B18	089, piece (	00980777	A04		page: 3
time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongatior [%] fill
1518.0	9.55	1.15	1.50	1.90	1660.0	9.95	1.03	1.62	1.62
1519.0	9.76 9.95	1.07	1.53	1.81	1661.0 1662.0	9.82 9.62	1.06	1.65	1.59
1520.0	9.81	1.03	1.57	1.67	1663.0	9.42	1.14	1.62	1.59
1522.0	9.61	1.13	1.57	1.66	1664.0	9.22 9.02	1.25	1.61	1.60
1521.0 1522.0 1523.0	9.42	1.18	1.56	1.67	1665.0		1.30	1.59	1.61
1524.0	9.21	1.25	1.57	1.69	1668.0	8.43	1.45	1.56	1.69
1527.0 1530.0	8.62	1.44	1.54	1.72	1671.0 1674.0	7.82	1.64	1.53	1.75
1533.0	7.43	1.76	1.48	1.90	1677.0	6.63	1.99	1.45	1.99
1536.0	6.83	1.95	1.42	2.00	1680.0	6.03	2.16	1.37	2.11
1539.0	6.23	2.11	1.37	2.13	1683.0	5.44	2.33	1.31	2.28
1542.0	5.64	2.27 2.46	1.29	2.29	1686.0	4.84	2.51	1.24	2.50
1545.0 1548.0	5.04	2.46	1.22	2.48 2.70	1689.0	4.24 3.64	2.68	1.14	2.69
1551.0	3.84	2.62	1.02	2.95	1693.0	3.45	2.86	1.04	2.50 2.69 2.94 2.99
1552.0	3.64	2.86	0.98	3.04	1694.0	3.25	2.97	0.94	3.09
1553.0	3.44	2.91	0.93	3.12	1695.0	3.25 3.05	3.03	0.93	3.15
1554.0	3.25 3.04	2.97 3.02	0.90	3.19	1696.0	3.02	3.03	0.88	3.21 3.25 3.27
1555.0 1556.0	3.04	2.98	0.83	3.29 3.32	1698.0 1700.0	3.02 3.03	3.04 3.03	0.87	3.25
1557.0	3.39	2.92	0.82	3.31	1702.0	3.02	3.04	0.87	3.29
1558.0	3.57 3.77	2.89 2.84	0.87	3.30 3.26	1704.0	3.02 3.02	3.03 3.02	0.86	3.31 3.33
1559.0		2.84	0.88	3.26	1710.0	3.02		0.84	3.33
1560.0 1563.0	3.98 4.57	2.75	0.91	3.22 3.13	1720.0 1730.0	3.01 3.01	3.03	0.83	3.34 3.35
1566.0	5.18	2.58 2.41	1.03	3.01	1740.0	3.01	3.03	0.83	3.35
1569.0	5.77	2.23	1.09	2.87	1750.0	3.01	3.02	0.81	3.35
1572.0	6.36	2.07	1.14	2.72	1760.0	3.02	3.02	0.82	3.36
1575.0	6.96	1.88	1.24	2.55	1770.0	3.02	3.02	0.81	3.37
1578.0 1581.0	7.56	1.73	1.31	2.39 2.19	1780.0 1790.0	3.02	3.03	0.81	3.36
1584.0	8.76	1.38	1.47	2.04	1800.0	3.01	3.02	0.80	3.38
1587.0	9.35	1.38 1.22	1.54	1.85	1810.0	3.01	3.04	0.79	3.39
1588.0	9.55	1.16	1.57	1.78	1820.0	3.02	3.04	0.78	3.38
1589.0 1590.0	9.76	1.10	1.61	1.73	1830.0 1840.0	3.03	3.03	0.78	3.39
1591.0	9.82	1.04	1.61	1.65	1850.0	3.02	3.03	0.79	3.40
1592.0	9.62	1.13	1.61	1.61	1860.0	3.02	3.02	0.77	3.41
1593.0	9.42	1.19	1.60	1.63	1870.0	3.02	3.01	0.79	3.39
1594.0	9.23	1.25	1.62	1.64	1880.0	3.01	3.03	0.78	3.41
1596.0 1599.0	8.82 8.24	1.37	1.60	1.65	1890.0 1900.0	3.01 3.02	3.03 3.04	0.79	3.41
1602.0	7.63	1.72	1.50	1.81	1910.0	3.02	3.03	0.78	3.41
1605.0	7.04	1.88	1.47	1.92	1920.0	3.01 3.02	3.04	0.78	3.42
1608.0	6.43	2.07	1.42	2.05	1930.0	3.02	3.04	0.78	3.42
1611.0 1614.0	5.84 5.23	2.21	1.36 1.26	2.19	1940.0 1950.0	3.02	3.03 3.01	0.77	3.43
1617.0	4.63	2.39 2.57 2.74	1.17	2.38 2.57	1960.0	3.02	3.04	0.76	3.43
1620.0	4.03	2.74	1.07	2.82	1970.0	3.03	3.03	0.76	3.43
1622.0	3.63	2.86	0.99	2.94	1980.0	3.02	3.04	0.77	3.43
1623.0 1624.0	3.44 3.24	2.91 2.96	0.96	3.06 3.13	1990.0 2000.0	3.02	3.02	0.76	3.43
1624.0	3.04	3.03	0.88	3.20	2010.0	3.01	3.03	0.76	3.44
1626.0	3.18	299	0.85	3.22	2020.0	3.03	3.03	0.76	3.44
1627.0	3.38	2.93	0.88	3.20	2030.0	3.01	3.02	0.75	3.44
1628.0	3.58	2.87	0.88	3.18	2040.0	3.01	3.03	0.76	3.44
1629.0 1632.0	3.78 4.37	2.82	0.90	3.19 3.09	2050.0 2060.0	3.03	3.03	0.76	3.45
1635.0	4.97	2.48	1.03	2.96	2070.0	3.01	3.03	0.76	3.45
1638.0	5.58	2.31 2.12	1.09	2.85 2.70	2080.0	3.02	3.03	0.76	3.45
1641.0	6.18 6.77	2.12	1.16	2.70	2090.0	3.01	3.02	0.76	3.44
1644.0 1647.0	7.37	1.96 1.78	1.24	2.53	2100.0 2110.0	3.00	3.04	0.75	3.44
1650.0	7.97	1.62	1.40	2.20	2120.0	3.02	2 99	0.75	3.46
1653.0	8.56	1.44	1.46	2.05	2130.0	3.01	3.03	0.75	3.45
1656.0	9.15	1.27	1.52	1.87	2140.0	3.01 3.01	3.03	0.74	3.45
1657.0 1658.0	9.36 9.56	1.20	1.54	1.78	2150.0 2160.0	3.02	3.02 3.04	0.76	3.45
1658.0	9.56	1.13	1.57	1.69	2170.0	3.02	3.04	0.76	3.44



# Measured data of hi-aviale tensile test



UNIVERSITÄT DUISBURG ESSEN

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

time [s] 2180.0			2	ersidag B18		94903945656747 - 80745	2 - 2012-1994:		page:
2180.0	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongati [%] fill
	3.01	3.05	0.76	3.45	2442.0	3.31	3.64	-0.09	5.07
2190.0 2200.0	3.01 3.02	3.02	0.76	3.45	2443.0 2444.0	3.22 3.12	3.44 3.25	-0.07 -0.02	5.04 4.93
2210.0 2220.0	3.00	3.04	0.75	3.45	2445.0	3.02	3.05	-0.00	4.94
2220.0 2230.0	3.02 3.02	3.03 3.03	0.76	3.45 3.45	2446.0 2447.0	3.09 3.18	3.21 3.41	0.02	4.91 4.92
2240.0	3.02	3.03	0.76	3.45	2447.0	3.13	3.61	-0.01	4.92
2240.0 2250.0	3.02	3.03	0.76	3.45	2451.0	3.56	4.21	-0.03	4.97
2260.0	3.01 3.01	3.03 3.02	0.76	3.45 3.45	2454.0 2457.0	3.84	4.80	-0.05 -0.08	5.03 5.08
2270.0 2280.0	3.02	3.04	0.76	3.45	2460.0	4.40	5.99	-0.15	5.15
2286.0	3.01	3.02	0.75	3.45	2463.0	4.68	6.60	-0.16	5.15 5.22
2288.0 2290.0	3.01 3.03	3.02 3.03	0.76	3.46 3.45	2466.0	4.97	7.20	-0.23 -0.25	5.28 5.33
2292.0	3.02	3.03	0.76	3.45	2469.0 2472.0	5.25 5.53 5.79	8.40	-0.28	5.41
2294.0	3.02	3.03	0.76	3.46	2475.0	5.79	8.98	-0.33	5.47
2296.0 2297.0	3.09	3.21 3.41	0.77	3.47 3.50	2478.0 2481.0	6.07 6.35	9.59 10.22	-0.34 -0.37	5.53 5.59
2298.0	3.27 3.55	3.59	0.75	3.57 3.73	2484.0	6.65	10.81	-0.40	5.64
2301.0	3.55	4.20	0.67	3.73	2487.0	6.93	11.40	-0.43	5.67
2304.0 2307.0	3.84	4.81	0.59	3.91 4.08	2490.0 2493.0	7.20	12.00 12.59	-0.47	5.76 5.78
2310.0 2313.0	4.40	6.02 6.59	0.44	4.23	2496.0 2499.0	7.76	13.19	-0.53 -0.54	5.85 5.88
2313.0	4.67	6.59	0.34	4.38	2499.0	8.03	13.80	-0.54	5.88
2316.0 2319.0 2322.0 2325.0	4.96 5.25 5.52 5.80	7.19	0.27	4.51 4.64	2502.0 2505.0	8.33	14.42	-0.59 -0.63	5.93 6.01
2322.0	5.52	8.40	0.10	4.81	2508.0 2511.0	8.88 9.15	15.62	-0.65	6.03 6.07
2325.0 2328.0	5.80	8.99 9.59	0.02	4.93 5.03	2511.0 2514.0	9.15	16.19 16.79	-0.67 -0.69	6.07
2331.0	6.36	10.20	-0.10	5.15	2517.0	9.71	17.40	-0.70	6.16
2334.0	6.64	10.81	-0.17	5.26	2518.0	9.80	17.61	-0.71	6.17
2337.0 2340.0	6.92	11.40 11.99	-0.24 -0.30	5.37 5.46	2519.0 2520.0	9.90	17.81 18.00	-0.70 -0.72	6.17 6.18
2343.0	7.47	12 60	-0.35	5.57 5.62	2521.0 2522.0	9.94	17.87	-0.72	6.20 6.20
2346.0	7.76	13.21	-0.42	5.62	2522.0	9.84	17.67	-0.72	6.20
2349.0 2352.0	8.04 8.32	13.81 14.39	-0.46 -0.51	5.70 5.79	2523.0 2526.0	9.76 9.47	17.45	-0.71 -0.75	6.20 6.16
2355.0	8.60	14.99	-0.54	5.85	2529.0 2532.0 2535.0	9.19	16.26	-0.75	6.16
2358.0 2361.0	8.87 9.17	15.61 16.22	-0.57 -0.63	5.91 5.97	2532.0	8.91 8.62	15.64 15.07	-0.75	6.14 6.14
2364.0	9.44	16.81	-0.66	6.05	2538.0	8.35	14.45	-0.73	6.09
2367.0	9.71	17.39	-0.68	6.08	2541.0	8.07 7.79	13.86	-0.70	6.07
2368.0 2369.0	9.81	17.39 17.59 17.79	-0.69 -0.70	6.11 6.12	2544.0 2547.0	7.79	13.26 12.65	-0.70 -0.66	6.03 6.02
2370.0	9.99	17.99	-0.70	6.13	2550.0	7.23	12.04	-0.65	5 99
2371.0 2372.0	9.93 9.83	17.85 17.66	-0.69	6.14 6.15	2553.0 2556.0	6.94 6.67	11.45 10.86	-0.66	5.93 5.92
2373.0 2376.0	9.74	17.46	-0.72	6.13	2559.0	6.39	10.26	-0.61	5.90
2376.0	9.47	16.85	-0.74	6.12	2562.0 2565.0	6.11	9.66	-0.58	5.83
2379.0 2382.0	9.19 8.90	16.85 16.25 15.63	-0.72	6.10 6.10	2565.0	5.82 5.55	9.05	-0.57 -0.57	5.79 5.78
2385.0	8.62	15.05	-0.71	6.07	2571.0 2574.0	5.27 5.00	7.85	-0.54	5.72 5.67
2388.0 2391.0	8.35 8.07	14.45 13.88	-0.70 -0.69	6.03 6.04	2574.0 2577.0	5.00	7.27	-0.50 -0.47	5.67
2394.0	7.80	13.25	-0.67	6.00	2580.0	4.43	6.05	-0.41	5.62 5.52
2397.0	7.51	12.62 12.04	-0.64	5.98	2583.0	4.14	5.45	-0.35	5.49
2400.0 2403.0	7.23	12.04	-0.65 -0.64	5.93 5.91	2586.0 2589.0	3.87 3.58	4.85 4.26	-0.29 -0.23	5.35 5.28
2406.0	6.67	10.87	-0.61	5.86	2592.0	3.32	3.66	-0.17	5.18
2409.0	6.39 6.10	10.26	-0.57	5.82 5.77	2593.0	3.23	3.48 3.26	-0.16	5.13 5.11
2412.0 2415.0	5.82	9.65 9.05	-0.58 -0.55	5.74	2594.0 2595.0	3.13 3.04	3.05	-0.15	5.07
2418.0	5.55	8.46	-0.52	5.70	2596.0	3.11	3.19	-0.09	5.05
2421.0 2424.0	5.28 5.00	7.86	-0.51 -0.46	5.64 5.61	2597.0 2598.0	3.19 3.29	3.41 3.60	-0.09 -0.08	5.05 5.06
2424.0	4.70	6.64	-0.42	5.51	2601.0	3.55	4.20	-0.08	5.06
2430.0	4.43	6.04	-0.35	5.49	2604.0	3.84	4.79	-0.13	5.16
2433.0 2436.0	4.15 3.87	5.45 4.87	-0.30 -0.25	5.34 5.29	2607.0 2610.0	4.12	5.38 6.00	-0.17 -0.22	5.20 5.27
2439.0	3.60	4.07	-0.19	5.19	2613.0	4.69	6.61	-0.22	5.34



Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

test: V11	12	1	material: V	ersidag B18	089, piece (	0980777	۹04		page: 5
time [s]	force [kN/m]	force [kN/m]	elongation [%]	elongation [%]	time [s]	force [kN/m]	force [kN/m]	elongation [%]	elongation [%]
0040.0	warp	fill	warp	fill	2012.0	warp	fill	warp	fill
2616.0 2619.0	4.96	7.20 7.80	-0.27 -0.32	5.38 5.47	2910.0 2920.0	3.02	3.02 3.05	-0.00 0.01	4.91 4.91
2622.0	5.52	8.39	-0.32	5.48	2930.0	3.02	3.03	0.01	4.91
2625.0	5.80	8.98	-0.38	5.57	2940.0	3.01	3.03	0.01	4.89
2628.0	6.08	9.60	-0.40	5.62	2950.0	3.02	3.03	0.02	4.89
2631.0	6.36	10.20	-0.43	5.65	2960.0	3.02	3.05	0.01	4.89
2634.0	6.64	10.82	-0.45	5.73	2970.0	3.02	3.04	0.02	4.89
2637.0 2640.0	6.93 7.21	11.41 12.00	-0.47 -0.50	5.77 5.81	2980.0 2990.0	3.01 3.01	3.03 3.02	0.01	4.88
2643.0	7.48	12.60	-0.52	5.87	3000.0	3.02	3.03	0.01	4.90
2646.0	7.75	13.19	-0.56	5.88	3010.0	3.02	3.03	0.01	4.89
2649.0	8.03	13.79	-0.59	5.95	3020.0	3.01	3.03	0.01	4.91
2652.0 2655.0 2658.0	8.32 8.59 8.88	14.40	-0.60	6.00	3030.0	3.01	3.02	0.01	4.89
2658.0	8.89	15.01	-0.64	6.01 6.05	3040.0 3050.0	3.02 3.01	3.03 3.03	0.02	4.89 4.91
2661.0	9.16	15.60 16.22	-0.67	6.12	3060.0	3.01	3.03	0.01	4.91
2664.0	9.44	16.81	-0.71	6.16	3070.0	3.03	3.02	0.00	4.90
2667.0	9.72	17.42	-0.73	6.19	3080.0	3.02	3.03	0.01	4.90
2668.0	9.81	17.62	-0.73	6.22	3090.0	3.02	3.03	0.01	4.90
2669.0 2670.0	9.90	17.81 18.01	-0.72 -0.73	6.22 6.22	3100.0 3110.0	3.02 3.01	3.01 3.02	0.01	4.91
2671.0	9.94	17.85	-0.73	6.22	3120.0	3.01	3.02	0.00	4.89
	9.84	17.66	-0.74	6.23 6.23	3130.0	3.02 3.02	3.03	0.01	4.90
2672.0 2673.0	9.74	17 46	-0.74	6.23	3140.0	3.02	3.03	-0.00	4.90
2676.0	9.46	16.85 16.26 15.66	-0.75	6.21	3150.0	3.03	3.04	0.01	4.91
2679.0 2682.0	9.18	16.26	-0.76	6.19 6.15	3160.0 3170.0	3.01 3.02	3.03 3.02	0.00	4.89
2685.0	8.62	15.06	-0.74	6.13	3180.0	3.01	3.01	-0.00	4.91
2688.0	8.35	14.44	-0.72	6.11	3190.0	3.02	3.03	0.01	4.89
2691.0	8.06	13.85	-0.73	6.08	3200.0	3.02	3.04	0.00	4.89
2694.0	7.79	13.25 12.67	-0.71	6.07	3210.0	3.02 3.02	3.06 3.02	0.01	4.90
2697.0 2700.0	7.50	12.07	-0.68	6.04	3220.0 3230.0	3.02	3.02	0.01	4.90
2703.0	6.96	11.46	-0.64	5.99 5.99	3240.0	3.01	3.01	0.01	4.88
2706.0	6.67	10.86	-0.64	5.94	3250.0	3.02	3.03	0.02	4.89
2709.0	6.39	10.26	-0.61	5.92 5.87	3260.0	3.02	3.03	0.02	4.89
2712.0 2715.0	6.12	9.65 9.06	-0.62	5.87 5.85	3270.0	3.02 3.01	3.04 3.03	0.01	4.89
2718.0	5.84 5.54	8.46	-0.61 -0.57	5.79	3280.0 3290.0	3.01	3.03	0.01	4.89
2721.0	5.27	7.85	-0.54	5.73	3300.0	3.01	3.02	0.02	4.89
2724.0	4.99	7.24	-0.53	5.72	3310.0	3.01	3.01	0.02	4.89
2727.0	4.70	6.64	-0.49	5.64	3320.0	3.01	3.02	0.02	4.89
2730.0 2733.0	4.43 4.15	6.03 5.44	-0.43	5.64 5.58 5.50	3330.0 3336.0	3.01 3.01	3.03 3.02	0.02	4.89
2736.0	3.87	4.85	-0.32	5.42	3338.0	3.00	3.02	0.02	4.88
2739.0	3.59	4.24	-0.28	5.34	3340.0	3.01	3.03	0.03	4.89
2742.0	3.30	3.64	-0.20	5.24	3342.0	3.02	3.02	0.02	4.88
2743.0 2744.0	3.21 3.12	3.45	-0.20	5.19	3344.0 3346.0	3.01 3.19	3.03 3.11	0.03	4.88
2744.0	3.03	3.25 3.05	-0.17	5.18 5.13	3347.0	3.38	3.21	0.02	4.89
2746.0	3.01	3.03	-0.12	5.10	3348.0	3.38 3.58	3.31	0.04	4.87
2748.0	3.01	3.03	-0.12	5.06 5.04	3351.0	4.18	3.61	0.09	4.84
2750.0	3.02	3.03	-0.10	5.04	3354.0	4.78	3.92	0.09	4.83
2752.0 2754.0	3.02	3.02 3.04	-0.09	5.03 5.03	3357.0 3360.0	5.37 5.98	4.22	0.14	4.81 4.79
2760.0	3.02	3.04	-0.03	5.03	3363.0	6.58	4.81	0.13	4.79
2770.0	3.02	3.03	-0.06	5.01	3366.0	7.18	5.11	0.28	4.77
2780.0	3.01	3.02	-0.06	5.00	3369.0	7.78	5.41	0.29	4.73
2790.0 2800.0	3.01 3.01	3.03 3.02	-0.05 -0.04	4.98	3372.0 3375.0	8.38	5.72 6.01	0.32	4.72
2800.0	3.01	3.02	-0.04	4.96	3375.0	9.58	6.01	0.35	4.70
2820.0	3.01	3.02	-0.03	4.97	3381.0	9.58 10.18	6.61	0.42	4.67
2830.0	3.01	3.03	-0.02	4.96	3384.0	10.78	6.91	0.47	4.64
2840.0	3.01	3.03	-0.01	4.95	3387.0	11.38 11.58	7.20 7.31	0.48	4.64
2850.0	3.00	3.03	-0.01	4.94	3388.0	11.58	7.31	0.50	4.63
2860.0 2870.0	3.01 3.02	3.04 3.03	-0.01 -0.01	4.93	3389.0 3390.0	11.78 11.97	7.42	0.51	4.63
2880.0	3.01	3.02	0.00	4.92	3391.0	11.85	7.44	0.53	4.61
2890.0	3.01	3.02	-0.01	4.92	3392.0	11.64	7.34 7.24	0.53	4.61 4.61 4.59
2900.0	3.02	3.02	0.00	4.91	3393.0	11.45	7.24	0.52	4.59





# NIVERSITÄT D U I S B U R G E S S E N

Fakultät für Ingenieurwissenschaften - Abteilung Bauwissenschaften Essener Labor für Leichte Flächentragwerke ELLF 45141 Essen, Universitätsstr. 15, Tel.: 0201/183-4223, Fax: -4276

test: V11	12		material: V	ersidag B18	089, piece (	00980777	A04		page:
time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [\$]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongati [%] fill
3396.0 3399.0	10.84 10.24	6.94 6.65	0.48	4.59 4.62	3568.0 3569.0	11.58 11.78	7.31 7.41	0.51	4.58 4.57
3402.0 3405.0	9.64 9.04	6.34	0.44	4.63	3570.0 3571.0	11.98	7.51	0.51	4.57 4.56
3408.0 3411.0	8.45 7.85	5.74 5.45	0.46	4.63 4.61	3572.0 3573.0	11.64	7.35 7.26	0.51	4.57 4.56
3414.0 3417.0	7.25	5.15 4.86	0.39	4.61 4.60	3576.0 3579.0	10.84	6.95 6.65	0.52	4.56 4.58
3420.0 3423.0	6.05 5.45	4.55 4.26 3.95	0.34	4.62 4.65	3582.0 3585.0	9.65 9.04	6.35 6.04	0.50	4.59 4.59
3426.0 3429.0	4.85 4.25	3.95 3.65	0.30	4.64	3588.0 3591.0	8.43 7.84	5.75	0.48	4.59 4.57
3432.0 3433.0	3.66	3.37 3.25 3.15	0.27 0.27 0.23	4.65	3594.0 3597.0	7.24	5.14	0.40	4.55
3434.0	3.45 3.26	3.15	0.27	4.69	3600.0	6.05	4.83	0.37	4.58
3435.0 3436.0	3.06 3.19	3.06 3.12	0.21 0.20	4.70 4.71	3603.0 3606.0	5.45 4.86	4.26 3.95	0.36	4.61 4.62
3437.0 3438.0	3.39 3.59	3.22 3.34	0.22 0.24	4.71 4.70	3609.0 3612.0	4.26	3.65 3.35	0.30	4.58 4.60
3441.0 3444.0	4.19 4.78	3.62 3.93	0.25	4.68 4.68	3613.0 3614.0	3.45 3.24	3.25 3.16	0.28	4.61 4.63
3447.0	5.39	4.22	0.26	4.67 4.69	3615.0 3616.0	3.05	3.04 3.03	0.27	4.64
3450.0 3453.0 3456.0	5.99 6.59 7.18	4.52 4.82 5.12	0.30 0.32 0.34	4.68	3618.0 3620.0	3.02 3.01 3.02	3.05 3.03	0.27 0.26 0.26	4.66
3459.0	7.78	5.41	0.36	4.63	3622.0	3.02	3.02	0.25	4.64
3462.0 3465.0	8.38 8.97	5.71 6.01	0.37	4.63	3624.0 3630.0	3.03	3.02 3.02	0.25	4.64
3468.0 3471.0	9.57 10.18	6.31 6.60	0.43	4.64 4.64	3640.0 3650.0	3.01 3.02	3.03 3.02	0.25	4.63 4.65
3474.0 3477.0	10.78 11.38	6.91 7.20 7.30	0.49	4.62 4.58	3650.0 3660.0 3670.0	3.02 3.02	3.03 3.04	0.24	4.64 4.64
3478.0 3479.0	11.58	7.30	0.54	4.58	3680.0 3690.0	3.02	3.04 3.03	0.23	4.65 4.64
3480.0 3481.0	11.98 11.84	7.52 7.43	0.54	4.60 4.58	3700.0 3710.0	3.00 3.02	3.02 3.01	0.23	4.65 4.65
3482.0 3483.0	11.64 11.44	7.35	0.55	4.57 4.56	3720.0 3730.0	3.01 3.01	3.02 3.03	0.23	4.65
3486.0	10.84	6.96 6.64	0.50	4.56 4.59	3740.0	3.02 3.02	3.03	0.22	4.65
3489.0 3492.0	9.65	6.35	0.47	4.61	3750.0 3760.0	3.02	3.03 3.03	0.22	4.65
3495.0 3498.0	9.05 8.45	6.07 5.76	0.45	4.60 4.60	3770.0 3780.0	3.01 3.01	3.01 3.02	0.22	4.65 4.65
3501.0 3504.0	7.85	5.45 5.14	0.43	4.58 4.57	3790.0 3800.0	3.02	3.05 3.04	0.22	4.65 4.65 4.65
3507.0 3510.0	6.64 6.05	4.85 4.53	0.39	4.57 4.61	3810.0 3820.0	3.01 3.01	3.03 3.05	0.22	4.65
3513.0 3516.0	5.44 4.84	4.24 3.93	0.34	4.60 4.62	3830.0 3840.0	3.02 3.02	3.06 3.03	0.23 0.21 0.22	4.65 4.64
3519.0 3522.0	4.25 3.64	3.62 3.33	0.31 0.29 0.25	4.60	3850.0 3860.0	3.02 3.01	3.02 3.01	0.22	4.65 4.65
3523.0 3524.0	3.44 3.24	3.23 3.14	0.25 0.24	4.63	3870.0 3880.0	3.02 3.03	3.03 3.05	0.22	4.65
3525.0	3.04	3.03	0.23	4.66	3890.0	3.02	3.04	0.22	4.65
3526.0 3527.0	3.18 3.38	3.10 3.20	0.23	4.66	3900.0 3910.0	3.01 3.00	3.02 3.03	0.21 0.21 0.21	4.64 4.65
3528.0 3531.0	3.58 4.17	3.31 3.62	0.23 0.25	4.66 4.62	3920.0 3930.0	3.00 3.01	3.03 3.02	0.21	4.64 4.65
3534.0 3537.0	4.79	3.90 4.21	0.27	4.62 4.65	3940.0 3950.0	3.02	3.04 3.05	0.21	4.65 4.65
3540.0 3543.0	5.99 6.60	4.54	0.32	4.62 4.62	3960.0 3970.0	3.02 3.02	3.04 3.03	0.21	4.64 4.65
3546.0 3549.0	7.19	4.82 5.12 5.41	0.37	4.64	3980.0 3990.0	3.01	3.03	0.21	4.64
3552.0 3555.0	8.39	5.71 6.01	0.40	4.60 4.60	4000.0	3.00	3.03 3.04	0.22	4.65
3558.0	8.98 9.58	6.31	0.44	4.62	4020.0	3.01	3.02	0.21	4.65
3561.0 3564.0	10.18	6.60 6.91	0.45	4.62	4030.0 4040.0	3.02 3.01	3.02	0.21	4.64
3567.0	11.38	7.21	0.49	4.57	4050.0	3.02	3.03	0.21	4.65

# UNIVERSITÄT DUISBURG ESSEN

Fakultät für Ingenieurwissenschaften Essener Labor für Leichte Flächentra 45141 Essen, Universitätsstr. 15, Tel

test: V11	12	r	material: V	ersidag B180	)89, piece	00980777/	٩04		page: 7
time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongatio [%] fill
4060.0	3.01	3.02	0.22 0.21 0.21 0.21 0.21	4.64	-				
4070.0	3.02 3.02	3.04 3.03	0.21	4.65 4.65				7	
4090.0 4100.0	3.03 3.01	3.02 3.04	0.21	4.64					
4110.0	3.03	3.04	0.22	4.64					
4120.0 4130.0	3.02 3.01	3.03 3.02	0.21	4.65 4.64				2	
4140.0	3.01	3.02	0.22	4.64					
4 150.0 4 160.0	3.02 3.02	3.01 3.02	0.22 0.21 0.22	4.65 4.65					-
4170.0	3.02	3.04	0.21	4.64					
4 180.0 4 190.0	3.03 3.01	3.02 3.05	0.22	4.64					
4200.0	3.02	3.02	0.22	4.64					
4206.0 4208.0	3.01 3.01	3.02 3.01	0.21	4.63 4.64				1	1
4210.0	3.01	3.01	0.22	4.63					
4212.0 4214.0	3.01 3.01	3.01 3.01	0.22	4.64					
4216.0	2.84	2.85	0.22	4.63					
4217.0	2.64	2.65	0.22	4.62					
4218.0 4219.0	2.44 2.24	2.45 2.25	0.21 0.20	4.63					
4220.0 4221.0	2.03	2.06 1.85	0.23	4.60 4.54				2	
4222.0	1.64	1.66	0.21	4.57					
4223.0 4224.0	1.44	1.46 1.25	0.21	4.50 4.51					
4224.0	1.24	1.25	0.22	4.46					
4226.0 4227.0	0.84	0.85	0.23	139					
4228.0	0.44	0.46	0.23	4.35 4.25 4.15					
4229.0 4230.0	0.24	0.25 0.12	0.17	4.15 4.03					
4231.0	0.10	0.12	0.11	3.98				1	
4232.0 4233.0	0.11	0.12	0.09	3.97 3.93					
4234.0	0.12	0.12	0.08	3.91					
4235.0	0.11	0.13	0.09	3.89					
								1	
						-			
								2	
						-			



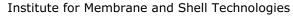
n - Abteilur	ng Bauwissenschaften
agwerke	ELLF
el.: 0201/18	33-4223, Fax: -4276

# Measured data of bi-axiale tensile test

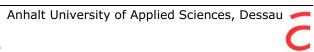
5	$\cap$	)9	മറ	7	7	7.	۵n	Λ	
-	5	20	00		1	"	70	Ξ.	

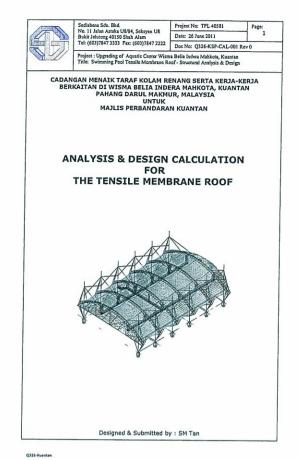


# **11.12 DESIGN CALCULATION**









(MARKED)	Sediabena Sdn. Bhd.	Project No: TPL 40581	Page:
1 A	No. 11 Jalan Astaka U8/84, Seksyen U8 Bukit Jelutong 40150 Shah Alam	Date: 26 June 2011	2
Mean Long	Tel: (603)7847 3333 Fax: (603)7847 2222	Doc No: Q326-KSP-CAL-00	Rev 0
	Project : Upgrading of Aquatic Center Wisn Title: Swimming Pool Tensile Membrane R		
TABLE OF CO	ONTENTS		PAGES
1 1. 1. 1.	ENERAL 1 INTRODUCTION 2 STRUCTURAL SYSTEM 3 SCOPE OF DOCUMENT 4 REFERENCE DOCUMENT 5 UNITS 6 DESIGN CODE & STANDARD		4 - 9
2. AN 2. 2.	ALYSIS AND DESIGN CRITERIA 1 COORDINATES SYSTEM 2 METHOD OF ANALYSIS 3 STRUCTURAL STEEL DESIGN 4 STEEL MATERIAL	MODEL	10 - 12
3. 3. 3. 3.	2 DEAD LOAD OF CATWALK		13 - 19
4. BA 4. 4. 4.	2 LOAD COMBINATION FOR SER	VICE LIMIT STATE	20 - 21
5. BO	UNDARY CONDITION		22
6. DE	SIGN OF STEEL MEMBERS		23 - 26
7. DE	SIGN OF CABLES		27
8. DE:	SIGN OF HOLDING DOWN BOLT		28 - 30
9. DE	SIGN OF CONNECTIONS		31 - 32
	<ul> <li>REACTIONS, REACTION SUMM</li> <li>STEEL DESIGN CHECK</li> <li>STEEL NODE NUMBER CORRES</li> <li>POINT</li> </ul>	ARY & ENVELOPE	a1 - a90 a91 a92 - a98 a99 - a20 a203 a204

TEN	Sediabena Sdn. Bhd. No. 11 Jalan Astaka U8/84, Seksyen U8	Project No: TPL 40581	Page:
E D	Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Date: 26 June 2011	
IN A		Doc No: Q326-KSP-CAL-00	
	Project : Upgrading of Aquatic Center Wister Title: Swimming Pool Tensile Membrane Re	aa Belia Indera Mahkota, Kuant oof - Structural Analysis & Desi	an Ign
TABLE OF CO	NTENTS		PAGES
11. AP	PENDIX B - FABRIC STATIC OUTF		
B1.	EDGE PANEL NEXT TO DIVING	S POOL	
	FABRIC NODE NUMBER LAYO	UT PLAN	b1
	<ul> <li>PRESTRESS LOAD CASE</li> <li>LIVE LOAD CASE</li> </ul>		b2 - b4 b5 - b7
	- WIND UPLIFT		b8 - b10
	<ul> <li>WIND PRESSURE</li> </ul>		b11 - b1
	<ul> <li>WIND FROM ENTRANCE</li> </ul>		b14 - b10
	<ul> <li>WIND FROM AUDIENCE ST</li> </ul>	AND	b17 - b19
B2.			
	<ul> <li>FABRIC NODE NUMBER LAYOL</li> <li>PRESTRESS LOAD CASE</li> </ul>	JT PLAN	b20 b21 - b23
	- LIVE LOAD CASE		b21 - b23
	- WIND UPLIFT		b27 - b29
	<ul> <li>WIND PRESSURE</li> </ul>		b30 - b32
	<ul> <li>WIND FROM ENTRANCE</li> </ul>		b33 - b35
	<ul> <li>WIND FROM AUDIENCE ST.</li> </ul>	AND	b36 - b38
B3.	EDGE PANEL NEXT TO SCORE FABRIC NODE NUMBER LAYOU		100
	- PRESTRESS LOAD CASE	JI PLAN	b39 b40 - b42
	- LIVE LOAD CASE		b43 - b45
	<ul> <li>WIND UPLIFT</li> </ul>		b46 - b48
	- WIND PRESSURE		b49 - b51
	<ul> <li>WIND FROM ENTRANCE</li> <li>WIND FROM AUDIENCE ST/</li> </ul>	AND	b52 - b54 b55 - b57
	ENDIX C - TECHNICAL DATA		
C1. C2.		B18089	c1 - c2 c3 - c4
		516665	23 - 24

 Scelishems San, Blid.
 Project No: TPL 40581
 1 = mail

 No. 11 Jain Artaka UBPA, Seksyen UB Buki: delutore, 40150 Shah Alam
 Date: 26 June 2011
 Date: 26 June 2011

 Tel: (603)7847 3333 Fax: (603)7847 2222
 Doc No: Q326/KSP-CAL-001 Rev 0
 Date: 26 June 2011
 Date: 26 June 2011

Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

The steel roof structure comprise of 6 nos of 3D triangulated truss of 1 top chord 15.m height and 2 bottom chord of 1.7m wide. These trusses are spaced at 16.5m and integrated with steel column at 54m center. The overall length of the

Due to site access and constraint, the steel structure is designed such that it will be able to be lifted by a small tonnage crane eg. 30 tons and so bolted

The 64m truss is then make into 4 segment with flange joint connection. The 30m high column is also flange jointed just before and after the 3D truss. So is the bracing and ties along the columns, at the end canopies are assembled in parts by

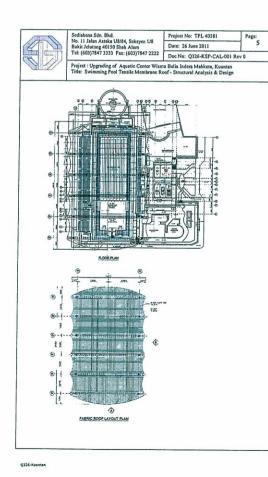
truss is 64m with 11.6m rise at the center. Each of these integrated truss with column height of 30m is stabilized with 1 front stay and 2 upper and lower backstay The stability of the structure is dependent on ties and bracing along the column longitudinally. They are also tied quarterly at 3 locations across the bottom chord of the trusses. At the upper part of the column, a pair of crossly brace safety cable is introduced.

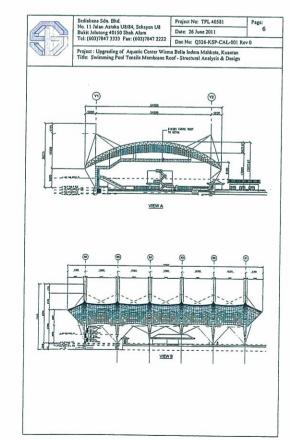
1.2 STRUCTURAL SYSTEM

tion is decided

bolting system.

Q326-Kuantan





Q326-Kuantan

TAN SIEW MOI



-

SECTION A1 - A1

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES



## Scélabona Sdri, Bhd. Project Ne: 11 to the state. No. 11 Julin Aratika U024, Sckopen UE Date: 26 June 2011 Date: 26 June 2011 Date: 26 June 2011 Det: 6603)714/7 3333 Fax: (603)714/7 2222 Dec No: 0226/KSP-CAL001 Rev. Page: Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Desig

1. GENERAL

### 1.1 INTRODUCTION

The proposed tensile fabric roof structure is part of the upgrading work over the existing Wisma Belia Indera Mahkota swimming pool complex at Kuantan. It is the aquatic vents venue for the 15<sup>th</sup> Malaysia Games held in Kuantan, Pahang Darul Makmur from 7<sup>th</sup> July to 16<sup>th</sup> July 2012.

The PTFE (polytetrafluoroethylene) coated glass fiber roof covered a main competition pool of 21m x 50m and a diving pool of 15m x 20m, both are of olympic standard. The membrane used is B18089 of Verseidag, Germany. The foot print of the roof is approximately 100m x 64m on plan.

The swimming pool roof is a barrel vault like structure of 82.5m length with both end a 9m cantilevered eyelid canopy which is about 24 deg tilted down vard.

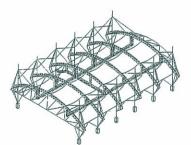
The steel roof structure comprise of 6 nos of 3D triangular truss spaced at 16.5m Each truss is integrated with steel mast at 54m center to center at both end. The overall height of columns are 30m and top of truss is 22m above the general pool level respectively. These columns are stabilized with frontstay and upper and lower backstay. There are 1 column near the main entrance which 'punch' through the roof of the VIP room. The overall structure are braced longitudinally along the column gridline and also 3 tie beam at 3 location of bottom chord of the 3D truss. The base of column mast is then fixed to RC stump of 2.8m above the general pool

Approximately 220m run of 1.2m wide catwalk is hanged from these 3D truss at 15 location to provide access for maintenance of light fitting which is also fixed on the railing of catwalk.

The fabric roof consist of 5 internal panel and 2 end panel of approximately 6000m<sup>2</sup> area in total. The internal fabric panel is secured across the bottom chord of 2 nos of 3D truss and inside of the triangular truss is then fixed with polycarbonate.

APPEND	Sediabena Sdn. Bhd.	Project No: TPL 40581	Page:		
	No. 11 Jalan Astaka U8/84, Seksyen U8 Bukit Jelutong 40150 Shah Alam	Date: 26 June 2011	8		
	Tel: (603)7847 3333 Fax: (603)7847 2222	Doc No: Q326-KSP-CAL-001 Rev 0			
	Project : Upgrading of Aquatic Center Wism Title: Swimming Pool Tensile Membrane Ro	na Belia Indera Mahkota, Kuantan			

The 3D trusses is also providing supports to about 220m run of catwalk at 15 location of general 4 hanging point each. There are 2 row of 82.5m long catwalk at 15 location of general 4 hanging point each. There are 2 row of 82.5m long catwalk parallel to and about 15m high from the swimming pool. Between these catwalk, there is interconnecting link along gridline X4. The catwalk is approximately 1.2m wide x 1.2m high.



3D VIEW OF CATWALK WITH STEEL TRUSS

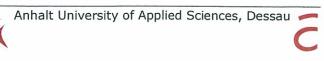
### 1.3 SCOPE OF DOCUMENT

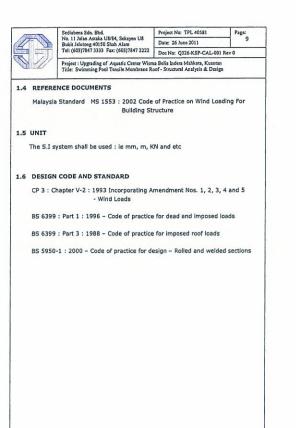
This document details the structural analysis and design of the steel roof cture with the fabric roof cover when in placed and subject to applied loading.

For ease of this analysis, secondary structure like catwalk etc are not modeled n the design model. A separate design check is done.

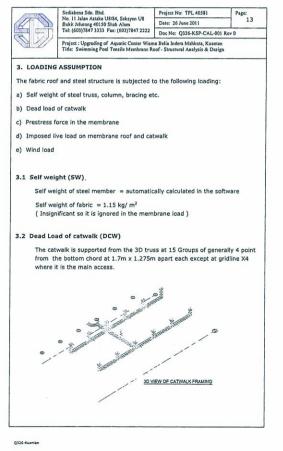
The design of the foundation and RC stump to resist the forces from the roof tructures is exclude in this document as it is not included in the roof contract.

Q326-Kuantan





Q326-Kuantan



Autor	Sediabena Sdn. Bhd.	Project No: TPL 40581	Page:			
(IFN)	No. 11 Jalan Astaka U8/84, Seksyon U8 Bukit Jelutong 40150 Shah Alam	Date: 26 June 2011	10			
	Tel: (603)7847 3333 Fax: (603)7847 2222	Doc No: Q326-KSP-CAL-001 Rev 0				
	Project : Upgrading of Aquatic Center Wism Title: Swimming Pool Tensile Membrane Ro	na Belia Indera Mahkota, Kuanta 00f - Structural Analysis & Desig	1			

2.1 COORDINATES SYSTEM The design model structural axis system is as follow:

- +X from arid line X6 to X1
- +Y from grid line Y2 to Y1
- +Z vertically up

### 2.2 METHOD OF ANALYSIS

The analysis of the tensioned membrane structure is done in two parts. Firstly is to do the form finding of the membrane. Then by using the forces from the static analysis of the prestressed membrane and applied to the steel structure and do a design check of the steel structure.

### 2.2.1) Fabric Roof

The task of determining appropriate forms of the membrane based on the given outline is using the software EASY from Germany.

The EASY form finding method is based on the method of force density algorithm. After the equilibrium shape is formed, the form is then applied with external load, ie imposed load, wind load and etc. and static analysis of the fabric is then carried out

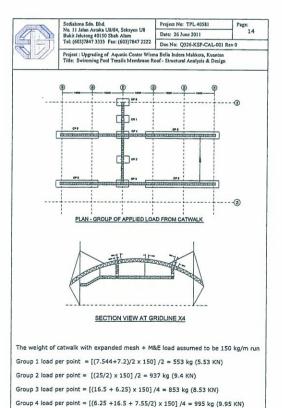
External load which will be applied to the surface of the membrane will be epresented by nodal forces.

2.2.2) Structural Steel System

The output forces from the membrane for all the load case from EASY is then extract for use as input forces to the structural steel and then for design purposes.

The finite element software used for the steel analysis is STAAD PRO2007, leveloped by Research Engineers International, USA.

Q326-Kuantar



Group 5 load per point = (16.5x150) /4 = 618 kg (6.2 KN)

Q326-Kuantan

Group 6 load per point =  $[(7.544/2 + 3.3) \times 150]/2 = 530 \text{ kg} (5.3 \text{ KN})$ 



frontstay, backstay, ties between truss, bracings between column. These are assumed to be truss member which will have a bolted connection at both end.

The stabilizing cable between top of mast are assumed to be tension only Member with solid round bar representing the cables.

w;		reference, the steel member of the design model has been g
a)		
b)	member	457 to 536 = edge member of eyelid canopy
		537 to 782 = bottom horizontal chord of 3D truss
d)	member	783 to 992 = top curved chord of 3D truss
		993 to 1928 = diagonal chord of 3D truss
f)		1929 to 1962 = bracing and prop member to eyelid canop
g)		1963 to 1977 = tie member between 3D truss
		1978 to 2041 = lower, intermediate and upper mast
i)	member	2042 to 2061 = tie member at between lower masts
j)	member	2062 to 2077 = mast front stay
k)		2078 to 2193 = mast backstay
1)		2194 to 2227 = internal short tie of backstay
m)	member	2228 to 2255 = longitudinal bracing between lower mast
n)	member	2256 to 2275 = stabilizing cable at intermediate mast
		1 Atri
		NT STOR
	E	
	in the second	A THE
	100	A ATA I A
	5.4	XAVE STY
		A A A A A A A A A A A A A A A A A A A
		W/ a
		7 B
	d.	

Q326-Kuantar



### 3.3 Prestress Load (PRE)

Prestress is induced to increase membrane stiffness and obtain a stable form which is in equilibrium. In this case, a prestress force of 3KN/m is assumed.

3.4 Imposed Live Load

Q326-Kuantan

3.4.1) Membrane roof (VL) Imposed live load on membrane roof = 0.25 KN/m<sup>2</sup> This load is applied vertically downward to the fabric roof.

3.4.2) Catwalk (LCW)

For localized catwalk design, assumed live load = 1.5  ${\rm KN/m^2}$ 

For global analysis of the structure roof, assumed live load applied simultaneously on all catwalk = 0.75  $\rm KN/m^2$ 

Using the same loading group as in the dead load case, Live load = 0.75 KN/m<sup>2</sup> x 1.2m internal clearance of catwalk = 0.9 KN/m

Group 1 load per point = [(7.544+7.2)/2 x 0.9] /2 = 3.32 KN Group 2 load per point = [(25/2) x 0.9] /2 = 5.62 KN Group 3 load per point =  $[(16.5 + 6.25) \times 0.9]/4 = 5.12$  KN Group 4 load per point = [(6.25 +16.5 + 7.55/2) x 0.9] /4 = 5.96 KN Group 5 load per point = (16.5x0.9) /4 = 3.71 KN

Group 6 load per point =  $[(7.544/2 + 3.3) \times 0.9]/2 = 3.18$  KN

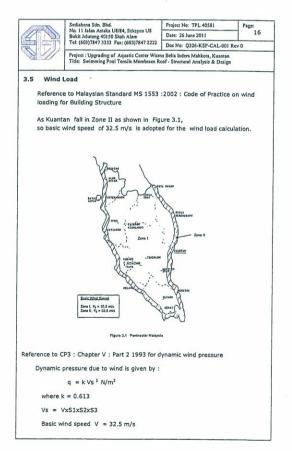


ATTEN	Sediabena Sdn. Bhd.	Project No: TPL 40581	Page:				
T	No. 11 Jalan Astaka U8/84, Seksyen U8 Bukit Jelutong 40150 Shah Alam	Date: 26 June 2011	12				
	Tel: (603)7847 3333 Fax: (603)7847 2222	Doc No: Q326-KSP-CAL-001 Rev 0					
	Project : Upgrading of Aquatic Center Wism Title: Swimming Pool Tensile Membrane Ro						
The follo	wing properties is used for the analy	vsis on the steel membe	er: -				
Young's I	Modulus = 2.10E08KN/m <sup>2</sup>						
	$dulus = 8.0E07 \text{ KN/ m}^2$						
Poisson F	Ratio = 0.3						
Mass den	sity of steel = 7850 kg/m <sup>3</sup>						
Gravitati	onal acceleration = 9.81 m/s <sup>2</sup>						
Coefficien	nt of thermal expansion = 11.7E-06	/deg C					
Circular I	y the following steel material or equ nollow section to BS EN 10210 S27 BS EN 10025 S275 or equal						
The choic	e of material used will be subject to	availability of material					
	e for the analysis and design of the 275 N/mm <sup>2</sup> .	structure steel roof, ass	umed yield				
2.5 DESIGN	N METHOD						
	n-placed analysis there will be 2 limi nate limit state.	t state analysis, service	limit state				
The servi	ce limit state relate to performance	under normal service of	onditions, e.				

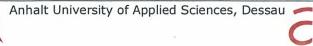
deflections. And ultimate limit state are related to safety and load carrying capacity of the structure where the specified loads is multiplied by relevant partial factor.

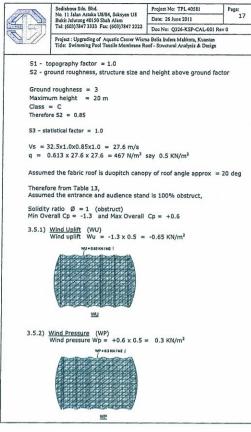
The design facility available in STAADPRO software shall be used to code check the members for member forces and mement due to the various loading combinations for both limit states.

Q326-Kuantan



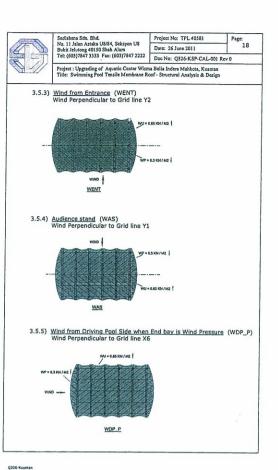
Q326-Kuant

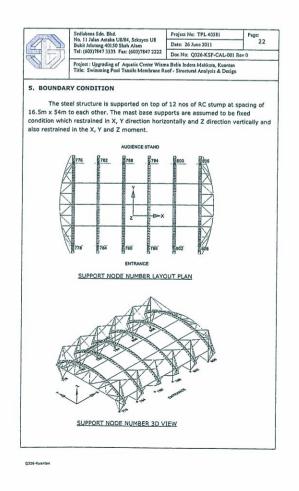


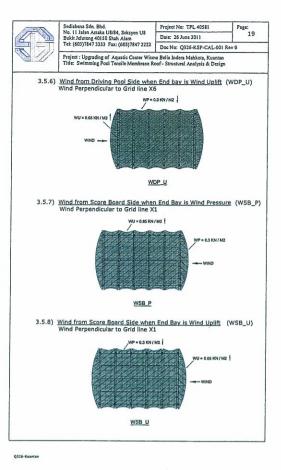


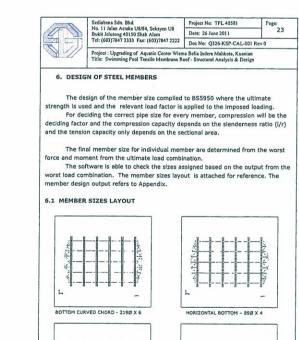
Q326-Kuantan

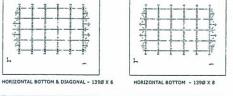
( allow )	Sediabe	ma Sdn. Bhd.	Project No: TPL 40581	Page:			
	No. 11 Bukit J	Jalan Astaka U8/84, Seksyen U8 elutong 40150 Shah Alam	Date: 26 June 2011	21			
Man Hang	Tel: (60	03)7847 3333 Fax: (603)7847 2222	Doc No: Q326-KSP-CAL-001 Rev 0				
		: Upgrading of Aquatic Center Wisn Swimming Pool Tensile Membrane R					
4.2 SERVIC	E LOAD	COMBINATION					
LOAD 1	00 =	SW + DCW + PRE					
LOAD 1	01 =	SW + DCW + LCW + VL					
LOAD 1	02 =	SW + DCW + WU					
		SW + DCW + WP					
		SW + DCW + WENT					
		SW + DCW + WAS					
LOAD 1	06 =	SW + DCW + WDP_P					
		SW + DCW + WDP_U					
		SW + DCW + WSB_P					
LOAD 1	09 =	SW + DCW + WSB_U					
1.2 111 TTMA	TE LOA	D COMBINATION					
1.5 OLITIMA		COMBINATION					
LOAD 2	= 00	1.4(SW + DCW+PRE)					
LOAD 2	01 =	1.4(SW+DCW) + 1.6(LCW	(+VL)				
		1.0(SW + DCW) + 1.4WU					
		1.2(SW + DCW) +1.2WP					
		1.2(SW + DCW) + 1.2(WE					
		1.2(SW + DCW) + 1.2(WA)					
		1.2(SW + DCW) + 1.2(WD					
		1.0(SW + DCW) + 1.4(WD					
		1.2(SW + DCW) + 1.2(WS					
LOAD 2	19 =	1.0(SW + DCW) + 1.4(WS	(B_U)				
The design	of the i	member sizes are based or	the above load combin	ation.			











Q326-Kuantan

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

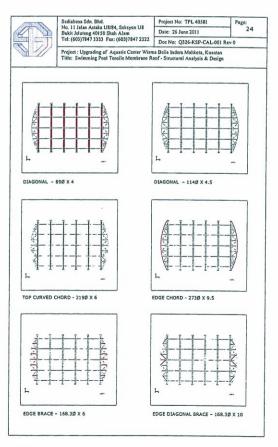
TAN SIEW MOI

Q326-Kuantar

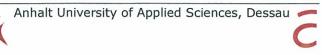


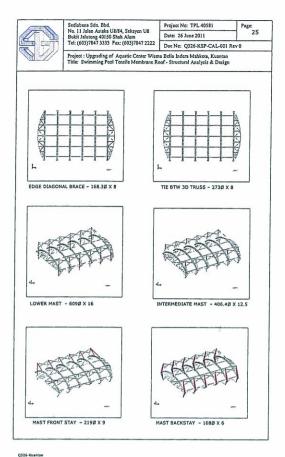
Sediabena Sdn. Bhd.	- 110	Project No: TPL 40581	Page:
No. 11 Jalan Astaka U8/84, Seksye Bukit Jelutong 40150 Shah Alam		Date: 26 June 2011	20
Tel: (603)7847 3333 Fax: (603)784	47 2222	Doc No: Q326-KSP-CAL-001	Rev 0
Project : Upgrading of Aquatic Ce Title: Swimming Pool Tensile Mer	nter Wisn mbrane R	a Belia Indera Mahkota, Kuantan bof - Structural Analysis & Desig	1 a
BASIC LOAD CASES & LOAD COME	INATI	ON	
The membrane roof and steel stru	cture s	ystem are analyzed bas	ed on the
ollowing load cases and load combination	ns.		
A.1 BASIC LOAD CASES			
LOAD 1 (SW) = Self weight of stee software	l struct	ure automatically calcul	ated by the
LOAD 2 (DCW) = Dead load of cat	walk +	ME load	
LOAD 3 (LCW) = Imposed Live Loa	ad on c	atwalk	
LOAD 4 (PRE) = Prestress load fro load	om mer	nbrane roof WITHOUT a	any externa
The following external load is app			
nembrane form. So the following load ca	se actu	ally consist of prestress	ing load.
LOAD 5 (VL) = Imposed Live Load	on me	mbrane roof	
LOAD 6 (WU) = Wind Uplift on men	nbrane	roof	
LOAD 7 (WP) = Wind Pressure on n	nembra	ne roof	
LOAD 8 (WENT) = Wind from Entra	nce sid	e (Y2)	
LOAD 9 (WAS) = Wind from Audio	ence Si	and (Y1)	
LOAD 10 (WDP_P) = Wind from Dri	ving Po	ol side (X6), End bay wi	nd pressure
LOAD 11 (WDP_U) = Wind from Dri	ving Po	ool side (X6), End bay w	ind uplift
LOAD 12 (WSB_P) = Wind from Sc	ore Boa	ard side (X1), End bay w	ind pressur
LOAD 13 (WSB_U) = Wind from Sco	ore Boa	rd side (X1), End bay w	ind uplift
And all the above load case are unfact	tored lo	ad.	

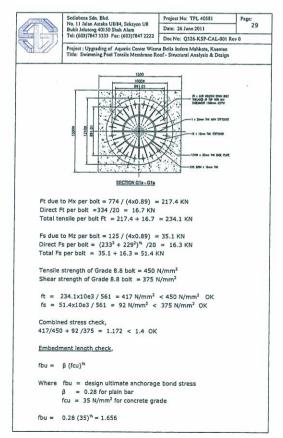
Q326-Kuantan

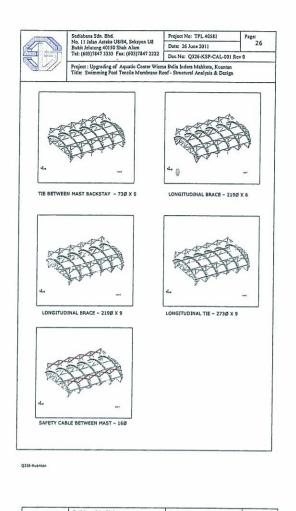


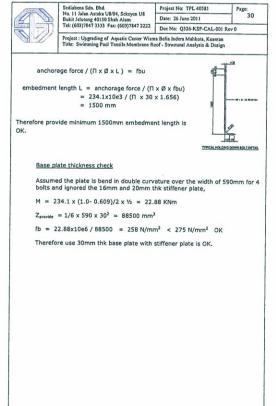
Q326-Kuantar



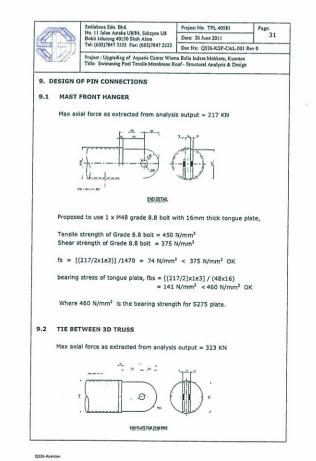




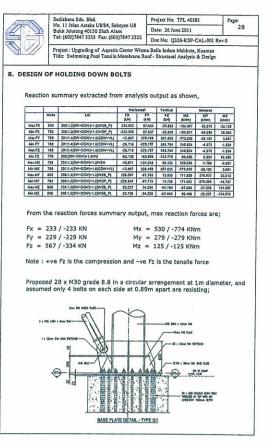




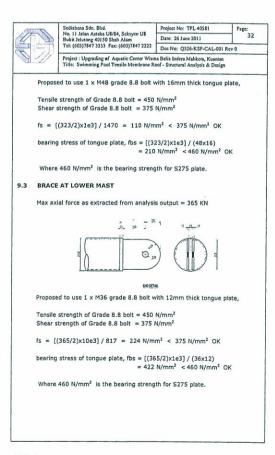
15	Sediabena Sdn. Bhd. No. 11 Jalan Astaka U8/84, Seksyen U8	Project No: TPL 40581	Page:							
Ľ	Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Date: 26 June 2011								
F	Tel: (603)/64/ 3333 Fax: (603)/84/ 2222	Doc No: Q326-KSP-CAL-001	Rev 0							
A	Project : Upgrading of Aquatic Center Wism Title: Swimming Pool Tensile Membrane Re	a Belia Indera Mahkota, Kuantan xof - Structural Analysis & Desig								
7. [	DESIGN OF CABLES									
7.1	STABILIZING CABLE AT TOP OF MAS	г								
	From the steel structure analysis output,									
	maximum axial force = 30 KN									
	Proposed to use 16mm Ø 1x19 galvanize	d steel wire rope								
	Min breaking load = 211 KN >>30	KN								
	Therefore is ok to use 16mm Ø wire rope	•								
7.2	MEMBRANE BORDER CABLE									
	From the membrane static output for the internal panel,									
	Prestress load case , cable force = 47 KN Imposed live load, cable force = 20 KN Wind Uplift case, cable force = 250 KN Wind pressure case, cable force = 35 KN Wind from Entrance (one side uplift & o Wind from grandstand (one side pressure	I ne side pressure) = 184								
	maximum unfactored tension force in the	border cable = 250 K	N from Wi							
	Proposed to use 28mm Ø 6 x 37 IWRC ga	Ivanized steel wire rope	,							
	Min breaking load = 49600 kg = 50	6 KN								
	Safety factor = 506 / 250 = 2.024									
	Therefore is ok to use 28mm Ø wire rope									



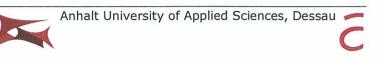
Q326-Kuantar

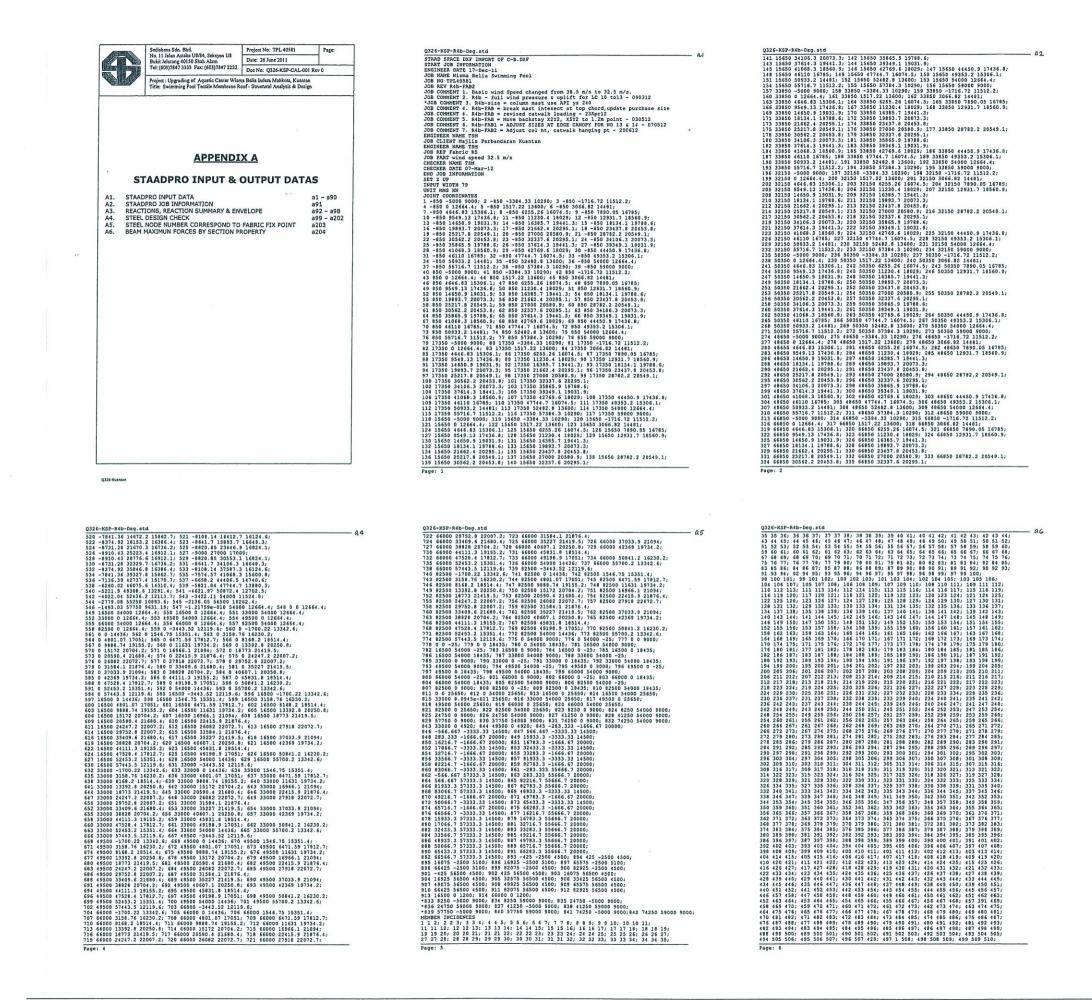


Q326-Kuantan



Q326-Kuantan





	G-KSP-R4b-Deg.std	a
336	66850 34106.3 20073.3; 337 66850 35865.9 19788.6;	- 4
338	66850 37614.3 19441.3; 339 66850 39349.1 19031.9; 66850 41068.3 18560.9; 341 66850 42769.6 18029; 342 66850 44450.9 17436.8;	
343	66850 46110 16785; 344 66850 47744.7 16074.5; 345 66850 49353.2 15306.1;	
46	66850 50933.2 14481; 347 66850 52482.8 13600; 348 66850 54000 12664.4;	
152	66850 55716.7 11512.2; 350 66850 57384.3 10290; 351 66850 59000 9000; 65350 -5000 9000; 353 65150 -3384 33 10290; 354 65150 -1216 22 11512 2;	
55	65150 -5000 9000; 353 65150 -3384.33 10290; 354 65150 -1716.72 11512.2; 65150 0 12664.4; 356 65150 1517.22 13600; 357 65150 3066.82 14481;	
858	65150 4646.83 15306.1; 359 65150 6255.26 16074.5; 360 65150 7890.05 16785;	
61	65150 9549.13 17436.8; 362 65150 11230.4 18029; 363 65150 12931.7 18560.9;	
366	65150 14650.9 19031.9; 365 65150 16385.7 19441.3; 65150 18134.1 19788.6; 367 65150 19893.7 20073.3;	
668	65150 21662.4 20295.1; 369 65150 23437.8 20453.8;	
370	65150 25217.8 20549.1; 371 65150 27000 20580.9; 372 65150 28782.2 20549.1;	
73	65150 30562.2 20453.8; 374 65150 32337.6 20295.1; 65150 34106.3 20073.3; 376 65150 35865.9 19788.6;	
375	65150 37614.3 19441.3; 378 65150 39349.1 19031.9;	
379	65150 41068.3 18560.9; 380 65150 42769.6 18029; 381 65150 44450.9 17436.8;	
82	65150 46110 16785; 383 65150 47744.7 16074.5; 384 65150 49353.2 15306.1;	
885	65150 50933.2 14481; 386 65150 52482.8 13600; 387 65150 54000 12664.4;	
888	65150 55716.7 11512.2; 389 65150 57384.3 10290; 390 65150 59000 9000; 83350 -5000 9000; 392 83350 -3384.33 10290; 393 83350 -1716.72 11512.2;	
94	83350 0 12664.4; 395 83350 1517.22 13600; 396 83350 3066.82 14481;	
97	83350 0 12664.4; 395 83350 1517.22 13600; 396 83350 3066.82 14481; 83350 4646.83 15306.1; 398 83350 6255.26 16074.5; 399 83350 7890.05 16785;	
00	83350 9549.13 17436.8; 401 83350 11230.4 18029; 402 83350 12931.7 18560.9;	
03	83350 14650.9 19031.9; 404 83350 16385.7 19441.3; 83350 18134.1 19788.6; 406 83350 19893.7 20073.3;	
07	83350 21662.4 20295.1; 408 83350 23437.8 20453.8;	
09	83350 25217.8 20549.1; 410 83350 27000 20580.9; 411 83350 28782.2 20549.1;	
12	83350 30562.2 20453.8; 413 83350 32337.6 20295.1;	
14	83350 34106.3 20073.3; 415 83350 35865.9 19788.6; 83350 37614.3 19441.3; 417 83350 39349.1 19031.9;	
18	83350 41068.3 18560.9; 419 83350 42769.6 18029; 420 83350 44450.9 17436.8;	
21	83350 46110 16785; 422 83350 47744.7 16074.5; 423 83350 49353.2 153061;;	
24	83350 50933.2 14481; 425 83350 52482.8 13600; 426 83350 54000 12664.4; 83350 55716.7 11512.2; 428 83350 57384.3 10290; 429 83350 59000 9000;	
30	81650 -5000 9000: 431 81650 -3384.33 10290; 432 81650 -1716.72 11512.2:	
33	81650 -5000 9000; 431 81650 -3384.33 10290; 432 81650 -1716.72 11512.2; 81650 0 12664.4; 434 81650 1517.22 13600; 435 81650 3066.82 14481;	
36	81650 4646.83 15306.1; 437 81650 6255.26 16074.5; 438 81650 7890.05 16785;	
39	81650 9549.13 17436.8; 440 81650 11230.4 18029; 441 81650 12931.7 18560.9; 81650 14650.9 19031.9; 443 81650 16385.7 19441.3;	
44	81650 18134.1 19788.6; 445 81650 19893.7 20073.3;	
46	81650 21662.4 20295.1; 447 81650 23437.8 20453.8;	
48	81650 25217.8 20549.1; 449 81650 27000 20580.9; 450 81650 28782.2 20549.1; 81650 30562.2 20453.8; 452 81650 32337.6 20295.1;	
53	81650 34106.3 20073.3; 454 81650 35865.9 19788.6;	
55	81650 37614.3 19441.3; 456 81650 39349.1 19031.9;	
57	81650 41068.3 18560.9; 458 81650 42769.6 18029; 459 81650 44450.9 17436.8;	
60	81650 46110 16785; 461 81650 47744.7 16074.5; 462 81650 49353.2 15306.1; 81650 50933.2 14481; 464 81650 52482.8 13600; 465 81650 54000 12664.4;	
66	81650 55716.7 11512.2; 467 81650 57384.3 10290; 468 81650 59000 9000;	
69	83993 -3750 9631.19; 470 84636.1 -2500 10262.4; 471 85279.1 -1250 10893.6;	
72	85922.1 0 11524.8; 473 86522 1563.81 12113.7; 474 87122 3127.63 12702.5;	
75	87721.9 4691.45 13291.4; 476 88321.8 6255.26 13880.3; 88760 7924.37 14310.4; 478 89198.2 9593.47 14740.6;	
79	89636.4 11262.6 15170.7; 480 90074.6 12931.7 15600.8;	
81	90341.4 14672.2 15862.7; 482 90608.1 16412.7 16124.6;	
83	90874.9 18153.2 16386.4; 484 91141.7 19893.7 16648.3; 91231.3 21670.3 16736.2; 486 91320.9 23446.9 16824.1;	
85	91231.3 21670.3 16736.2; 486 91320.9 23446.9 16624.1; 91410.4 25223.4 16912.1; 488 91500 27000 17000;	
89	91410.4 28776.6 16912.1; 490 91320.9 30553.1 16824.1;	
91	91231.3 32329.7 16736.2; 492 91141.7 34106.3 16648.3;	
93	90874.9 35846.8 16386.4; 494 90608.1 37587.3 16124.6;	
97	90341.4 39327.8 15862.7; 496 90074.6 41068.3 15600.8; 89636.4 42737.4 15170.7; 498 89198.2 44406.5 14740.6;	
99	88760 46075.6 14310.4; 500 88321.8 47744.7 13880.3;	
01	87721.9 49308.6 13291.4; 502 87122 50872.4 12702.5;	
03	86522 52436.2 12113.7; 504 85922.1 54000 11524.8;	
08	85279.1 55250 10893.6; 506 84636.1 56500 10262.4; 507 83993 57750 9631.19; -1493.03 -3750 9631.19; 509 -2136.05 -2500 10262.4;	
10	-2779.08 -1250 10893.6; 511 -3422.11 0 11524.8; -4022.04 1563.81 12113.7; 513 -4621.97 3127.63 12702.5;	
12	-4022.04 1563.81 12113.7; 513 -4621.97 3127.63 12702.5;	
14	-5221.9 4691.45 13291.4; 515 -5021.84 6255.26 13880.3; -6260.02 7924.37 14310.4; 517 -6698.2 9593.47 14740.6;	
	-5260.02 7924.37 14310.4; 517 -6598.2 9593.47 14740.6; -7136.39 11262.6 15170.7; 519 -7574.57 12931.7 15600.8;	

500	5	10	511	501	511	512:	502	512	513:	503	513	514:	504	514	515:	505	515	516;
506	5	16	517	507	517	518:	508	518	519;	509	519	520;	510	520	521:	511	521	522:
512	5	22	523	513	523	524;	514	524	525;	515	525	526;	516	526	527;	517	527	528;
518	5:	28	529;	519	529	530;	520	530	531;	521	531	532;	522	532	533;	523	533	522; 528; 534;
524	5:	34	535;	525	535	536;	526	536	537;	527	537	538;	528	538	539;	529	535	540;
530	5	10	541;	531	541	542;	532	542	543;	533	543	544;	534	544	545;	535	545	546;
536	5	16	39;	537	1 40	; 538	2 4	1; 5	39 3	42;	540	5 44;	541	6 4	5; 54	2 46	7;	127
543	8	47	; 54	4 9	48;	545 1	0 49	; 54	6 11	50;	547	12 51	; 54	8 13	52;	549	53 1	4;
550	2	1	5; ;	51 5	5 16	; 552	17	56;	553 5	/ 18	; 55	4 58	19;	555	59 20	; 55	6 60	21;
501	6		2: :	58 6	2 23	, 566	20	247	560 6 567 3	9 23	56	0 30	20;	560	37 74	: 50	0 25	28;
571	3	1 7	3. 6	72 7	2 33	, 573	71	32.	574 7	9 11	R . 5	75 80	119	. 57	6 81	120.	0 33	
577	8	3 1	22:	578	84 1	23: 5	79 1	24 8	5; 58	0 86	125	: 581	87	126:	582	88 1	27:	
583	8	9 1	28;	584	90 1	29: 5	85 9	1 13	0: 58	6 13	1 92	; 587	132	93;	588	133	94:	
589	9	5 1	34 :	590	135	96: 5	91 1	36 9	7: 59	2 13	7 98	: 593	138	99:	594	139	100:	
595	14	10	101;	596	141	102;	597	142	103; 109; 111;	598	143	104;	599	144	105;	600	145	106;
601	14	16	107;	602	147	108;	603	148	109;	604	117	156;	605	116	155;	606	115	154;
607	11	13	152;	608	112	151;	609	150	111;	610	149	110;	611	157	196;	612	158	197;
613	1	59	198;	614	161	200;	615	162	201;	616	202	163;	617	164	203;	618	165	204;
619	10	56	205;	620	167	206;	621	168	207;	622	169	208;	623	209	170;	624	210	171;
		17	172;	626	1/3	212;	627	213	174; 180;	628	214	101	629	215	1/6;	630	216	177;
631	21	12	104	632	218	1/9;	633	219	180;	640	220	197.	641	105	182;	030	10-	183;
643	14	3	104;	644	191	230-	645	190	229;	644	220	189.	647	227	180.	640	235	233;
649		16	275.	650	237	276.	651	239	278;	652	240	279.	653	280	241.	654	242	281.
655		13	282	656	244	283	657	245	284;	658	246	285	659	247	286	660	287	248:
661	21	88	249:	662	289	250;	663	251	290;	664	291	252;	665	292	253;	666	293	254:
667	25	14	255;	668	295	256;	669	296	257;	670	297	258;	671	298	259;	672	299	260:
673		00	261;	674	301	262;	675	302	263;	676	303	264;	677	304	265;	678	273	312;
679	27	12	311;	680	271	310;	681	269	308;	682	268	307;	683	306	267;	684	305	266;
685	31	13	352;	686	314	353;	687	315	354;	688	317	356;	689	318	357;	690	358	319;
691	32	20	359;	692	321	360;	693	322	361; 328;	694	323	362;	695	324	363;	696	325	364;
697	36	55	326;	698	366	327;	699	367	328;	700	329	368;	701	369	330;	702	370	331;
703	37	1	332;	704	372	333;	705	373	334;	706	374	335;	707	375	336;	708	376	337;
709	37	7	338;	710	378	339;	711	379	340;	712	380	341;	713	381	342;	714	382	343;
715	35	1	390;	716	350	389;	717	349	388;	718	347	386;	719	346	385;	720	384	345;
721	38	3	344;	722	391	430;	723	392	431; 438;	724	393	432;	725	395	434;	726	396	435;
121	1.	D	397;	728	398	43/1	129	399	438;	730	400	4357	731	101	440;	732	402	441;
733	1	13	4927	734	440	4104;	733	444	405; 411; 417; 467;	742	493	410;	743	452	413.	730	462	408;
745	23	4	415.	746	455	416.	747	456	417.	748	457	418	749	458	419.	750	450	420.
751	46	0	421:	752	429	468:	753	428	467:	754	427	466:	755	425	464:	756	424	463:
757	46	2	423:	758	461	422;	759	36	547;	760	547	75: 7	61 4	548	: 762	548	43:	
763	11	4	549;	764	549	153;	765	82	550;	766 :	550	121;	767	192	551;	768	551	
769	16	0	552;	770	552	-199;	771	270	553;	772	553	309;	773	238	554;	774	554	277;
775	34	8	555;	776	555	387;	777	316	556;	778	556	355;	779	426	557;	780	557	465;
781	35	4	558;	782	558	433;	783	559	560; 566; 572;	784	560	561;	785	561	562;	786	562	563;
787	56	3	564;	788	564	565;	789	565	566;	790	566	567;	791	567	568;	792	568	569;
793	56	9	570;	794	570	571;	795	571	572;	796	572	573;	797	573	574;	798	574	575;
799	57	5	576;	800	576	577;	801	577	578;	802	578	579;	803	579	580;	804	580	581;
805	28	1	382;	806	582	383;	807	583	584;	808	284	383;	809	285	380;	810	286	587;
									590; 597;									
011	23	5	601	818	232	502-	825	236	603;	820	607	604-	827	504	505-	022	233	600;
826	60	6	607.	830	607	608-	831	602	609;	833	600	610.	833	610	611.	834	611	612.
835	61	2	613.	836	613	614	837	614	615;	838	615	616	839	616	617	840	617	618:
841		8	619.	842	619	620	843	620	621;	844	621	622 :	845	622	623	846	623	624:
847		4	625:	848	625	626:	849	626	627;	850	627	628 :	851	628	629:	852	629	630;
853		1	632:	854	632	633:	855	633	634;	856	634	635:	857	635	636:	858	636	637:
859	63	7	638:	860	638	639;	861	639	640;	862	640	641;	863	641	642;	864	642	643;
865	64	3	644;	866	644	645;	867	645	646;	868	646	647;	869	647	648;	870	648	649;
871	64	9	650;	872	650	651;	873	651	652;	874	652	653;	875	653	654;	876	654	655:
877	65	5	656;	878	656	657;	879	657	658;	880	658	659;	881	659	660;	882	660	661;
883	66	1	662;	884	662	663;	885	663	664;	886	664	665;	887	665	666;	888	667	668;
889	66	8	669;	890	669	670;	891	670	671;	892	671	672;	893	672	673;	894	673	674:
895	67	4	675;	896	675	676;	897	676	677;	898	677	678;	899	678	679;	900	679	680;
901	68	0	681;	902	681	682;	903	682	683;	904	683	684;	905	684	685;	906	685	686;
907	68	6	687;	908	687	688;	909	688	689;	910	689	690;	911	690	691;	912	691	692;
									695;									
									701;									
									708;									
931	71	1	712;	932	712	713;	933	713	714;	934	714	715;	935	715	716;	936	716	717;
937	71	2	/18;	938	718	/19;	939	719	720;	940	120	/21;	941	721	/22;	942	722	723;
943	72	3	/24;	944	124	125;	545	125	726; 732;	996	126	727;	397	121	128;	998	/28	129;

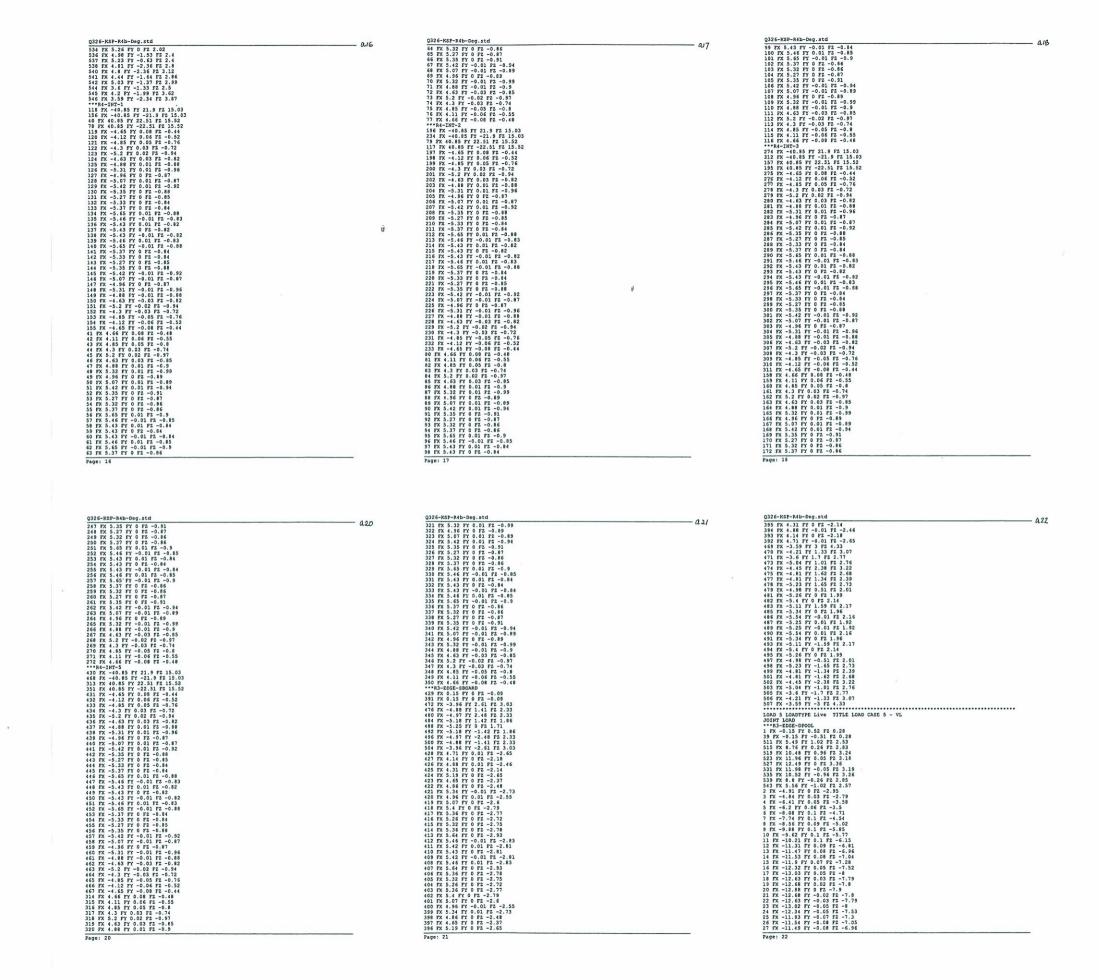
783 783 784 784 785	1011 1011 1011 1011 1011 1011 1011 101	<pre>////////////////////////////////////</pre>
<code-block><code-block><code-block><code-block><code-block></code-block></code-block></code-block></code-block></code-block>	<page-header><code-block><code-block></code-block></code-block></page-header>	2026-MRP-NB-Deg.rd       2019         2026 BER MY HR       2019         2026 START MK NY HR       2019         2027 START MK NY HR       2019         2028 START MK NY HR       2019         2029 START MK NY HR       2019         2029 START MK NY HR       2019         2029 START MK NY HR       2019         2021 START MK NY HR

TAN SIEW MOI

2123 866 468; 2124 867 868; 2125 868 429; 2126 869 870; 2127 870 81	7:
2128 871 872; 2129 872 235; 2130 873 874; 2131 874 819; 2132 875 87	
2133 876 313; 2134 877 878; 2135 878 156; 2136 879 880; 2137 880 11	7;
2138 881 882; 2139 882 234; 2140 883 884; 2141 884 195; 2142 885 88	6;
2138 881 882; 2139 882 234; 2140 883 884; 2141 884 195; 2142 885 88 2143 886 312; 2144 887 888; 2145 888 273; 2146 889 890; 2147 890 39	0;
2148 891 892; 2149 892 351; 2150 778 893; 2151 40 894; 2152 39 901;	
2153 776 902; 2154 913 896; 2155 118 895; 2156 117 904; 2157 782 90	3;
2158 843 157; 2159 196 843; 2160 195 906; 2161 788 905; 2162 844 23	5;
2163 274 844; 2164 273 908; 2165 794 907; 2166 914 898; 2167 352 89	7;
2168 351 910; 2169 800 909; 2170 808 900; 2171 430 899; 2172 429 91	2;
2173 806 911; 2174 893 1; 2175 894 778; 2176 895 913; 2177 896 79; 2178 897 914; 2179 898 313; 2180 899 808; 2181 900 391; 2182 901 77	
2178 897 914; 2179 898 313; 2180 899 808; 2181 900 391; 2182 901 77	6;
2183 902 78; 2184 903 156; 2185 904 782; 2186 905 234; 2187 906 788	2
2188 907 312; 2189 908 794; 2190 909 390; 2191 910 800; 2192 911 46	8;
2193 912 806; 2194 845 848; 2195 846 847; 2196 849 852; 2197 850 85	
2198 853 856; 2199 854 855; 2200 857 860; 2201 858 859; 2202 862 86	4;
2203 861 863; 2204 866 868; 2205 865 867; 2206 869 872; 2207 870 87	17
2208 8/3 8/6; 2209 8/4 8/5; 2210 8/8 880; 2211 8// 8/9; 2212 882 88	
2208 873 876; 2209 874 875; 2210 878 880; 2211 877 879; 2212 882 88 2213 881 883; 2214 886 888; 2215 885 887; 2216 890 892; 2217 889 89 2218 893 894; 2219 895 896; 2220 897 896; 2221 899 900; 2222 901 90	2.
2223 903 904; 2224 905 906; 2225 907 908; 2226 909 910; 2227 911 91	2.
2228 903 904; 2224 905 906; 2225 907 908; 2228 905 910, 2227 911 91 2228 777 511; 2229 775 543; 2230 807 472; 2231 805 504; 2232 778 82	3.
2223 913 823; 2234 776 824; 2235 782 824; 2236 778 511; 2237 776 54	3:
2238 913 825; 2239 843 825; 2240 782 826; 2241 788 826; 2242 843 82	7:
2243 844 827. 2244 788 828. 2245 794 828. 2246 844 829. 2247 914 82	9:
2248 794 830: 2249 800 830: 2250 914 831; 2251 808 831: 2252 800 83	2;
2248 794 850; 2249 800 830; 2250 914 831; 2251 808 831; 2252 800 83 2253 806 832; 2254 808 472; 2255 806 504; 2256 811 785; 2257 813 77	9;
2258 812 786; 2259 814 780; 2260 813 791; 2261 815 785; 2262 814 79	2;
2263 816 786; 2264 815 797; 2265 817 791; 2266 816 798; 2267 818 79	2;
2268 817 803; 2269 819 797; 2270 818 804; 2271 820 798; 2272 819 80	9;
2273 821 803; 2274 820 810; 2275 822 804;	
***************************************	
DEFINE MATERIAL START	
ISOTROPIC STEEL	
E 205	
POISSON 0.3	
DENSITY 7.68195e-008	
ALPHA 1.2e-005	
DAHP 0.03	
END DEFINE MATERIAL	
** MEMBER SIZES	
START USER TABLE	
TABLE 1	
UNIT METER KN	
PIPE	
CHS114X10.0	
0.114 0.094 0.00328 0.00328	
CHS609X16	
0.609 0.577 0.029807 0.029807	
CHS114X8.0	
0.114 0.098 0.00267 0.00267	
CH5219X9.0	
0.219 0.201 0.005937 0.005937	
CH588.9X5.5	
0.0889 0.0779 0.001441 0.001441	
CH5168.3X7	
0.1683 0.1543 0.00354 0.00354	
CH5168.3X11	
0.1683 0.1463 0.005435 0.005435	
CH5177.8X8	
0.1778 0.1618 0.004267 0.004267	
CH5273X9.5	
0.273 0.254 0.007864 0.007864	
CHS273X9.0	
0.273 0.255 0.007464 0.007464	
CH573X5.16	
0.073 0.06268 0.001099 0.001099	
END	
UNIT MMS KN	
MEMBER PROPERTY BRITISH	

26-KSP-R4b-Deg.std 85 123 237 275 313 351 427 CON GZ -3.71 1.51	
52 CON GZ -3.18 0.637	
49 CON GZ -3.18 7.612	
AD 4 LOADTYPE None TITLE LOAD CASE 4 - PRE	
DINT LOAD	
*R3-EDGE-DPOOL FX -0.15 FY 0.67 FZ 0.44	
FX -0.15 FY -0.67 F2 0.44	
1 FX 3.96 FY 2.66 FZ 3.16	
5 FX 4.87 FY 0.65 FZ 2.03 9 FX 4.96 FY 1.45 FZ 2.1	
3 FX 5.18 FY 0.01 F2 1.67	
7 FX 5.24 FY 0 F2 1.78 1 FX 5.18 FY -0.01 F2 1.67	
5 FX 4.96 FY -1.45 FZ 2.1	
9 FX 4.87 FY -0.65 FZ 2.03	
3 FX 3.96 FY -2.66 FZ 3.16 FX -4.71 FY -0.01 FZ -2.72	
FX -4.14 FY 0 FZ -2.23	
FX -4.87 FY 0 F2 -2.52	
FX -4.31 FY 0 FZ -2.2 FX -5.2 FY -0.01 FZ -2.73	
FX -4.64 FY 0.01 FZ -2.42	
FX -4.87 FY 0 F2 -2.55	
FX -5.31 FY 0 FZ -2.79 FX -4.96 FY 0 FZ -2.6	
FX -5.07 FY 0 FZ -2.66	
FX -5.42 FY 0 FZ -2.86 FX -5.35 FY -0.01 FZ -2.82	
FX -5.27 FY -0.01 FZ -2.78	
FX -5.33 FY 0 FZ -2.81	
FX -5.37 FY 0 FZ -2.84 FX -5.65 FY 0.01 FZ -2.99	
EX -5.46 FY -0.01 FZ -2.89	
FX -5.43 FY 0.01 FZ -2.87	
FX -5.43 FY 0 FZ -2.87 FX -5.43 FY -0.01 FZ -2.87	
FX -5.46 FY 0.01 FZ -2.89	
FX -5.65 FY -0.01 FZ -2.99	
FX -5.37 FY 0 FZ -2.84 FX -5.33 FY 0 FZ -2.81	
FX -5.27 FY 0.01 FZ -2.78	
FX -5.35 FY 0.01 FZ -2.82 FX -5.42 FY 0 FZ -2.86	
FX -5.42 FI 0 FZ -2.66	
FX -4.96 FY 0 FZ -2.6	
FX -5.31 FY 0 FZ -2.79 FX -4.87 FY 0 FZ -2.55	
FX -4.64 FY -0.01 FZ -2.42	
FX -5.2 FY 0.01 FZ -2.73	
FX -4.31 FY 0 FZ -2.2 FX -4.87 FY 0 FZ -2.52	
FX -4.14 FY 0 F2 -2.23	
FX -4.71 FY 0.01 FZ -2.72	
8 FX 3.59 FY 2.34 FZ 3.87 9 FX 4.2 FY 1.99 FZ 3.62	
0 FX 3.6 FY 1.33 FZ 2.5	
2 FX 5.03 FY 1.37 FZ 2.99 3 FX 4.44 FY 1.64 FZ 2.86	
3 FX 4.44 FY 1.54 FZ 2.85 4 FX 4.8 FY 2.36 FZ 3.12	
6 FX 4.81 FY 2.36 FZ 2.8	
7 FX 5.23 FY 0.63 F2 2.4	
8 FX 4.98 FY 1.53 FZ 2.4 0 FX 5.26 FY 0 FZ 2.02	
1 FX 5.4 FY 0.28 FZ 2.24	
2 FX 5.11 FY 2.72 FZ 2.45	
4 FX 5.34 FY 0 FZ 2 5 FX 5.54 FY -0.01 FZ 2.2	
6 FX 5.24 FY 0.01 FZ 1.96	
8 FX 5.24 FY -0.01 FZ 1.96	
9 FX 5.54 FY 0.01 FZ 2.2 0 FX 5.34 FY 0 FZ 2	
2 FX 5.11 FY -2.72 FZ 2.45	
3 FX 5.4 FY -0.28 FZ 2.24	

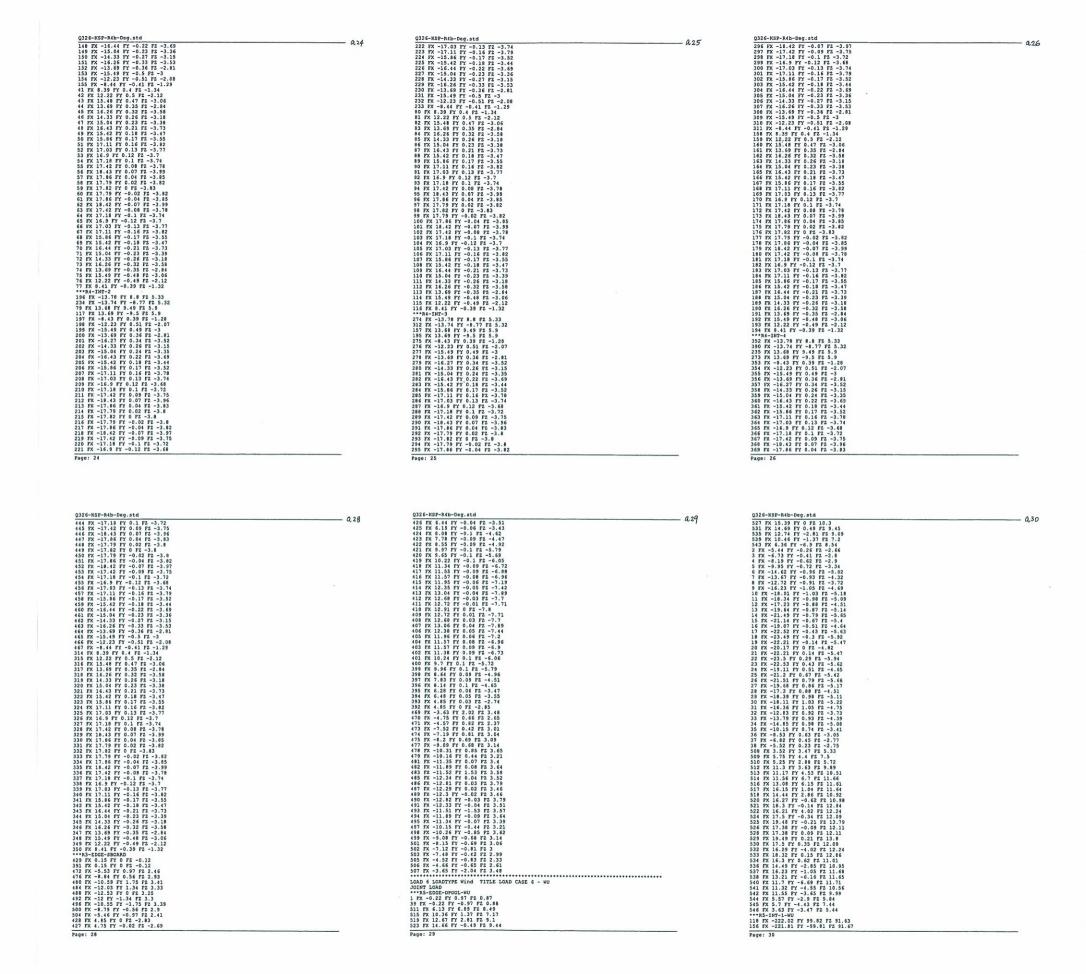






Q326-KSP-R4b-Deg.std	- 10
173 FX 5.65 FY 0.01 FZ -0.9 174 FX 5.46 FY -0.01 FZ -0.85 175 FX 5.43 FY 0.01 FZ -0.84 176 FX 5.43 FY 0 FZ -0.84	a19
175 FX 5.43 FY 0.01 FZ -0.84 176 FX 5.43 FY 0 FZ -0.84	
176 FX 5.43 FY 0 FZ -0.84 178 FX 5.43 FY 0 FZ -0.84 178 FX 5.46 FF 0.01 FZ -0.84 180 FX 5.57 FY 0 FZ -0.86 181 FX 5.57 FY 0 FZ -0.86 181 FX 5.52 FY 0 FZ -0.86 182 FX 5.52 FY 0 FZ -0.87 183 FX 5.53 FY 0 FZ -0.87 184 FX 5.42 FY 0 FZ -0.91 184 FX 5.42 FY 0 FZ -0.94 185 FX 5.55 FY 0 FZ -0.89 185 FX 5.57 FY 0 FZ -0.85 FX 5.57 FY 0 FZ -0.89 185 FX 5.57 FY 0 FZ -0.85 FX 5.57 FY 0 FZ -0.57 FX 5.57 FX 5.57	
79 FX 5.65 FY -0.01 FZ -0.9 80 FX 5.37 FY 0 FZ -0.86	
80 FX 5.37 FY 0 FZ -0.86 81 FX 5.32 FY 0 FZ -0.86 82 FX 5.7 FY 0 FZ -0.87	
81 FX 5.32 FY 0 FZ -0.86 82 FX 5.27 FY 0 FZ -0.87 83 FX 5.35 FY 0 FZ -0.91	
54 FX 5.42 FY -0.01 FZ -0.94 55 FX 5.07 FY -0.01 FZ -0.59 65 FX 4.56 FV 0 FZ -0.59 67 FX 5.52 FY -0.01 FZ -0.59	
86 FX 4.96 FY 0 FZ -0.89 87 FX 5.32 FY -0.01 FZ -0.99	
87 FX 5.32 FY -0.01 FZ -0.99 88 FX 4.88 FY -0.01 FZ -0.9 95 FX 4.63 FY -0.03 FZ -0.9 95 FX 4.63 FY -0.03 FZ -0.85	
90 FX 5.2 FY -0.02 F2 -0.97 91 FX 4.3 FY -0.03 F2 -0.74	
92 FX 4.85 FY -0.05 FZ -0.8	
93 FX 4.11 FY -0.06 FZ -0.55 94 FX 4.66 FY -0.08 FZ -0.48	
*** - W - W - W	
90 FX -40.85 FY -21.9 FZ 15.03 35 FX 40.85 FY 22.51 FZ 15.52	
73 FX 40.85 FY -22.51 FZ 15.52 53 FX -4.65 FY 0.08 FZ -0.44	
54 FX -4.12 FY 0.06 FZ -0.52	
55 FX -4.85 FY 0.05 FZ -0.76 56 FX -4.3 FY 0.03 FZ -0.72	
57 FX -5.2 FY 0.02 FZ -0.94 58 FX -4.63 FY 0.03 FZ -0.82	
59 FX -4.88 FY 0.01 FZ -0.88 60 FX -5.31 FY 0.01 FZ -0.96	
5 FX - 4.36 FX 0.01 FZ -0.96 61 FX - 4.96 FY 0 FZ -0.87 62 FX - 5.17 FY 0.01 FZ -0.87 63 FX - 5.42 FY 0.01 FZ -0.82	
53 FX -5.42 FY 0.01 FZ -0.92 54 FX -5.35 FY 0 FZ -0.88	
54 FX -5.35 FY 0 FZ -0.88 55 FX -5.27 FY 0 FZ -0.85 57 FX -5.27 FY 0 FZ -0.85	
53 fX -5.42 FY 0.01 FZ -0.32 65 fX -5.25 FY 0 52 -0.85 55 fX -5.27 FY 0 52 -0.85 65 fX -5.37 FY 0 52 -0.84 67 X -5.37 FY 0 52 -0.84 67 X -5.37 FY 0 52 -0.84 67 X -5.47 FY 0.17 FX -0.88 75 X -5.47 FY 0.01 FZ -0.85 75 X -5.47 FY 0.72 -0.87 75 X -5.57 FY	
57 FX -5.35 FY 0.01 FZ -0.88 59 FX -5.46 FY -0.01 FZ -0.83	
70 FX -5.43 FY 0.01 FZ -0.82 71 FX -5.43 FY 0 FZ -0.82	
73 FX -5.43 FY -0.01 FZ -0.82 73 FX -5.46 FY 0.01 FZ -0.83	
74 FX -5.65 FY -0.01 FZ -0.88 25 FX -5.37 FY 0 FZ -0.84	
75 FX -5.37 FY 0 FZ -0.84 76 FX -5.33 FY 0 FZ -0.84 77 FX -5.27 FY 0 FZ -0.85	
77 FX -5.27 FY 0 FZ -0.85 78 FX -5.35 FY 0 FZ -0.88	
$\begin{array}{c} 5 \ \mbox{$T$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	
11 FX -4.96 FY 0 FZ -0.87 12 FX -5.31 FY -0.01 FZ -0.96 3 FX -4.88 FY -0.01 FZ -0.88	
3 FX -4.88 FY -0.01 FZ -0.88 4 FX -4.63 FY -0.03 FZ -0.82	
5 FX -5.2 FY -0.02 FZ -0.94 6 FX -4.3 FY -0.03 FZ -0.72	
6 FX -4.3 FY -0.03 FZ -0.72 7 FX -4.85 FY -0.05 FZ -0.76 8 FX -4.12 FY -0.06 FZ -0.52	
6 FX 4.66 FY 0.08 FZ -0.48	
6 FX 4.66 FY 0.08 FZ -0.48 7 FX 4.11 FY 0.06 FZ -0.55 8 FX 4.95 FY 0.05 FZ -0.5	
10 $172 - 5.07$ $177 - 0.0$ $172 - 0.0$	
0 FX 5.2 FY 0.02 FZ -0.97 1 FX 4.63 FY 0.03 FZ -0.85	
1 FX 4.63 FY 0.03 FZ -0.85 2 FX 4.88 FY 0.01 FZ -0.9 3 FX 5.32 FY 0.01 FZ -0.99 4 FX 4.96 FY 0 FZ -0.89	
5 FX 5.07 FY 0.01 FZ -0.89	
6 FX 5.42 FY 0.01 FZ -0.94 age: 19	
326-KSP-R4b-Deg.std 8 FX -11.35 FY -0.09 F2 -6.84	a 2
326-KSP-R4b-Deg.std 6 FX -11.35 FY -0.09 FZ -6.84 9 FX -10.22 FY -0.1 FZ -6.15 0 FX -9.6 FY -0.1 FZ -5.8	az
8 FX -11.35 FY -0.09 F2 -6.84 9 FX -10.22 FY -0.1 F2 -6.15 9 EX -9.67 FY -0.1 F2 -5.8	az
$8 \ \text{FX} - 11.35 \ \text{FY} - 0.09 \ \text{FZ} - 6.44$ $9 \ \text{FX} - 10.22 \ \text{FY} - 0.1 \ \text{FZ} - 6.15$ $0 \ \text{FX} - 9.02 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $1 \ \text{FX} - 9.32 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $2 \ \text{FX} - 8.61 \ \text{FY} - 0.01 \ \text{FZ} - 5.05$ $3 \ \text{FX} - 7.7 \ \text{FY} - 0.1 \ \text{FZ} - 4.56$	az
$8 \ \text{FX} - 11.35 \ \text{FY} - 0.08 \ \text{FZ} - 6.44$ $9 \ \text{FX} - 10.28 \ \text{FY} - 0.1 \ \text{FZ} - 6.15$ $0 \ \text{FX} - 9.02 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $1 \ \text{FX} - 9.52 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $2 \ \text{FX} - 9.5 \ \text{FY} - 0.1 \ \text{FZ} - 5.67$ $2 \ \text{FX} - 9.75 \ \text{FY} - 0.1 \ \text{FZ} - 5.67$	az
$8 \ \text{FX} - 11.35 \ \text{FY} - 0.08 \ \text{FZ} - 6.44$ $9 \ \text{FX} - 10.28 \ \text{FY} - 0.1 \ \text{FZ} - 6.15$ $0 \ \text{FX} - 9.02 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $1 \ \text{FX} - 9.52 \ \text{FY} - 0.1 \ \text{FZ} - 5.87$ $2 \ \text{FX} - 9.5 \ \text{FY} - 0.1 \ \text{FZ} - 5.67$ $2 \ \text{FX} - 9.75 \ \text{FY} - 0.1 \ \text{FZ} - 5.67$	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{F}$x$} - 1.1 \ \mbox{ $5$} \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.5 \ \mbox{ $\mathbf{F}$} - 0.5 \ \mbox{ $\mathbf{F}$x$} - $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{F}$x$} - 1.1 \ \mbox{ $5$} \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.5 \ \mbox{ $\mathbf{F}$} - 0.5 \ \mbox{ $\mathbf{F}$x$} - $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{F}$x$} - 1.1 \ \mbox{ $5$} \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.5 \ \mbox{ $\mathbf{F}$} - 0.5 \ \mbox{ $\mathbf{F}$x$} - $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{F}$x$} - 1.1 \ \mbox{ $5$} \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.6 \ \mbox{ $\mathbf{F}$x$} - 0.5 \ \mbox{ $\mathbf{F}$} - 0.5 \ \mbox{ $\mathbf{F}$x$} - $	a.2
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a.2.
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	a.2.
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	a.2
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a2
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$\begin{array}{c} 1 \ \mbox{ $\mathbf{r}$} \ \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a.2
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a.2.
$\begin{array}{c} 8 \ \mbox{ rx} - 1.1 \ \mbox{ rx} + 7 \ \mbox{ rot} - 6.14 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 6.15 \\ \mbox{ rx} - 9.2 \ \mbox{ rx} + 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.87 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.1 \ \mbox{ rz} - 5.67 \\ \mbox{ rx} - 7.7 \ \mbox{ rz} - 0.5 \ \mbox{ rz} - 3.54 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 6.48 \ \mbox{ ry} - 0.0 \ \mbox{ rz} - 2.95 \\ \mbox{ bs} \ \mbox{ rx} - 5.9 \ \mbox{ rz} - 3.62 \\ \mbox{ rx} - 5.87 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.5 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.68 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 0.68 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10 \ \mbox{ rz} - 2.95 \\ \mbox{ rz} - 7.10 \ \mbox{ rz} - 7.10$	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a2
$ \begin{array}{l} 8 \ \mbox{rx} - 11.35 \ \mbox{ry} - 0.69 \ \mbox{rz} - 6.14 \\ 9 \ \mbox{rx} - 10.27 \ \mbox{rx} - 0.1 \ \mbox{rz} - 6.15 \\ 0 \ \mbox{rx} - 9.5 \ \mbox{ry} - 0.1 \ \mbox{rz} - 6.15 \\ 1 \ \mbox{rx} - 9.5 \ \mbox{rz} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 5.87 \\ 2 \ \mbox{rx} - 6.3 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 1.67 \ \mbox{rz} - 1.67 \\ 4 \ \mbox{rz} - 1.67 \ \mbox{rz} - 1.67 \\ 5 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.68 \\ 6 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 1 \ \mbox{rz} - 1.67 \ rz$	42
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	az
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a2
$ \begin{array}{l} 8 \ \mbox{rx} - 11.35 \ \mbox{ry} - 0.69 \ \mbox{rz} - 6.14 \\ 9 \ \mbox{rx} - 10.27 \ \mbox{rx} - 0.1 \ \mbox{rz} - 6.15 \\ 0 \ \mbox{rx} - 9.5 \ \mbox{ry} - 0.1 \ \mbox{rz} - 6.15 \\ 1 \ \mbox{rx} - 9.5 \ \mbox{rz} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 5.87 \\ 2 \ \mbox{rx} - 6.3 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 1.67 \ \mbox{rz} - 1.67 \\ 4 \ \mbox{rz} - 1.67 \ \mbox{rz} - 1.67 \\ 5 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.68 \\ 6 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 1 \ \mbox{rz} - 1.67 \ rz$	42
$ \begin{array}{l} 8 \ \mbox{rx} - 11.35 \ \mbox{ry} - 0.69 \ \mbox{rz} - 6.14 \\ 9 \ \mbox{rx} - 10.27 \ \mbox{rx} - 0.1 \ \mbox{rz} - 6.15 \\ 0 \ \mbox{rx} - 9.5 \ \mbox{ry} - 0.1 \ \mbox{rz} - 6.15 \\ 1 \ \mbox{rx} - 9.5 \ \mbox{rz} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 5.87 \\ 2 \ \mbox{rx} - 6.3 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 1.67 \ \mbox{rz} - 1.67 \\ 4 \ \mbox{rz} - 1.67 \ \mbox{rz} - 1.67 \\ 5 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.68 \\ 6 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 1 \ \mbox{rz} - 1.67 \ rz$	a2
$ \begin{array}{l} 8 \ \mbox{rx} - 11.35 \ \mbox{ry} - 0.69 \ \mbox{rz} - 6.14 \\ 9 \ \mbox{rx} - 10.27 \ \mbox{rx} - 0.1 \ \mbox{rz} - 6.15 \\ 0 \ \mbox{rx} - 9.5 \ \mbox{ry} - 0.1 \ \mbox{rz} - 6.15 \\ 1 \ \mbox{rx} - 9.5 \ \mbox{rz} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 5.87 \\ 2 \ \mbox{rx} - 6.3 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 7.7 \ \mbox{rz} - 0.1 \ \mbox{rz} - 1.67 \\ 3 \ \mbox{rx} - 1.67 \ \mbox{rz} - 1.67 \\ 4 \ \mbox{rz} - 1.67 \ \mbox{rz} - 1.67 \\ 5 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.68 \\ 6 \ \mbox{rx} - 6.48 \ \mbox{rz} - 0.0 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 0 \ \mbox{rx} - 1.67 \ \mbox{rz} - 2.95 \\ 1 \ \mbox{rz} - 1.67 \ rz$	a2
$ \begin{array}{l} 8 \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \mbox{ $\mathbf{r}$} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	a2
8 FX -11.35 FY -0.09 FZ -6.44 9 FX -01.27 -0.1 FZ -6.15 0 FX -9.22 FY -0.1 FZ -6.15 0 FX -9.22 FY -0.1 FZ -6.15 1 FX -9.22 FY -0.1 FZ -4.57 5 FX -6.22 FY -0.1 FZ -4.67 5 FX -6.27 FY -0.07 FZ -3.62 5 FX -6.4 FY -0.05 FZ -3.62 1 FX -6.4 FY -0.05 FZ -3.72 1 FX -5.7 FY -0.07 FZ -3.74 1 FX -7.7 FY -0.07 FZ -3.75 1 FX -7.7 FY -7.7 FY -3.77 1 FX -7.7 FY -0.07 FZ -3.75 1 FX -7.7 FY -7.7 FY -3.77 1	4.2





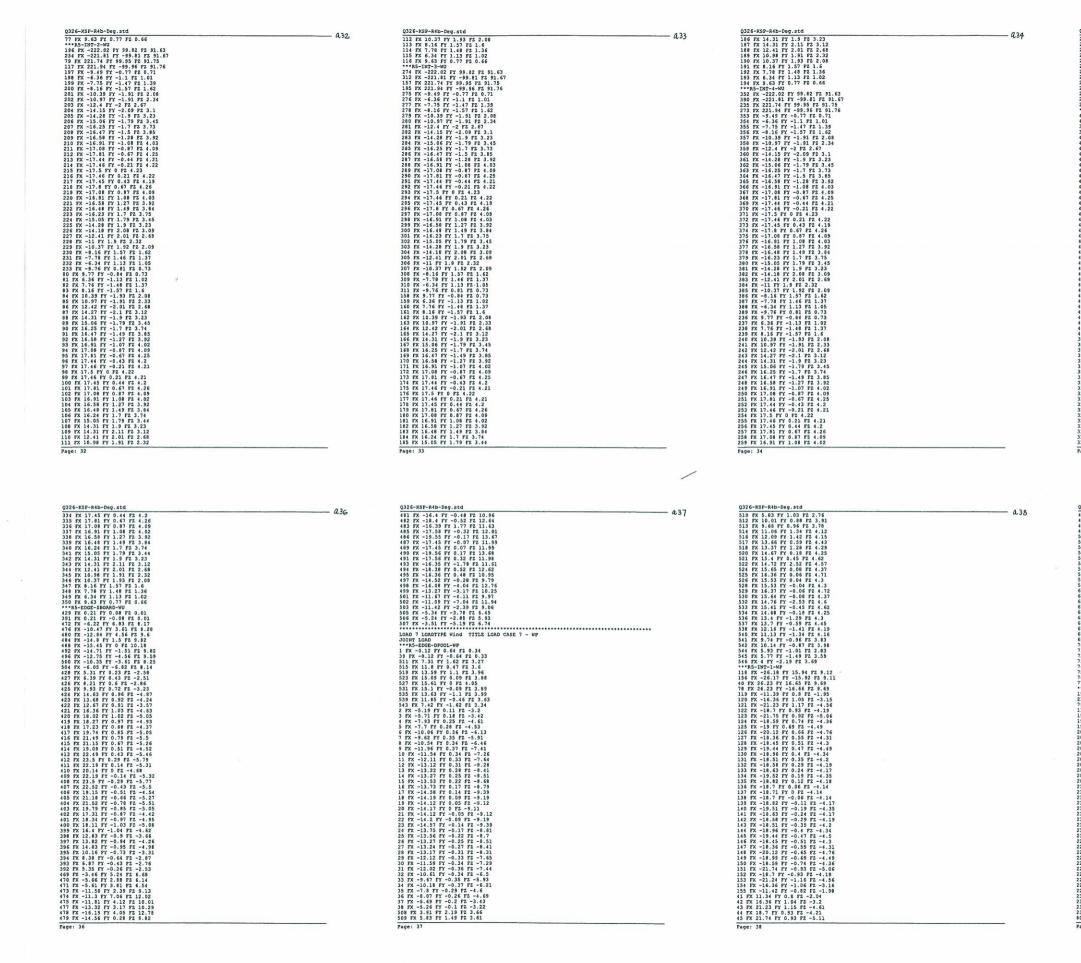
TAN SIEW MOI



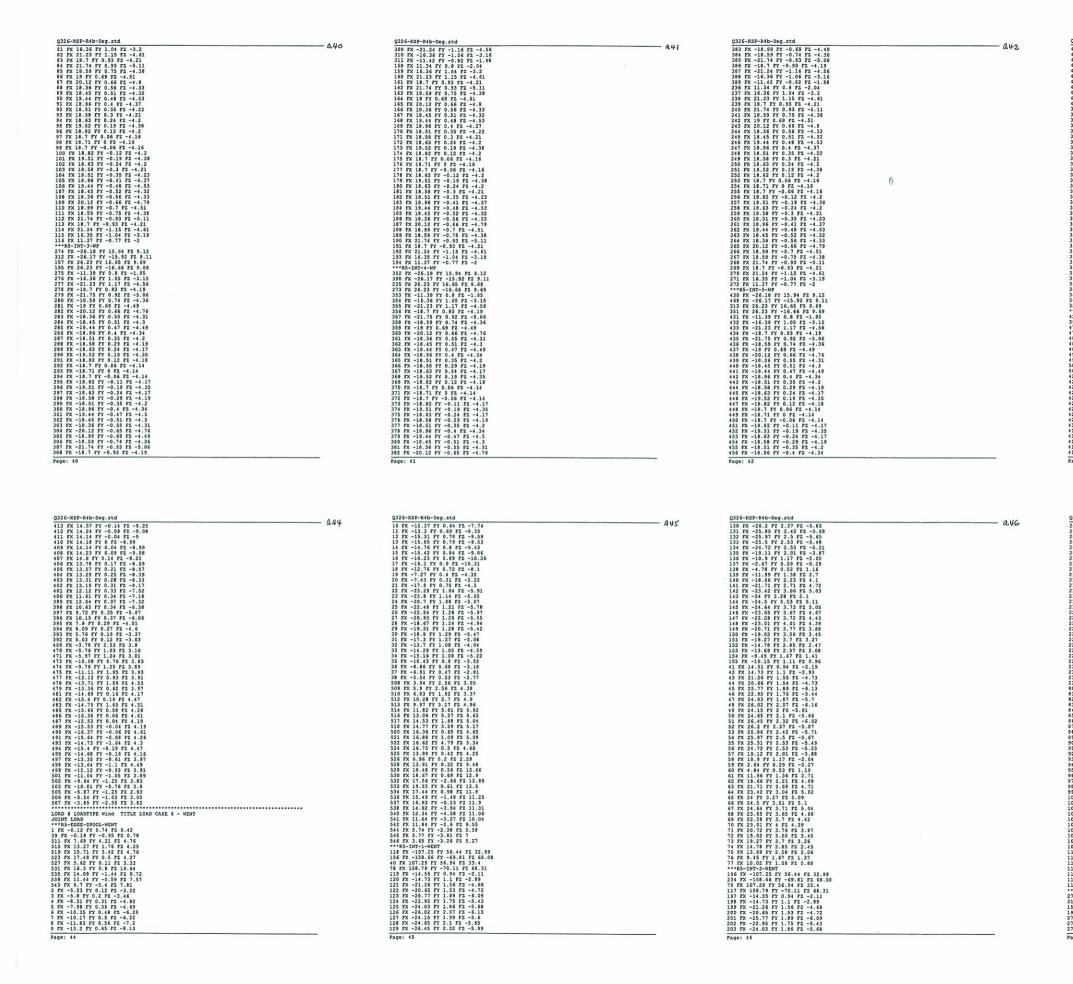
Q326-KSP-R4b-Deg.std	
Q226-KSF-RHb-Deg.std 370 FX -17.79 FY 0.02 F2 -3.6 371 FX -17.78 FY -0.02 F2 -3.8 372 FX -17.78 FY -0.02 F2 -3.8 373 FX -17.85 FY -0.02 F2 -3.8 374 FX -17.85 FY -0.02 F2 -3.75 375 FX -17.82 FY -0.02 FZ -3.75 376 FX -17.18 FY -0.17 FZ -3.72 377 FX -16.9 FY -0.12 FZ -3.76 378 FX -17.01 FY -0.13 FZ -3.79 379 FX -16.9 FY -0.12 FZ -3.74 370 FX -15.85 FY -0.72 FZ -3.82 371 FX -15.85 FY -0.72 FZ -3.82 372 FX -16.9 FY -0.17 FZ -3.82 373 FX -16.9 FY -0.17 FZ -3.82 374 FX -15.85 FY -0.72 FZ -3.85 375 FX -17.01 FY -0.13 FZ -3.79 376 FX -15.95 FY -0.73 FZ -3.85 376 FX -15.85 FY -0.72 FZ -3.85 376 FX -15.85 FY -0.73 FZ -3.85 376 FX -15.85 FY -0.73 FZ -3.85 376 FX -15.87 FY -0.74 FZ -3.84 377 FX 12.22 FY 0.5 FZ -3.85 378 FX -16.26 FY -0.73 FZ -3.85 378 FX -16.26 FY -0.73 FZ -3.85 379 FX -15.49 FY -0.74 FZ -1.24 370 FX 13.50 FY -0.57 FZ -3.85 376 FX 3.37 FY 0.4 FZ -1.24 376 FX 3.37 FY 0.5 FZ -3.85 376 FX 3.37 FY 0.74 FZ -1.34 377 FX 13.22 FY 0.5 FZ -3.87 376 FX 3.37 FY 0.74 FZ -1.34 377 FX 13.22 FY 0.75 FZ -3.87 376 FX 13.97 FY 0.14 FZ -1.29 376 FX 3.37 FY 0.04 FZ -1.34 377 FX 13.22 FY 0.75 FZ -3.87 377 FX 13.22 FY 0.75 FZ -3.74 378 FX 13.42 FY 0.04 FZ -3.87 378 FX 13.42 FY 0.04 FZ -3.87 379 FX 13.42 FY 0.04 FZ -3.87 370 FX 13.42 FY 0.04 FZ -3.87 371 FX 13.53 FY 0.15 FZ -3.74 372 FX 13.42 FY 0.16 FZ -3.87 375 FX 13.42 FY 0.17 FZ -3.75 376 FX 13.42 FY 0.18 FZ -3.75 376 FX 13.42 FY 0.18 FZ -3.76 377 FX 13.64 FY -0.17 FZ -3.87 378 FX 13.42 FY 0.18 FZ -3.77 378 FX 13.42 FY 0.18 FZ -3.78 379 FX 13.42 FY 0.18 FZ -3.78 370 FX 13.42 FY 0.18 FZ -3.78 37	a27
431       Tx - 8.43       TY 0.39       Fz - 1.28         432       Tx - 1.2.23       FY 0.51       Fz - 2.07         432       Tx - 1.2.43       FY 0.51       Fz - 2.07         433       Tx - 1.5.43       FY 0.54       Fz - 3.01         435       Tx - 1.6.27       FY 0.34       Fz - 3.52         435       Tx - 1.6.43       FY 0.26       Fz - 3.15         437       Tx - 1.6.43       FY 0.22       Fz - 3.52         438       Tx - 1.6.42       FY 0.3.17       F. 3.15         439       Tx - 1.6.42       FY 0.3.17       F. 3.15         439       Tx - 1.6.42       FY 0.3.17       F. 3.15         431       Tx - 1.6.02       FT - 3.52       FX - 1.6.43         431       Tx - 1.0.22       FY - 3.52       FX - 1.6.43         441       Tx - 1.7.01       FY 0.3.16       FZ - 3.78         442       Tx - 1.7.01       FY 0.3.16       FZ - 3.74	
0326-KSP-RMb-Deg.std 10 FX 221.74 FY 39.55 FZ 31.75 11 FX 221.74 FY 39.55 FZ 31.75 12 FX -6.15 FY -1.1 FZ 1.01 12 FX -6.15 FY -1.17 FZ 1.02 12 FX -6.15 FY -1.17 FZ 1.03 12 FX -6.15 FY -1.17 FZ 1.04 12 FX -6.15 FY -1.07 FZ 1.29 12 FX -7.15 FY -1.07 FZ 1.02 12 FX -7.15 FY -1.07 FZ 2.04 12 FX -7.15 FY -1.07 FZ 2.04 12 FX -7.15 FY -2.07 FZ 2.01 12 FX -7.15 FY -2.07 FZ 3.03 13 FX -16.05 FY -1.27 FZ 3.04 13 FX -17.06 FY -0.87 FZ 4.09 13 FX -17.06 FY -0.87 FZ 4.20 13 FX -17.06 FY -0.87 FZ 4.20 14 FX -10.67 FY -1.7 FZ 3.52 14 FX -17.46 FY 0.03 FZ 4.20 15 FX -10.47 FY 0.48 FZ 0.07 16 FX -12 FY -1.9 FZ 3.63 17 FX -16.59 FY 1.17 FZ 3.52 14 FX -16.63 FY 1.17 FZ 3.52 14 FX -16.63 FY 1.17 FZ 3.52 14 FX -16.63 FY 1.17 FZ 3.62 15 FX -10.77 FY -1.84 FZ 0.07 15 FX -10.77 FY -1.84 FZ 0.07 15 FX -10.77 FY -1.84 FZ 0.07 15 FX -10.77 FY -1.94 FZ 0.07 15 FX -0.077 FY -1.97 FZ 0.07 15 FX -0.077 FY 0.077 FZ 0.07 15 FX 0.077 FY 0.077 FZ 0.07 15 FX 0.077 FY 0.077 FZ 0.07 15 FX 0.077 FY 0.077 FZ 0.07 17 FX 0.077	a31



122

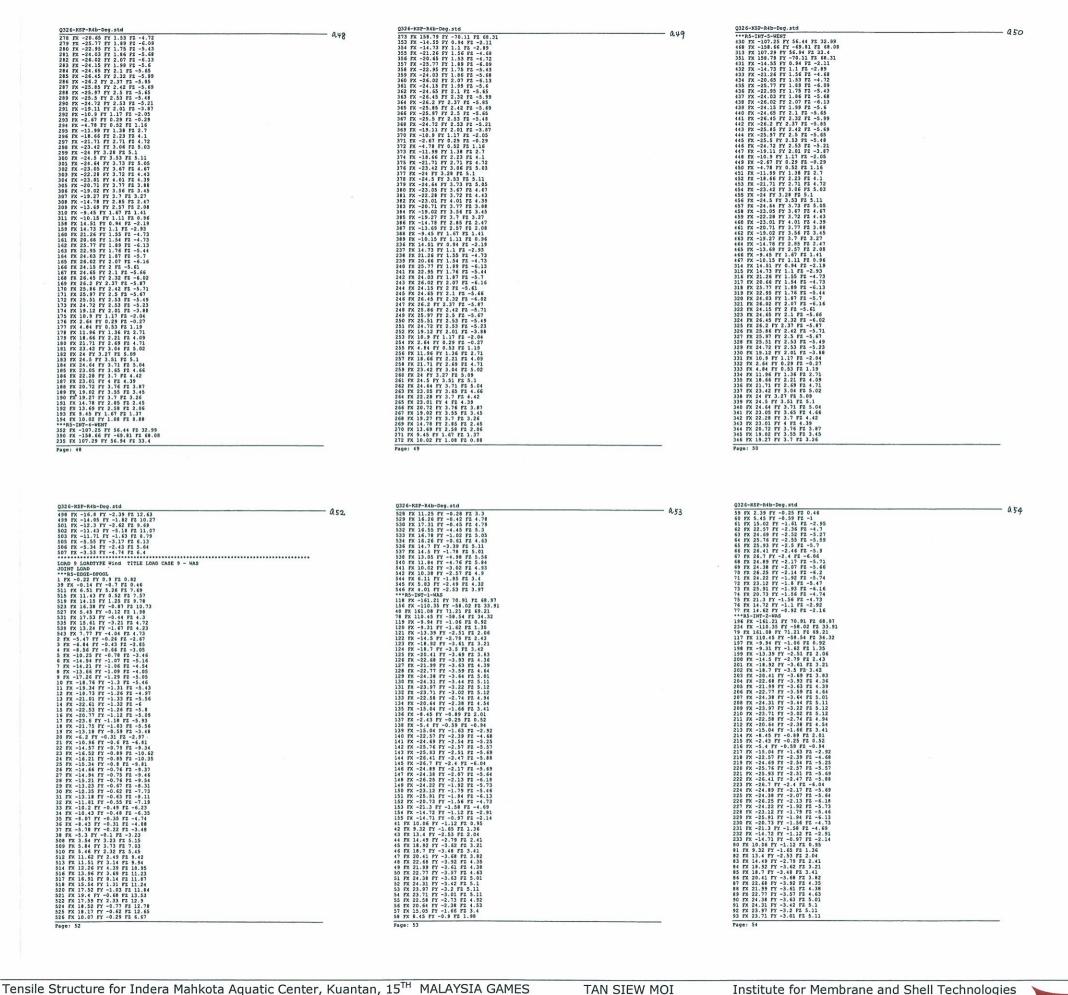


Q326-KSP-R4b-Deg.std	
140         TX 16.58         TY 1.27         TZ 3.54           250         TX 15.68         TY 1.47         TZ 3.74           252         TX 15.78         TY 1.57         TZ 3.74           254         TX 15.78         TY 1.57         TZ 3.74           255         TX 15.78         TY 1.57         TZ 3.74           256         TX 15.71         TY 2.3.73         TX 1.57           256         TX 1.31         TY 1.57         TZ 3.23           257         TX 10.58         TY 1.59         TZ 2.08           256         TX 1.57         TY 1.59         TZ 2.08           257         TX 9.53         TY 1.59         TZ 2.08           250         TX 9.53         TY 1.59         TZ 2.08           272         TX 9.53         TY 0.77         TZ 0.66           273         TX 5.14         TY 9.59         TZ 1.02           274         TX 7.03         TY -0.77         TZ 0.16           274         TX 7.51         TZ 1.57         T.137           274         TX 7.51         TZ 1.57         T.177           275         TY 1.57         TZ 1.67         TY 1.57           276         TY 1.57         TZ 1.67	- 4.35
433 FF -11.08 FF 0.187 FE 4.03 453 FF -16.48 FF 1.107 FE 4.03 456 FF -16.48 FF 1.107 FE 4.03 456 FF -16.48 FF 1.49 FE 3.44 457 FF -16.23 FF 1.97 FE 3.43 458 FF -16.48 FF 1.49 FE 3.45 458 FF -16.48 FF 1.97 FE 3.43 458 FF -16.41 FF 2.01 FE 2.69 451 FF -12.41 FF 2.01 FE 2.69 452 FF -11 FF 1.97 FE 2.32 453 FF -16.47 FF 1.97 FE 2.69 456 FF -1.97 FF 1.97 FE 2.69 457 FF -1.57 FF 0.03 FF 1.67 456 FF -1.37 FF 1.67 456 FF -1.37 FF 0.03 314 FF 5.77 FF -0.48 FE 0.73 315 FF 5.36 FF -1.37 FE 2.69 456 FF -1.37 FF 2.167 317 FF 8.16 FF -1.37 FE 2.167 318 FF 1.97 FF -0.48 FE 0.73 318 FF 1.97 FF -0.48 FE 0.73 317 FF 3.67 FF -1.97 F2 2.08 318 FF 1.97 FF -1.91 FE 2.08 319 FF 1.057 FF -1.91 FE 2.08 321 FF 1.63 FF -1.97 F2 2.08 322 FF 1.43 FF -1.9 FF 3.45 324 FF 1.62 FF -1.77 F2 3.45 325 FF 1.63 FF -1.97 F2 3.45 326 FF 1.62 FF -1.78 F2 3.45 327 FF 1.64 FF -1.37 F2 3.45 328 FF 1.62 FF -1.07 F2 3.45 329 FF 1.64 FF -1.37 F2 3.45 327 FF 1.64 FF -0.47 F2 3.45 328 FF 1.62 FF -0.07 F2 4.09 329 FF 1.64 FF -0.47 F2 4.22 327 FF 1.64 FF -0.47 F2 4.22 328 FF 1.64 FF -0.47 F2 4.22 329 FF 1.64 FF -0.47 F2 4.22 327 FF 1.64 FF -0.47 F2 4.22 328 FF 1.60 FF -0.47 F2 4.22 329 FF 1.7.64 FF -0.47 F2 4.22 329 FF 1.7.64 FF -0.47 F2 4.22 320 FF 1.64 FF -0.47 F2 4.22 321 FF 1.64 FF -0.47 F2 4.22 322 FF 1.64 FF -0.47 F2 4.22 323 FF 1.64 FF -0.47 F2 4.22 324 FF 1.64 FF -0.47 F2 4.22 325 FF 1.7.64 FF -0.47 F2 4.22 326 FF 1.7.64 FF -0.47 F2 4.22 327 FF 1.64 FF -0.47 F2 4.22 328 FF 1.7.64 FF -0.47 F2 4.22 329 FF 1.7.64 FF 0.63 FF 4.22 320 FF 1.64 FF -0.47 F2 4.22 321 FF 3.64 FF -0.47 F2 4.22 322 FF 1.65 FF -0.77 F2 4.22 325 FF 1.7.64 FF 0.63 FF 4.22 326 FF 1.7.64 FF 0.63 FF 4.22 327 FF 1.64 FF 0.64 FF 4.22 328 FF 1.65 FF 0.67 F2 4.22 328 FF 1.65 FF 0.67 F2 4.22 329 FF 1.7.64 FF 0.63 FF 4.22 320 FF 1.64 FF 0.64 FF 4.22 320 FF 1.64 FF 0.64 FF 4.22 321 FF 1.64 FF 0.64 FF 4.22 322 FF 1.7.64 FF 0.64 FF 4.22 325 FF 1.7.64 FF 0.64 FF 4.22 326 FF 1.7.64 FF 0.64 FF 4.22 327 FF 1.64 FF 0.64 FF 4.22 328 FF	
Q326-KSP-R4b-Deg.std 46 FX 18.59 FY 0.75 FZ -4.38 47 FX 13 FY 0.69 FZ -4.51 46 FX 13.67 0.56 FZ -4.51 46 FX 13.67 0.56 FZ -4.33 50 FX 18.45 FY 0.55 FZ -4.33 51 FX 13.44 FY 0.48 FZ -4.53	- a39
$ \begin{array}{c} 52 \ \text{PX} \ 10.96 \ \text{PY} \ 0.4 \ \text{PZ} - 4.37 \\ 54 \ \text{PX} \ 10.35 \ \text{PZ} - 4.22 \\ 54 \ \text{PX} \ 10.36 \ \text{PY} \ 0.3 \ \text{PZ} - 4.21 \\ 55 \ \text{PX} \ 10.56 \ \text{PY} \ 0.36 \ \text{PZ} - 4.21 \\ 55 \ \text{PX} \ 10.56 \ \text{PY} \ 0.36 \ \text{PZ} - 4.21 \\ 55 \ \text{PX} \ 10.57 \ \text{PX} \ 0.66 \ \text{PZ} - 4.2 \\ 55 \ \text{PX} \ 10.57 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 55 \ \text{PX} \ 10.71 \ \text{PY} \ 0.72 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 62 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 62 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PY} \ 0.06 \ \text{PZ} - 4.16 \\ 61 \ \text{PX} \ 10.77 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.37 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.37 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.52 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.53 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.53 \ \text{PZ} - 4.28 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.53 \ \text{PZ} - 4.38 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.53 \ \text{PZ} - 4.38 \\ 61 \ \text{PX} \ 10.52 \ \text{PY} \ -0.53 \ \text{PX} \ -0.53 \ \text{PX} \ -0.53 \ \text{PX} \ 10.53 \ \text{PX} \ 10.75 \ \text{PX} \ 10.55 \ \text{PX} \ 10.55 \ \text{PX} \ 10.55 \ \text{PX} \ 10.55 \$	
53 FX 18-51 FY 0.35 Fz $-4.22$ 55 FX 18-53 FY 0.3 Fz $-4.21$ 55 FX 18-63 FY 0.3 Fz $-4.21$ 55 FX 18-63 FY 0.3 Fz $-4.21$ 57 FX 18-62 FY 0.19 Fz $-4.38$ 57 FX 18-72 FY 0.19 Fz $-4.16$ 58 FX 18-77 FV 0.66 FZ $-4.16$ 59 FX 18-77 FV 0.66 FZ $-4.16$ 50 FX 18-78 FV $-0.12$ FZ $-4.16$ 61 FX 18-63 FY $-0.12$ FZ $-4.2$ 62 FX 19-53 FY $-0.15$ FZ $-4.2$	



0326-KSP-R4b-Deg std		
$\begin{array}{c} 0.222-0.55-0.41-0.29, -t.d. \\ 457 \ [FX - 13.46 \ FY - 0.5 \ FZ - 4.31 \\ 459 \ [FX - 13.46 \ FY - 0.5 \ FZ - 4.31 \\ 460 \ [FX - 12.95 \ [FY - 0.5 \ FZ - 4.36 \ [FX - 1.56 \ [FX - 4.56 \ [FX - 1.56 \ [FX - 1.57 \ [FX - 1$	4	- 443
$ \begin{array}{c} 2326 + KS P - R4 b - Dag. std \\ \hline 2046 \ FX & -26.02 \ FY 2.07 \ FZ & -6.13 \\ 0.06 \ FX & -24.15 \ FY 1.39 \ FZ & -5.65 \\ 0.07 \ FX & -26.45 \ FY 2.32 \ FZ & -5.65 \\ 0.08 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.08 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.09 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.09 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.09 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.09 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.09 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.10 \ FX & -25.65 \ FY 2.42 \ FZ & -5.65 \\ 0.11 \ FX & -25.67 \ FY 2.45 \ FZ & -5.65 \\ 0.12 \ FX & -25.67 \ FY 2.45 \ FZ & -5.65 \\ 0.12 \ FX & -25.67 \ FY 0.53 \ FZ & -5.65 \\ 0.12 \ FX & -21.67 \ FY 0.59 \ FZ & -2.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -5.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -5.65 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY 0.59 \ FZ & -2.67 \\ 0.12 \ FX & -21.79 \ FY & -2.59 \ FZ & -2.61 \\ 0.13 \ FX & -21.67 \ FY & -2.59 \ FZ & -2.61 \\ 0.13 \ FX \ -21.67 \ FY \ -2.59 \ FZ & -2.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.59 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.59 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ & -5.61 \\ 0.15 \ FX \ -21.57 \ FY \ -2.57 \ FZ \ -2.60 \\ 0.15 \ FX \ -2.57$		- â.¥-

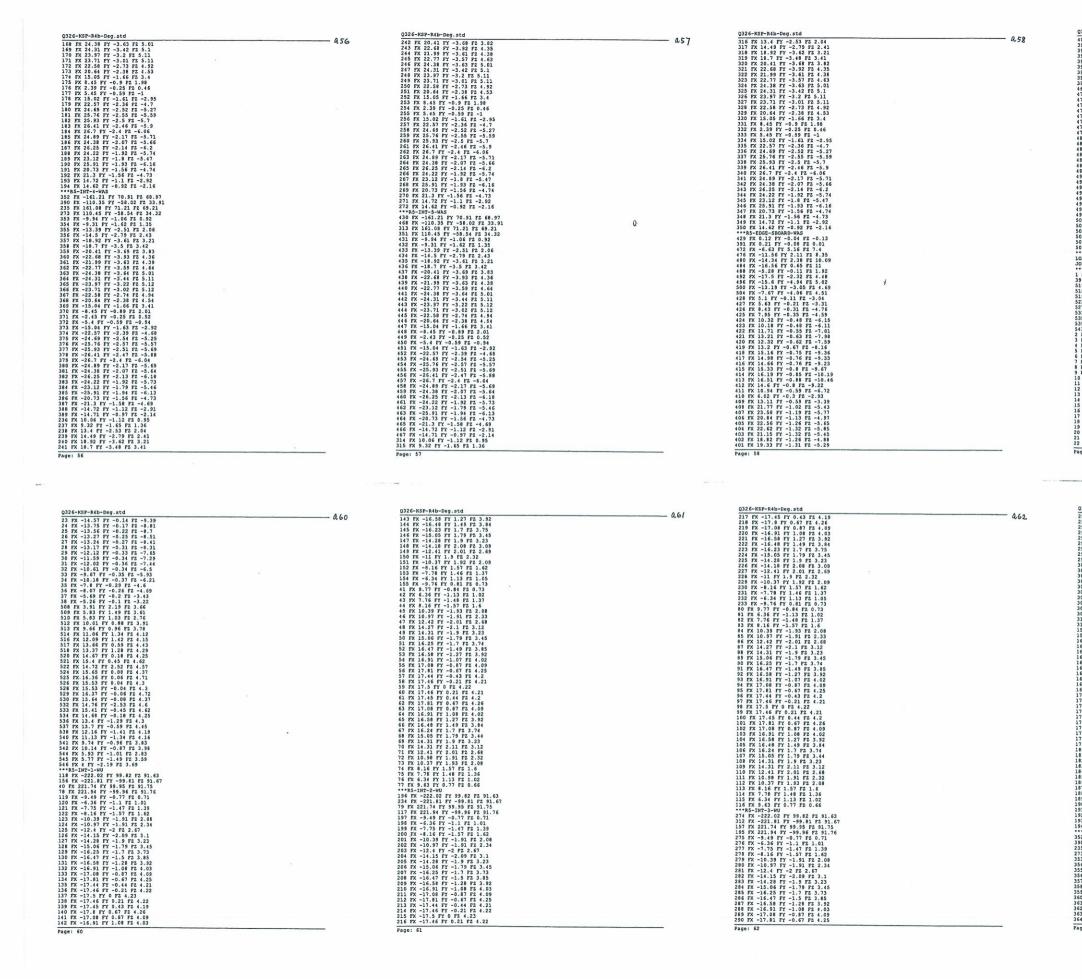
Anhalt University of Applied Sciences, Dessau 🦛





_	Anhalt University of Applied Sciences,	Dessau	
			C

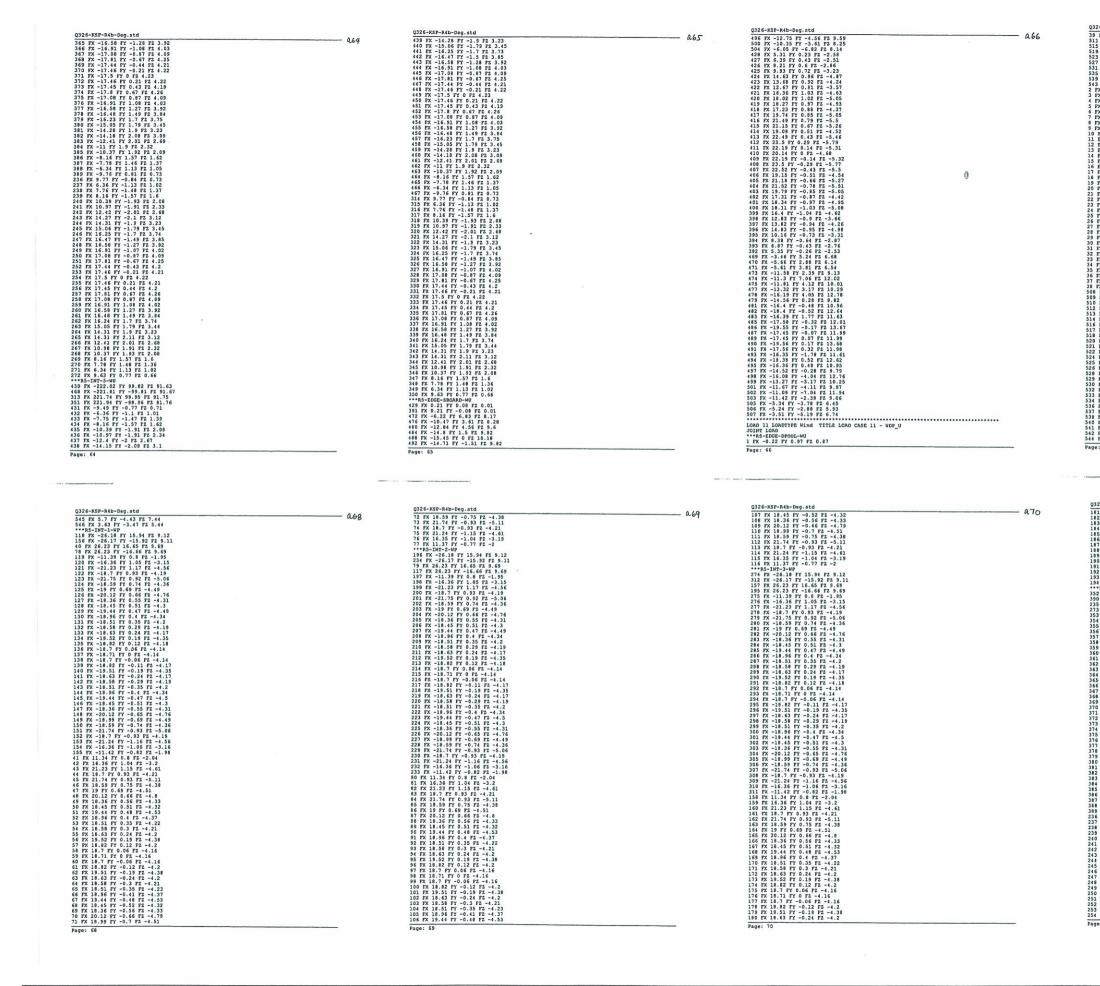
0226-KSP-R4b-Deg.std 347 FX 14.78 FY 2.58 FZ 2.45 348 FX 13.69 FY 2.58 FZ 2.06 349 FX 9.45 FY 1.67 FZ 1.37 350 FX 10.02 FY 1.08 FZ 0.88	a51
348 pr 8 3.45 pr 1.46 pr 2.1.37 350 pr 10.02 pr 1.08 pr 2.0.89 **N5-2005-2003A0-VENT 351 pr 0.1 pr 0.08 pr 2.0.13 352 pr -7.8 pr 4.22 pr 2.4.26 453 pr 0.17 pr 0.48 pr 2.0.13 451 pr 0.17 pr 3.22 pr 2.4.26 456 pr -14.17 pr 0.48 pr 2.4.23 458 pr -15.75 pr 3.22 pr 2.4.26 458 pr -15.75 pr 3.22 pr 2.4.26 459 pr -11.17 pr -0.48 pr 2.0.89 450 pr -11.13 4 pr -2.23 pr 0.31 450 pr -11.11 pr -2.64 pr 2.0.85 550 pr -11.13 4 pr -2.23 pr 0.31 452 pr -16.31 pr -0.78 pr -3.3 455 pr 0.63 pr 0.64 pr -2.35 457 pr 0.51 pr 0.64 pr -2.36 457 pr 1.1.17 pr -2.44 pr -2.43 455 pr 1.1.17 pr -2.44 pr -2.43 455 pr 1.1.17 pr -2.44 pr -2.43 455 pr 1.1.17 pr -2.45 pr -3.43 455 pr 1.1.17 pr -2.45 pr -3.43 455 pr 1.1.17 pr -2.45 pr -3.44 452 pr 1.1.37 pr 1.28 pr 25.3 455 pr 1.1.27 pr 1.28 pr 25.3 455 pr 1.1.27 pr 1.28 pr 25.42 457 pr 1.1.17 pr 1.128 pr 25.3 457 pr 1.1.17 pr 1.128 pr 25.3 458 pr 1.1.17 pr 1.128 pr 25.3 459 pr 1.1.17 pr 1.128 pr 25.42 451 pr 1.1.17 pr 1.128 pr 25.42 451 pr 1.1.17 pr 1.128 pr 25.42 452 pr 1.1.17 pr 1.128 pr 25.42 453 pr 1.1.17 pr 1.128 pr 25.42 454 pr 1.1.17 pr 1.1.28 pr 25.42 455 pr 1.1.17 pr 1.28 pr 25.42 455 pr 1.1.17 pr 2.1.27 pr 24.45 455 pr 1.1.17 pr 2.1.27 pr 24.45 455 pr 1.1.17 pr 2.1.27 pr 24.45 455 pr 1.1.17 pr 2.2 pr 24.45	
429 FX 0.21 FY 0.08 FZ 0.01 391 FX 0.12 FY 0.04 FZ -0.13 472 FX -7.8 FY 4.22 FZ 4.66	
476 FX -13.34 FY 3.2 FZ 4.79 480 FX -15.77 FY 5.22 FZ 5.13 484 FX -17.5 FY 2.45 FZ 4.5	
408 FX -5.75 FY 0.1 FZ 3.23 492 FX -16.31 FY -0.81 FZ 10.89 496 FX -14.11 FY -2.64 FZ 10.05	
500 FX -11.34 FY -2.23 FZ 8.31 504 FX -6.42 FY -5.27 FZ 7.43 428 FX 5.34 FY 0.23 FZ -2.6	
427 FX 6.5 FY 0.45 FZ -2.56 426 FX 8.58 FY 0.65 FZ -3 425 FX 10.21 FY 0.78 FZ -3.34	
424 FX 14.93 FY 1.06 FZ -5 423 FX 14.18 FY 1.05 FZ -4.44 422 FX 13.54 FY 1.07 FZ -3.87	
421 FX 17.3 FY 1.26 FZ -4.96 420 FX 18.7 FY 1.28 FZ -5.3 419 FX 19.19 FY 1.28 FZ -5.24	
418 FX 18.61 FY 1.23 FZ -4.78 417 FX 20.98 FY 1.28 FZ -5.42 416 FX 22.51 FY 1.28 FZ -5.81	
416 FX 22.42 F1 1.22 F2 -5.01 414 FX 20.67 FY 1.07 F2 -4.92 413 FX 23.76 FY 1.14 FZ -5.78	
411 FX 17.81 FY 0.75 FZ -4.36 410 FX 7.54 FY 0.31 FZ -2.12 409 FY 7.35 FZ -4.27	
408 FX 12.79 FY 0.73 F2 -7.99 407 FX 16.11 FY 0.91 F2 -10.15 405 FY 16.26 FY 0.9 F2 -10.22	
405 FX 15.45 FY 0.84 FZ -9.74 404 FX 14.78 FY 0.8 FZ -9.3 403 FX 15.12 FY 0.8 FZ -9.42	
402 FX 15.35 FY 0.79 FZ -9.45 401 FX 13.32 FY 0.69 FZ -8.23 400 FX 12.43 FY 0.64 FZ -7.65	
399 FX 13.29 FY 0.65 FZ -8.04 398 FX 11.89 FY 0.56 FZ -7.1 397 FX 10.28 FY 0.5 FZ -6.18	
396 FX 10.44 FY 0.48 FZ -5.21 595 FX 8.1 FY 0.36 FZ -4.47 394 FX 8.51 FY 0.33 FZ -4.84 393 FX 5.87 FY 0.23 FZ -4.84 395 FX 5.87 FY 0.21 FZ -3.43 395 FX 5.08 FX 0.12 FZ -3.46	
392 FX 5.08 FY 0.12 FZ -3.06	
470 FY -5 85 FY 1.82 FZ 3.73	
474 FX -10.07 FY 4.49 FZ 5.58 475 FX -11.86 FY 3.6 FZ 5.15 477 FX -13.08 FY 3.22 FZ 4.85	
478 FX -14.57 FY 3.88 FZ 5.63 479 FX -14.76 FY 1.57 FZ 4.42 481 FX -16.37 FY 0.66 FZ 4.58	
482 FX -16.88 FY 0.66 FZ 4.89 483 FX -16.63 FY 2.86 FZ 4.88 485 FX -16.76 FY 0.46 FZ 4.55	
466 FX -14 FY 0.39 FZ 4.15 487 FX -7.02 FY 0.18 FZ 2.22 489 FX -13.99 FY 0.29 FZ 9.38	
171         Fx         -6.13         FY         2.28         FX         3.76           173         FX         -0.03         FY         4.48         FX         4.58           174         FX         -0.03         FY         4.48         FX         5.58           175         FX         -1.16         FY         5.75         5.13           175         FX         -1.16         FY         5.75         5.13           175         FX         -1.16         FY         5.75         5.13           175         FX         -1.17         FY         -3.14         FY         -3.14           175         FX         -1.17         FY         3.16         FY         -3.15           175         FX         -1.17         FY         3.14         FY         -3.14           176         FX         -1.16         FY         -1.68         FY         -1.65           176         FY         0.18         FY         -1.55         FY         -1.67           177         FX         -1.02         FY         0.18         FY         -1.35           177         FY         -1.03         FY	
99 17 - 12, 38 F 10, 55 F 21, 51 45 F 78 - 13, 51 F 10, 56 F 2 11, 51 497 F 78 - 13, 51 F 10, 34 F 2 10, 37 Page: 51	
Q326-KSP-R4b-Deg.std 54 FX 22.56 FY -2.73 FZ 4.92 55 FX 20.64 FY -2.78 FZ 4.53	a.5 <u>1</u>
0326-KSP-84b-Deg.std 94 fX 22.38 fY -2.73 f2 4.92 95 fX 12.5 fY -1.6 fF 3.4 97 fX 8.45 FY -0.9 f2 1.98 98 fX 2.39 FY -0.29 f2 1.98 98 fX 2.39 FY -0.25 f2 0.46	a 5 <u>1</u>
Q326-KSP-R4b-Deg.std 94 FX 22.58 FF -2.73 F2 4.92 95 FX 20.64 FY -2.38 F2 4.53 95 FX 15.65 FF -1.56 F2 3.4 97 FX 8.45 FY -0.59 F2 1.38 99 FX 8.45 FY -0.59 F2 -1 100 FX 15.02 FY -0.58 F2 -4.7 100 FX 15.02 FY -2.58 F2 -4.7	a.5 <u>1</u>
Q326-KSP-R4b-Deg.std 94 FX 22.58 FF -2.73 F2 4.92 95 FX 20.64 FF -2.38 F2 4.53 97 FX 14.64 FF -2.18 F2 4.53 98 FX 2.35 FY -0.9 F1 .08 99 FX 2.35 FY -0.57 F2 -1.86 99 FX 2.35 FY -0.57 F2 -1 100 FX 15.02 FF -1.66 F2 -2.57 102 FX 24.66 FY -2.55 F2 -5.77 103 FX 25.76 FY -2.55 F2 -5.59 104 FX 25.75 FF -2.55 F2 -5.79 105 FX 25.76 FY -2.55 FY -5.77 105 FX 25.76 FY -2.55 FY -5.77 105 FX 25.77 105 FX 25.76 FY -2.55 FY -5.77 105 FX 25.77 105 FX 25.76 FY -2.55 FY -5.77 105 FX 25.77 105 FX 25.77	a.5 <u>3</u>
0326-KSP-R4b-Deg.std 94 fX 22.58 fY -2.73 fZ 4.52 95 fX 20.44 fY -2.78 fZ 4.53 96 fX 10.55 fY -1.66 fX 3.4 97 fX 8.45 FY -0.9 fZ 1.98 98 fX 2.37 fY -0.25 fZ -1 107 fX 15.02 fY -1.61 fZ -2.55 107 fX 15.02 fY -1.61 fZ -2.55 107 fX 24.09 fY -2.56 fZ -4.77 103 fX 25.76 fY -2.55 fZ -5.59 104 fX 25.59 fY -2.5 fZ -5.59 105 fX 26.1 fY -2.4 fZ -6.06 107 fX 26.49 fY -2.1 fZ -5.71 105 fX 26.49 fY -2.5 fZ -5.59 104 fX 25.59 fY -2.5 fZ -5.59 105 fX 26.41 fY -2.4 fZ -6.06 107 fX 26.49 fF -2.1 fZ -5.71 107 fX 26.49 fF -2.1 fZ -5.71 107 fX 26.49 fF -2.5 fZ -5.59 106 fX 26.7 fY -2.5 fZ -5.57 107 fX 26.49 fF -2.5 fZ -5.72 107 fX 26.49 fZ -5.72	45 <u>1</u>
Q326-KSP-R4b-Deg.std 54 FX 22.58 FY -2.73 F2 4.92 55 FX 20.64 FY -2.73 F2 4.53 95 FX 20.55 FY -1.66 F3 .4 97 FX 8.45 FY -0.59 F2 1.98 98 FX 2.35 FY -0.25 F2 -4.7 101 FX 22.57 FY -2.36 F2 -4.7 102 FX 24.69 FY -2.52 F2 -5.29 103 FX 25.75 FY -2.36 F2 -5.59 105 FX 26.31 FY -2.47 F2 -5.13 105 FX 26.31 FY -2.47 F2 -5.13 105 FX 26.32 FY -2.17 F2 -5.16 107 FX 24.69 FY -2.17 F2 -5.16 108 FX 24.38 FY -2.07 F2 -5.66 109 FX 24.38 FY -2.07 F2 -5.66 109 FX 26.35 FY -2.14 F2 -5.71 108 FX 26.35 FY -2.14 F2 -5.62 109 FX 26.35 FY -2.14 F2 -5.62 109 FX 26.35 FY -2.14 F2 -5.62 109 FX 26.35 FY -2.14 F2 -5.64 109 FX 26.35 FY -2.14 F2 -5.74 111 FX 23.27 FY -36 F5 -5.74 111 FX 23.27 FY -36 F5 -5.74	4 <i>5</i> 1
94 FX 22.38 FY -2.73 FZ 4.92 95 FX 20.64 FY -2.38 FZ 4.53 96 FX 15.05 FY -1.66 FZ 3.4 97 FX 15.05 FY -1.67 FZ 3.4 98 FX 5.45 FY -0.25 FZ -1 100 FX 5.02 FY -0.59 FZ -1 100 FX 5.02 FY -0.61 FZ -2.95 100 FX 72.40 FY -0.25 FZ -4.77 101 FX 72.57 FY -2.55 FZ -4.77 102 FX 25.05 FY -2.57 FZ -5.57 104 FX 25.53 FY -2.17 FZ -5.57 105 FX 26.41 FY -2.48 FZ -5.57 106 FX 25.53 FY -2.17 FZ -5.57 107 FX 26.43 FY -2.17 FZ -5.73 108 FX 26.43 FY -2.17 FZ -5.71 108 FX 26.43 FY -2.17 FZ -5.71 108 FX 26.43 FY -2.17 FZ -5.64 109 FX 26.43 FY -2.17 FZ -5.64 109 FX 26.43 FY -2.17 FZ -5.64 109 FX 26.25 FY -2.17 FZ -5.64 101 FX 25.53 FY -2.17 FZ -5.64 102 FX 26.53 FY -2.17 FZ -5.64 103 FX 26.73 FY -1.59 FZ -5.14 111 FX 25.53 FY -1.93 FZ -6.16 113 FX 26.73 FY -1.57 FZ -5.67 114 FX 25.73 FY -1.57 FZ -5.74 115 FX 26.73 FY -5.74 115 FX	4 <i>5</i> 3
Q326-KSP-R4b-Deg.std 94 FX 22.58 FY -2.73 FZ 4.92 95 FX 20.64 FY -2.38 FZ 4.53 97 FX 1264 FY -2.18 FZ 4.53 98 FX 2.35 FY -0.57 FZ -1.86 99 FX 2.35 FY -0.57 FZ -1 100 FX 15.02 FY -1.61 FZ -2.75 100 FX 15.02 FY -1.62 FZ -2.77 103 FX 25.76 FY -2.55 FZ -5.77 103 FX 25.76 FY -2.55 FZ -5.77 104 FX 25.37 FY -0.57 FZ -5.77 105 FX 26.41 FF -2.17 FZ -5.71 106 FX 25.37 FY -2.18 FZ -5.77 107 FX 26.41 FF -2.17 FZ -5.71 108 FX 25.57 FZ -1.17 FZ -5.71 108 FX 26.57 FY -2.14 FZ -5.71 109 FX 26.57 FY -2.14 FZ -5.71 108 FX 26.57 FY -2.14 FZ -5.71 109 FX 26.32 FY -2.14 FZ -5.71 108 FX 26.32 FY -2.14 FZ -5.71 109 FX 26.32 FY -2.14 FZ -5.71 109 FX 26.32 FY -2.14 FZ -5.71 110 FX 26.32 FY -1.36 FZ -5.71 111 FX 26.32 FY -1.36 FZ -5.71 112 FX 25.32 FY -1.36 FZ -6.16 113 FX 20.73 FY -1.56 FZ -4.73 115 FX 21.37 FY -1.56 FZ -4.73 115 FX 21.42 FY -0.92 FZ -2.16 ***B5-IMT-3+KS	45 <u>1</u>
$\begin{array}{c} 0326-KSP-RAb-Deg.std\\ 54  FX 22.36 \mbox{ FY -2.73 \mbox{ FZ 4.53 \mbox{ FX 20.44 \mbox{ FY -2.38 \mbox{ FZ 4.53 \mbox{ FY -0.58 $	45 <u>1</u>
Q326-KSP-R4b-Deg.std 94 FX 22.58 FY -2.73 FZ 4.92 95 FX 20.64 FY -2.38 FZ 4.53 95 FX 20.65 FY -1.66 FZ 3.4 97 FX 8.45 FY -0.59 FZ 1.98 98 FX 5.45 FY -0.59 FZ -1 100 FX 15.02 FY -1.61 FZ -2.95 101 FX 22.57 FY -2.36 FZ -4.7 102 FX 25.67 FY -2.57 FZ -1 103 FX 25.67 FY -2.57 FZ -1 105 FX 26.41 FY -2.47 FZ -5.7 105 FX 26.41 FY -2.47 FZ -5.7 105 FX 26.41 FY -2.47 FZ -5.7 106 FX 26.7 FY -2.47 FZ -5.7 107 FX 24.89 FY -2.17 FZ -5.71 108 FX 25.91 FY -1.92 FZ -5.74 111 FX 23.18 FY -2.07 FZ -5.65 112 FX 25.59 FY -1.93 FZ -6.16 113 FX 20.73 FY -1.58 FZ -4.71 115 FX 21.42 FY -1.92 FZ -5.74 115 FX 21.42 FY -1.92 FZ -4.74 115 FX 21.42 FY -1.95 FZ -2.16 ***F5-IN7-3-WAS 127 FX -10.55 FY -5.61 FZ 3.32 137 FX -10.55 FY -5.61 FZ 3.32 147 FX -10.55 FY -5.61 FZ 3.32 157 FX -5.94 FY -1.05 FZ -5.12 157 FX 10.55 FY -5.61 FZ 3.32 157 FX -5.94 FZ -1.05 FZ 5.91 FZ -5.74 157 FX -10.55 FY -5.61 FZ 3.32 157 FX -5.94 FZ -1.05 FZ 5.91 FZ -5.74 157 FX -10.55 FY -5.61 FZ 3.32 157 FX -5.94 FZ -1.05 FZ 5.91 FZ -5.74 157 FX 10.75 FY -5.61 FZ 5.92 157 FX -5.94 FZ -1.05 FZ 5.92 157 FX -5.94 FY -5.95 FY 5.95 FX 5.92 157 FX -5.94 FY -5.95 FX 5.92 157 FX -5.94 FY -5.95 FX 5.92 157 FX -5.	4 <i>5</i> 1
0326-KSP-RMb-Deg.std 94 FX 22.58 FY -2.73 FZ 4.92 95 FX 20.64 FY -2.38 FZ 4.53 95 FX 20.65 FY -1.66 FZ 3.4 97 FX 5.45 FY -0.57 FZ -1 100 FX 15.02 FY -1.61 FZ -2.95 100 FX 25.57 FY -2.58 FZ -4.7 100 FX 25.57 FY -2.58 FZ -5.7 105 FX 26.57 FY -2.58 FZ -5.7 105 FX 26.57 FY -2.46 FZ -5.7 105 FX 26.57 FY -2.46 FZ -5.7 105 FX 26.57 FY -2.46 FZ -5.7 105 FX 26.57 FY -2.47 FZ -5.74 117 FX 21.52 FY -2.17 FZ -5.74 118 FX 21.57 FY -3.57 FZ -5.17 115 FX 14.72 FY -1.57 FZ -4.13 115 FX 14.72 FY -1.57 FZ -4.13 115 FX 14.72 FY -1.57 FZ -2.16 116 FX 16.07 FY 70.91 FZ 64.97 117 FX 161.08 FY 70.91 FZ 64.97 118 FX 16.07 FY 70.91 FZ 64.93 119 FX 16.67 FY -5.47 FZ -2.17 127 FX 161.08 FY -1.06 FZ 6.32 127 FX 16.57 FY 2.47 FZ 2.7 137 FX 161.08 FY -1.67 FZ 6.32 137 FX 16.57 FY 2.47 FZ 2.57 FZ 2.57 147 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.50 FY 70.91 FZ 64.97 157 FX 16.50 FY 70.91 FZ 64.93 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.50 FY 70.91 FZ 64.93 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.47 FZ 2.57 FZ 2.47 157 FX 16.50 FY 70.91 FZ 64.93 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.47 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.47 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.47 FZ 2.57 FZ 2.47 157 FX 16.57 FZ 2.57 FZ 2.43 157 FX 16.57 FZ 2.77 FZ 2.43 157 FX 2.53 FY 2.77 Z2 2.47 157 FX	4 <i>5</i> 3
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	45 <u>1</u>
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	45 <u>1</u>
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	4 <i>5</i> 1
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	453
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	45 <u>1</u>
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	45 <u>1</u>
115 FR 24.7 FF x 13 f2 - 2.35 116 FR 24.6 FT - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FF -58.02 FZ 33.91 135 FX 110.45 FY -58.04 FZ 34.32 275 FX -9.84 FF -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 2.06 278 FX -14.5 FF -2.78 FZ 2.43 278 FX -14.5 FF -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -2.78 FZ 2.43 278 FX -14.5 FZ -2.78 FZ -	453
115 FD 214.72 FY 137 L5 - 2.35 116 FD 214.72 FY 137 L5 - 2.35 116 FD 214.62 FY - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FY -58.02 FZ 33.91 135 FX 110.45 FY -58.54 FZ 34.32 275 FX -9.84 FY -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 1.35 277 FX -13.5 FY -2.78 FZ 2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.45 278 FX -14.5 FY -2.78 FZ	453
115 FD 214.72 FY 137 L5 - 2.35 116 FD 214.72 FY 137 L5 - 2.35 116 FD 214.62 FY - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FY -58.02 FZ 33.91 135 FX 110.45 FY -58.54 FZ 34.32 275 FX -9.84 FY -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 1.35 277 FX -13.5 FY -2.78 FZ 2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.45 278 FX -14.5 FY -2.78 FZ	451
115 FD 214.72 FY 137 L5 - 2.35 116 FD 214.72 FY 137 L5 - 2.35 116 FD 214.62 FY - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FY -58.02 FZ 33.91 135 FX 110.45 FY -58.54 FZ 34.32 275 FX -9.84 FY -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 1.35 277 FX -13.5 FY -2.78 FZ 2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.45 278 FX -14.5 FY -2.78 FZ	45 <u>1</u>
115 FD 214.72 FY 137 L5 - 2.35 116 FD 214.72 FY 137 L5 - 2.35 116 FD 214.62 FY - 0.92 FZ - 2.16 ***05-107-3-WAS 312 FX -110.35 FY -58.02 FZ 33.91 135 FX 110.45 FY -58.54 FZ 34.32 275 FX -9.84 FY -1.06 FZ 1.35 276 FX -9.33 FY -2.16 FZ 1.35 277 FX -13.5 FY -2.78 FZ 2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.43 278 FX -14.5 FY -2.78 FZ -2.78 FZ -2.45 278 FX -14.5 FY -2.78 FZ	—— 45 <u>1</u>
115 FF 214.72 FY -13.1 F2 -2.12 116 FF 214.62 FY -0.52 FZ -2.16 ***F5-INT-3-WAS 116 FF 214.62 FY -0.53 FZ -2.16 ***F5-INT-3-WAS 117 F110.35 FY -156.02 FZ 33.12 115 FF 2110.35 FY -156.72 FZ 3.12 115 FF 2110.45 FY -36.5 FZ 3.43 115 FF 2110.45 FY -36.5 FZ 3.43 127 FF -31.38 FY -2.51 FZ 2.05 127 FF -31.38 FY -2.51 FZ 2.05 127 FF -31.52 FY -3.5 FZ 3.42 128 FF -120.41 FY -3.65 FZ 3.43 128 FF -120.41 FY -3.65 FZ 3.43 128 FF -22.68 FY -3.51 FZ 4.165 128 FF -22.68 FY -3.61 FZ 4.165 128 FF -22.68 FY -3.61 FZ 4.165 128 FF -22.68 FY -3.61 FZ 4.165 128 FF -22.71 FY -3.19 FZ 4.164 128 FF -22.71 FY -3.19 FZ 4.164 129 FF -23.75 FF -2.57 FZ -3.19 129 FF -23.75 FF -2.57 FZ -3.19 120 FF -25.64 FY -6.68 FZ 2.01 128 FF -25.75 FY -2.39 FZ 4.164 129 FF -25.75 FY -2.39 FZ 4.64 129 FF -25.75 FY -2.39 FZ -3.64 129 FF -25.75 FY -2.39 FZ -3.64 120 FF -26.75 FY -2.57 FZ -3.57 130 FF -26.75 FY -2.57 FZ -2.17 130 FF -26.77 FY -2.57 FZ -2.17 130	453
115 FF 214.72 FF -131 FF -2.52 116 FF 214.62 FF -0.52 FZ -2.16 ************************************	453



2326-K3P-R4b-Deg.std 400 PX 18.46 PY -1.31 PZ -5.35 539 FX 17.42 PY -1.36 PZ -4.97 539 FX 17.42 PY -1.66 PZ -4.97 539 FX 17.43 PY -1.66 PZ -4.97 539 FX 17.43 PY -1.66 PZ -4.47 539 FX 16.47 PY -0.69 FZ -3.62 539 FX 6.39 FY -0.68 PZ -2.81 539 FX 16.47 PY -0.68 PZ -2.81 527 FX 3.17 PT 0.27 FZ -2.54 170 FX -5.76 FY 2.39 FZ 5.33 171 FX -5.87 FX 3.15 FZ 6.48 571 FX -11.69 FY 1.57 FZ 8.48 571 FX -15.53 FY -0.42 FZ 10.63 578 FX -15.57 FY -0.42 FZ 10.63 578 FX -16.26 FY -0.57 FZ 12.67 585 FX -16.26 FY -0.57 FZ 12.67 585 FX -16.26 FY -0.57 FZ 12.45 597 FX -16.26 FY -0.57 FZ 12.45 597 FX -16.26 FY -0.57 FZ 12.46 597 FX -16.26 FY -0.57 FZ 1.54 597 FX -16.27 FY -1.57 FZ 5.41 597 FX -16.27 FY -1.57 FZ 5.41 597 FX -16.26 FY -1.57 FZ 5.41 597 FX -16.26 FY -1.57 FZ 5.44 597 FX -16.27 FY -1.57 FZ 5.44 597 FX -16.26 FY -1.57 FZ 5.44 597 FX -16.27 FY -1.57 FZ 5.44 597 FX -16.47 FY -1	- 459
07 FX -3.47 FY -3.28 F2 4.38 07 FX -3.47 FY -3.28 F2 4.38 07 FX -0.12 FY 0.64 F2 0.34 FX -0.12 FY 0.64 F2 0.34 FX -0.12 FY 0.64 F2 0.34 1FX -0.12 FY 0.64 F2 0.34 1FX -0.12 FY 0.47 F2 3.6 1FX -0.31 FY 1.62 F3 3.27 15 FX 11.8 FY 0.47 F2 3.6 15 FX 11.8 FY 0.47 F2 3.6 15 FX 11.8 FY 0.47 F2 3.6 15 FX 11.8 FY -0.19 F2 3.86 15 FX 13.6 FY -0.19 F2 3.86 15 FX 13.6 FY -0.19 F2 3.64 17 FX -5.7 FY 0.018 F2 -3.42 FX -5.7 FY 0.18 F2 -3.42 FX -5.7 FY 0.31 F2 -5.93 FX -10.54 FY 0.31 F2 -5.84 17 FX -10.54 FY 0.37 F2 -7.46 17 FX -10.54 FY 0.47 F2 -7.46 17 FX -10.47 FY 0.47 F2 -7.47 18 FX -10.57 FY 0.47 F2 -7.40 18 FX -10.57 FY 0.47 F2 -7.40 19 FX -10.47 FY 0.40 F2 -7.12 19 FX -10.47 FY 0.40 F2 -7.12 19 FX -10.47 FY 0.40 F2 -7.12 10 FX -10.47 FY 0.40 F2 -7.1	
0236-KSP-B4b-Deg.std 232 IK -17.44 FY -0.21 F2 4.21 232 IK -17.46 FY -0.21 F2 4.22 233 IK -17.64 FY 0.91 F2 4.23 234 IK -17.46 FY 0.91 F2 4.29 235 IK -17.0 FY 0.91 F2 4.29 237 IK -17.0 FY 0.91 F2 4.09 238 IK -16.58 FY 1.37 F2 3.92 308 IK -16.58 FY 1.37 F2 3.92 308 IK -16.58 FY 1.37 F2 3.92 308 IK -16.58 FY 1.37 F2 3.09 308 IK -16.58 FY 1.37 F2 3.23 308 IK -16.58 FY 1.37 F2 3.09 308 IK -16.58 FY 1.37 F2 3.02 308 IK -10.37 FY 1.35 F2 1.62 308 IK -10.37 FY 1.35 F2 1.62 308 IK -10.37 FY 1.35 F2 1.55 317 F3 5.05 FY 1.37 F2 3.05 316 IK -10.17 FY -1.38 F2 1.02 46 IK 1.07 FY -1.38 F2 1.02 46 IK 1.07 FY -1.38 IF2 1.02 46 IK 1.07 FY -1.38 IF2 1.02 46 IK 1.07 FY -1.39 IF2 2.33 46 IK 1.08 FY -1.77 F2 3.74 47 F1 -1.07 F2 3.15 47 F1 -1.07 FY -1.48 F2 3.15 47 F1 -1.07 FY -1.48 F2 3.15 47 IK 1.76 FY -1.48 F2 3.15 47 IK 1.76 FY -1.48 F2 3.15 48 IK 1.07 FY -1.48 F2 3.15 48 IK 1.07 FY -1.48 F2 4.23 47 IK 1.76 IY 0.47 F2 4.28 47 IK 1.76 IY 0.47 F2 4.28 47 IK 1.76 IY 0.47 F2 4.28 47 IK 1.76 IY 0.47 F2 4.28 48 IK 1.62 IY 1.77 F3 3.74 48 IK 1.62 IY 1.77 F3 5.75 3.74 48 IK 1.62 IY 1.77 F3 5.75 3.74 48 IK 1.62 IY 1.77 F3 5.75 3.75 51 IK 1.74	- &6:

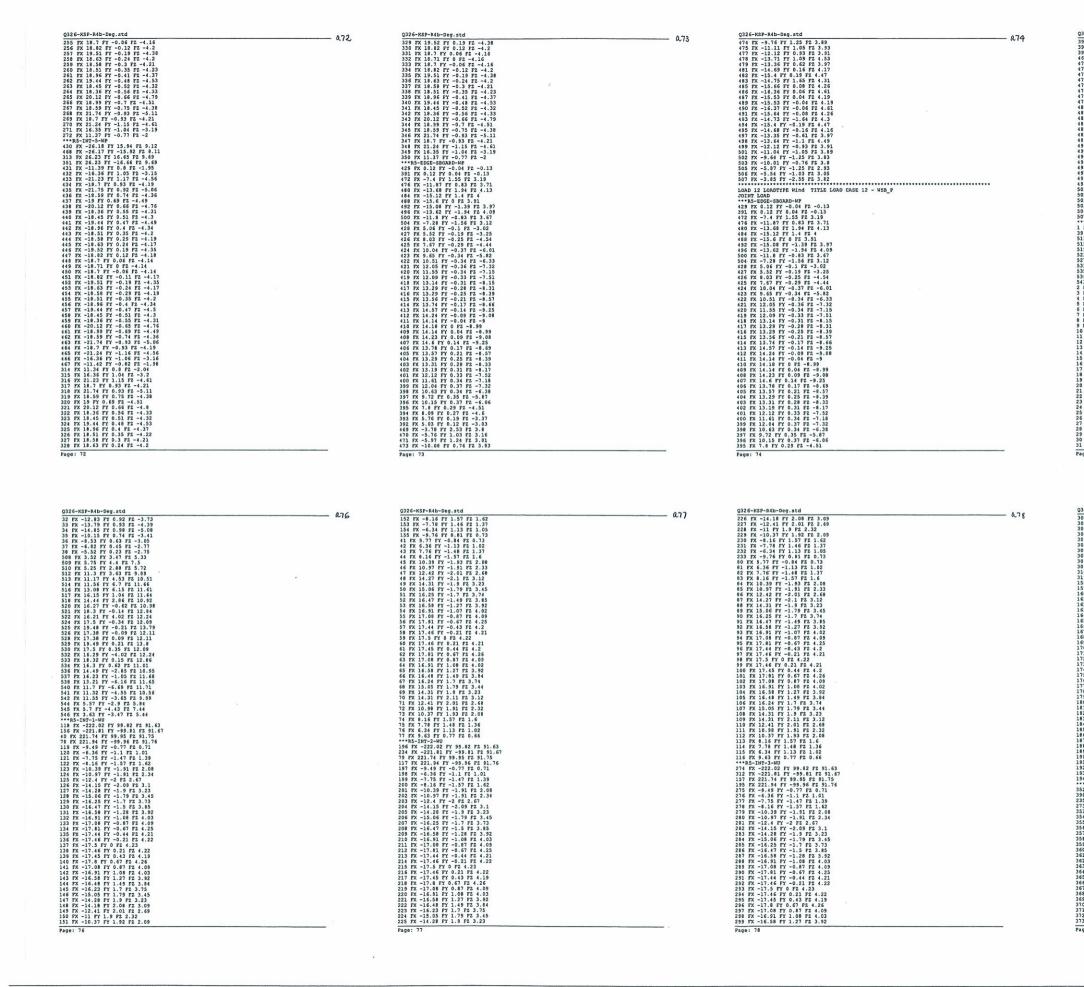
126

Anhalt University of Applied Sciences, Dessau

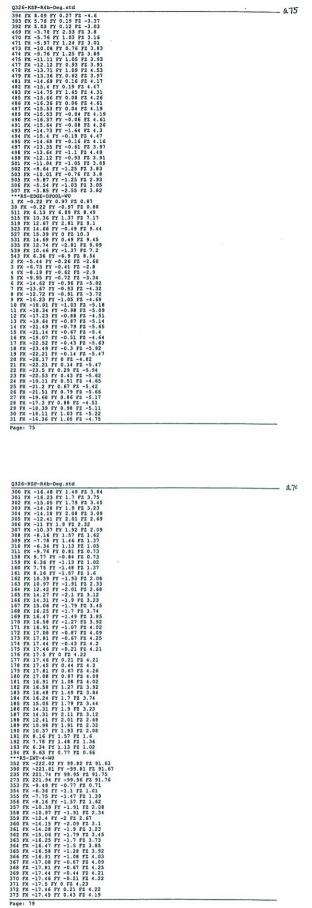


26-K5P-R45-Deg.std 26-K5P-R45-Deg.std 27K-0.22 FY -0.57 FE 0.88 1 FK 0.13 FY 6.88 FE 0.48 5 K 10.36 FY 2.81 FE 0.17 9 FX 12.67 FY 2.81 FE 0.13 15 K 14.66 FY -0.49 FE 0.44 7 FX 15.35 FY 0.75 10.3 15 K 14.65 FY 0.45 FE 0.45 9 FX 10.45 FY -1.37 FE 7.2 3 FK 0.35 FY -5.97 FE 7.2 3 FK 0.35 FY -6.9 FE 0.54 5 FX 10.45 FY -6.97 FE 7.2 3 FK 0.35 FY 0.59 FE 7.2 5 FK 0.54 FY -5.97 FE 7.2 5 FK 0.54 FY 0.54 FE 0.54 5 FK 0.55 FY 0.54 FK 0.54 FK 0.54 FK 0.55 FK	6.
The second sec	
FX         15.49         FY         10.31         FZ         10.32         FZ         -6.66         FZ         10.32         FZ         -6.66         FZ         10.71         FZ         10.55         FZ	
226-KSF-R4b-Deg.std       A7         13 FX 16.5 FY -0.3 FZ -4.23         14 FX 16.5 FY -0.3 FZ -4.23         15 FX 16.5 FY -0.4 FZ -4.23         16 FX 16.5 FY -0.4 FZ -4.23         17 FX 20.12 FY -0.5 FZ -4.32         16 FX 16.5 FY -0.4 FZ -4.33         17 FX 20.12 FY -0.5 FZ -4.32         18 FX 16.5 FY -0.4 FZ -4.33         17 FX 20.12 FY -0.5 FZ -4.34         18 FX 16.5 FY -0.5 FZ -4.31         18 FX 16.5 FY 1.05 FZ -4.35         18 FX 16.5 FY 1.05 FZ -4.35         18 FX 16.5 FY 1.05 FZ -4.35         18 FX 16.5 FY 0.55 FZ -4.36         18 FX 16.5 FY 0.55 FZ -4.35         18 FX 16.5 FY 0.55 FZ -4.36         18 FX 16.5 FY 0.55 FZ -4.35         18 FX 16.5 FY 0.55 FZ -4.36         18 FX 16.5 FY 0.55 FZ -4.31         18 FX 10.5 FY 0.55	71

Anhalt University of Applied Sciences, Dessau 🦛 

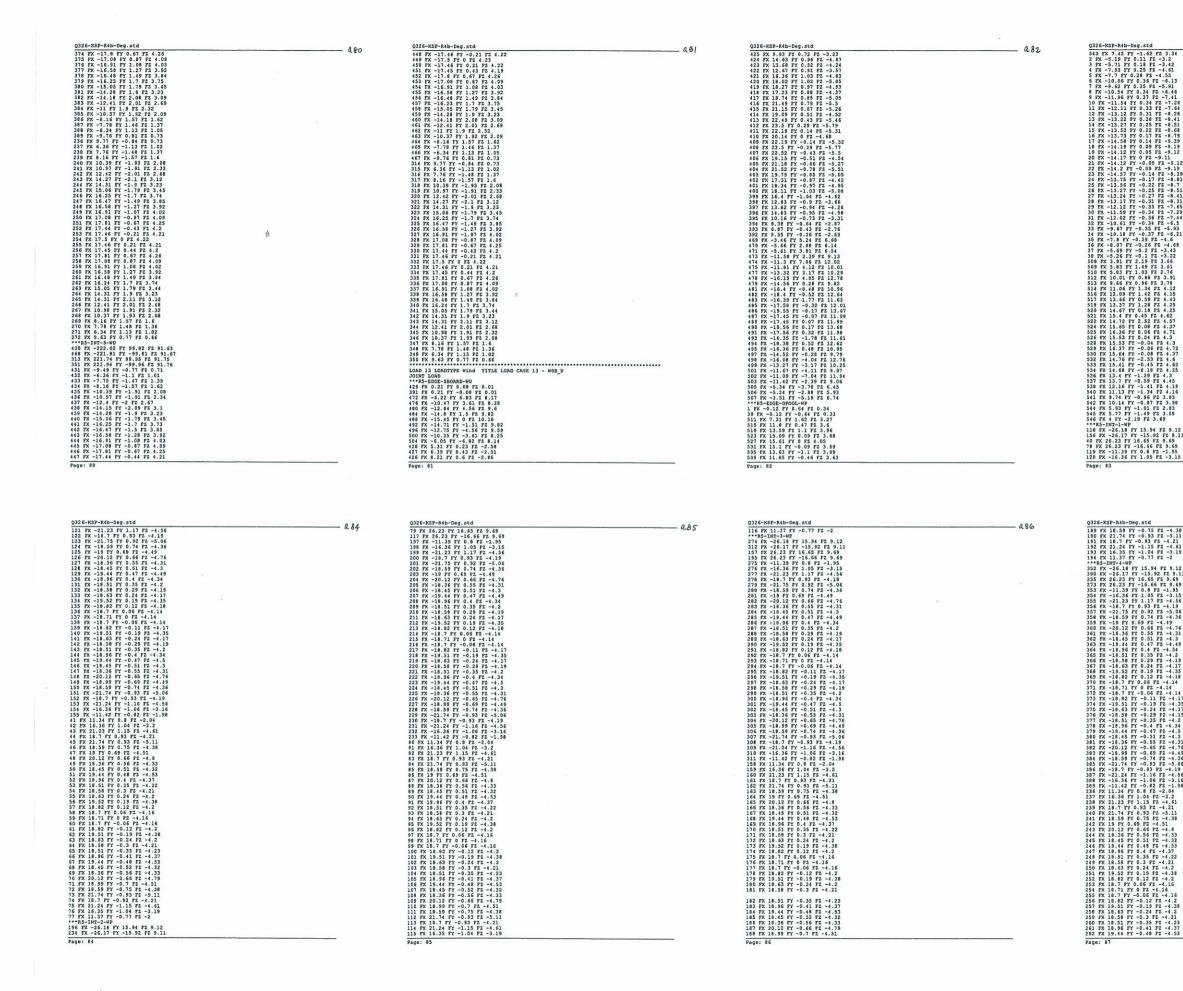








Anhalt University of Applied Sciences, Dessau



TAN SIEW MOI

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

Institute for Membrane and Shell Technologies



$\begin{array}{c} \textbf{X} & -1.19 \ \textbf{rf} & 0.09 \ \textbf{Z} & -3.19 \\ \textbf{Y} & -1.12 \ \textbf{rf} & 0.09 \ \textbf{Z} & -3.12 \\ \textbf{F} & -1.13 \ \textbf{Ff} & 0.68 \ \textbf{Z} & -3.12 \\ \textbf{F} & -1.13 \ \textbf{Ff} & 0.68 \ \textbf{Z} & -3.12 \\ \textbf{F} & -1.13 \ \textbf{Ff} & 0.68 \ \textbf{Z} & -3.12 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{Z} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.18 \\ \textbf{F} & -3.15 \ \textbf{Ff} & -0.23 \ \textbf{F} & -7.45 \\ \textbf{F} & -3.13 \ \textbf{Ff} & -0.33 \ \textbf{F} & -7.45 \\ \textbf{F} & -3.13 \ \textbf{Ff} & -0.33 \ \textbf{F} & -7.45 \\ \textbf{F} & -3.13 \ \textbf{Ff} & -0.33 \ \textbf{F} & -7.45 \\ \textbf{F} & -3.13 \ \textbf{Ff} & -0.34 \ \textbf{F} & -5.5 \\ \textbf{F} & -3.64 \ \textbf{Ff} & -0.34 \ \textbf{F} & -5.5 \\ \textbf{F} & -3.64 \ \textbf{Ff} & -0.34 \ \textbf{F} & -5.4 \\ \textbf{F} & -3.25 \ \textbf{Ff} & -0.37 \ \textbf{F} & -3.62 \\ \textbf{F} & -3.64 \ \textbf{Ff} & -0.37 \ \textbf{F} & -3.46 \\ \textbf{F} & -3.64 \ \textbf{Ff} & -0.37 \ \textbf{F} & -3.46 \\ \textbf{F} & -3.62 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.46 \\ \textbf{F} & -3.26 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.46 \\ \textbf{F} & -3.26 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.46 \\ \textbf{F} & -3.26 \ \textbf{Ff} & -0.17 \ \textbf{F} & -3.46 \\ \textbf{F} & \textbf{F} & 3.91 \ \textbf{F} & 3.66 \\ \textbf{F} & 5.36 \ \textbf{Ff} & 0.91 \ \textbf{F} & 3.78 \\ \textbf{F} & 5.36 \ \textbf{Ff} & 0.98 \ \textbf{Ff} & 3.78 \\ \textbf{F} & 1.06 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 3.16 \\ \textbf{F} & 1.06 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.15 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.10 \\ \textbf{F} & 1.106 \ \textbf{Ff} & 1.49 \ \textbf{Ff} & 4.10 \\ \textbf{F} & 1$	_
26-KSP-R4b-Deg.std	- <i>a</i> 87
$ \begin{array}{c} \begin{array}{c} & 1.5 \\ 1.5$	

All	a 92 RAD-FAB2	Job No TPL- zansed to Transerve Pro Lid	40581 a 93 Rev speed 32.5 m/s	Solvan Renaed to Transerva Pile LLd	Job No         Deat No         Rev           TPL40581         a 94         R4b-FAB2           Perflwind speed 32.5 m/s	Solverse Scienced to Trans true Pie LM	Perfiving speed 32.5 m/s
Ref Fabric RS	Jeb Tile Wisma Bella S			Jeb Tile Wisma Bella Swimming Pool	Ref Fabric R5	Jeh Tite Wisma Bella Swimming Pool	Ral Fabric R5 By TSM Dality Dec.11 Ord TC
1011 11-	eo-11 CM TSM Delo/Time 10-Jul-2012 16:43 Cfent Majlis Perbanc	idaran Kuanlan Re 0326	-KSP-R4b-Deg.sld Date/Time 10-Jul-2012 16:43	Client Majilis Perbandaran Kuantan	By         TSM         Dais17-Dec-11         Did TSM           Pile         Q326-KSP-R4b-Deg.std         Dais707e         10-Jul-2012 15:43	Clent Majlis Perbandaran Kuantan	Py TSM Dele17-Dec-11 Chd TS File Q326-KSP-R4b-Deg.std Date/Time 10-Jul-2
Vertical         Marane           750         105         105           101         115         105           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115           101         115         115         115           101         115         115         115           101         115         115         115           101         115         115         115           101         115         115         115           101         115         115	14.040           14	Interaction         Vertices         Journal           78         79         78         74           78         78         78         74           78         78         74         74           50         74         75         74         74           50         74         74         74         74           50         71         71         71         71         71           50         71         71         71         71         71         71         71           50         71		Partine Term       Term <td>1015 Malba 21</td> <td>Reaction Cont_st           Image: An intermed processing of the intermed procesing of the intermed processing of the intermed procesin</td> <td>702.16</td>	1015 Malba 21	Reaction Cont_st           Image: An intermed processing of the intermed procesing of the intermed processing of the intermed procesin	702.16

TAN SIEW MOI

Q326-KSP-R4b-Deg.std	 Q326-KSP-
263 FX 18.45 FY -0.52 FZ -4.32	 337 FX 16
264 FX 18.36 FY -0.56 FZ -4.33	338 FX 16
265 FX 20.12 FY -0.66 FZ -4.79 266 FX 18.99 FY -0.7 FZ -4.51	339 FX 18 340 FX 19
267 FX 18.59 FY -0.75 F2 -4.38	341 FX 18
268 FX 21.74 FY -0.93 FZ -5.11	342 FX 18
269 FX 18.7 FY -0.93 FZ -4.21	343 FX 20
270 FX 21.24 FY -1.15 FZ -4.61 271 FX 16.35 FY -1.04 FZ -3.19	344 FX 18 345 FX 18
272 FX 11.37 FY -0.77 FZ -2	346 FX 21
***R5-INT-5-WP	347 FX 18
430 FX -26.18 FY 15.94 FZ 9.12	348 FX 21
468 FX -26.17 FY -15.92 FZ 9.11 313 FX 26.23 FY 16.65 F2 9.69	349 FX 16 350 FX 11
351 FX 26.23 FY -16.66 FZ 9.69	********
431 FX -11.39 FY 0.8 FZ -1.95	* SERVICE
432 FX -16.36 FY 1.05 FZ -3.15 433 FX -21.23 FY 1.17 FZ -4.56	LOAD COME
434 FX -18.7 FY 0.93 FZ -4.19	1 1.0 2 1
435 FX -21.75 FY 0.92 FZ -5.06	
436 FX -18.59 FY 0.74 FZ -4.36	LOAD COMB
437 FX -19 FY 0.69 FZ -4.49 438 FX -20.12 FY 0.66 FZ -4.76	1 1.0 2 1
439 FX -18.36 FY 0.55 FZ -4.31	LOAD COMB
440 FX -18.45 FY 0.51 F2 -4.3	1 1.0 2 1
441 FX -19.44 FY 0.47 FZ -4.49 442 FX -18.96 FY 0.4 FZ -4.34	LOAD COMB
443 FX -18.51 FY 0.35 FZ -4.2	1 1.0 2 1
444 FX -18.58 FY 0.29 FZ -4.19	
445 FX -18.63 FY 0.24 F2 -4.17 446 FX -19.52 FY 0.19 F2 -4.35	LOAD COMB 1 1.0 2 1
447 FX -18.82 FY 0.12 FZ -4.18	
448 FX -18.7 FY 0.06 FZ -4.14	LOAD COMB
449 FX -18.71 FY 0 FZ -4.14 450 FX -18.7 FY -0.06 FZ -4.14	1 1.0 2 1
451 FX -18.82 FY -0.11 FZ -4.17	LOAD COMB
452 FX -19.51 FY -0.19 FZ -4.35	1 1.0 2 1
453 FX -18.63 FY -0.24 FZ -4.17	****
454 FX -18.58 FY -0.29 FZ -4.19 455 FX -18.51 FY -0.35 FZ -4.2	LOAD COMB 1 1.0 2 1
456 FX -18.96 FY -0.4 FZ -4.34	****
157 FX -19.44 FY -0.47 FZ -4.5	LOAD COMB
458 FX -18.45 FY -0.51 FZ -4.3 459 FX -18.36 FY -0.55 FZ -4.31	1 1.0 2 1
160 FX -20.12 FY -0.65 FZ -4.76	LOAD COMB
161 FX -18.99 FY -0.69 FZ -4.49	1 1.0 2 1
162 FX -18.59 FY -0.74 FZ -4.36 163 FX -21.74 FY -0.93 FZ -5.06	· ULTIMAT
164 FX -18.7 FY -0.93 FZ -4.19	
165 FX -21.24 FY -1.16 FZ -4.56	LOAD COMB
166 FX -16.36 FY -1.06 FZ -3.16	1 1.4 2 1
167 FX -11.42 FY -0.82 FZ -1.98 814 FX 11.34 FY 0.8 FZ -2.04	LOAD COMB
315 FX 16.36 FY 1.04 FZ -3.2	1 1.4 2 1
16 FX 21.23 FY 1.15 FZ -4.61	
17 FX 18.7 FY 0.93 FZ -4.21 18 FX 21.74 FY 0.93 FZ -5.11	LOAD COMB 1 1.0 2 1
119 FX 18.59 FY 0.75 FZ -4.38	
20 FX 19 FY 0.69 FZ -4.51	LOAD COMB
21 FX 20.12 FY 0.66 FZ -4.8 22 FX 18.36 FY 0.56 FZ -4.33	1 1.2 2 1
123 FX 18.45 FY 0.51 FZ -4.32	LOAD COMB
24 FX 19.44 FY 0.48 FZ -4.53	1 1.2 2 1
25 FX 18.96 FY 0.4 FZ -4.37	
26 FX 18.51 FY 0.35 FZ -4.22 27 FX 18.58 FY 0.3 FZ -4.21	LOAD COMB 1 1.2 2 1
28 FX 18.63 FY 0.24 FZ -4.2	
29 FX 19.52 FY 0.19 FZ -4.30	LOAD COMB
30 FX 18.82 FY 0.12 FZ -4.2 31 FX 18.7 FY 0.06 FZ -4.16	1 1.2 2 1
32 FX 18.71 FY 0 FZ -4.16	LOAD COMB
33 FX 18.7 FY -0.06 FZ -4.16	1 1.0 2 1.
34 FX 18.62 FY -0.12 FZ -4.2	
135 FX 19.51 FY -0.19 FZ -4.38 136 FX 18.63 FY -0.24 FZ -4.2	LOAD COMB 1 1.2 2 1.

B

Client Majils Per Reactions

 Press
 Press

 778
 1.5.5

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2
 1.5.2

 1.5.2

Val TeneDala: 1102/2012 17-2

Q326-KSP-R4b-I	Deg.std
338 FX 18.51 1 339 FX 18.96 1 340 FX 19.44 1	FY -0.3 FZ -4.21 FY -0.35 FZ -4.23 FY -0.41 FZ -4.37 FY -0.48 FZ -4.53
342 FX 18.36 1 343 FX 20.12 1 344 FX 18.99 1	FY -0.52 F2 -4.32 FY -0.56 F2 -4.33 FY -0.66 F2 -4.79 FY -0.76 F2 -4.51
346 FX 21.74 H 347 FX 18.7 F1 348 FX 21.24 H	$\begin{array}{c} rr & -0.75 \ rz & -4.38 \\ rr & -0.39 \ rz & -5.11 \\ rr & -0.39 \ rz & -4.21 \\ rr & -1.15 \ rz & -4.61 \\ rr & -1.15 \ rz & -4.61 \\ rr & -1.17 \ rz & -4.61 \\ rr & -1.17 \ rz & -1.52 \end{array}$
* SERVICE LOAD LOAD COMB 100 1 1.0 2 1.0 4	D COMBINATION (SW+DCW+PRE)
LOAD COMB 101 1 1.0 2 1.0 3	(SW+DCW+LCW+VL) 1.0 5 1.0
LOAD COMB 102 1 1.0 2 1.0 6	1.0
LOAD COMB 103 1 1.0 2 1.0 7	1.0
LOAD COMB 104 1 1.0 2 1.0 8	1.0
LOAD COMB 105 1 1.0 2 1.0 9	(SW+DCW+WAS) 1.0 (SW+DCW+WDP P)
1 1.0 2 1.0 10	(SW+DCW+WDP_0)
1 1.0 2 1.0 11 LOAD COMB 108	1.0
1 1.0 2 1.0 12	2 1.0 (SW+DCW+WSB U)
. ULTIMATE LOA	D COMBINATION
	1.4 (SR+DCN+PRE) 1.0
LOAD COMB 201 1 1.4 2 1.4 3	1.4 (SW+DCW)+1.6 (CDW+VL) 1.6 5 1.6
1 1.0 2 1.0 6	
1 1.2 2 1.2 7	
1 1.2 2 1.2 8	1.2 (SH+DCH)+1.2WEN 1.2 1.2 (SH+DCH)+1.2WAS
1 1.2 2 1.2 9	1.2 (SN+DCW) +1.2 (MDP P)
LOAD COMB 207	1.2 1.0 (SW+DCW)+1.4 (WDP U)
LOAD COMB 208	1.4
1 1.2 2 1.2 12	1.2

Q326-KSP-R4b-Deg.std	. 0.
****	a90
LOAD COMB 209 1.0 (SW+DCW)+1.4 (WSB_U)	
1 1.0 2 1.0 13 1.4	
***************************************	
PERFORM ANALYSIS PRINT STATICS CHECK	
LOAD LIST ALL	
PARAMETER 1 CODE BS5950	
PY 275000 MEMB 1 TO 2255	
CHECK CODE ALL	
PRINT CG	
STEEL TAKE OFF LIST 1 TO 2275	
FINISH	

2				TPL40581	Sheet No	a 91	Rev R4b-FA		
2	Software licensed to Transerve Pie Lid			Partwind speed 32.5 m/s					
	Wisma Bela Swimming Pool			Ref Fabric R5					
	-			By TSM	Dele17-D	lec-11 Ch	TSM		
Majis Pe	erbandatan K	luantan		11 Q326-KSP-F			Jul-2012 16:43		
Job Info	rmation								
	Engineer	Checked	Approved						
Name:	TEM	TSM							
Date:	17-Dec-11	07-Mar-12							
Lann I		1							
Comments									
Structure Typ	. SPACE F	Nume							
Number of Nor Number of Ele Number of Bas Number of Cor	des 9: manis 72:	KULLE Highasi Node 5 Highasi Beam 13 Cases 20	314 2275				J		
Number of Nor Number of Ele Number of Bas Number of Cor	des 91 ments 223 sic Lood Cases mbination Load 1	ALARE	1 314						
Number of Nor Number of Ele Number of Bas Number of Con Included in this	des 91 ments 223 alc Load Cases mbination Load ( printed are data The Whole Sirv	ALARE	314 2276		0				
Number of Non Number of Ele Number of Bas Number of Cor Included in INIs All Included in INIs	des 5: ments 223 alc Load Cases mbination Load ( princeut are deta The Whole Stry princeut are resu	ALANE X   Highesi Node 5   Highesi Beam 13 Ceses 20 Ant Core Na for losd ceses:	314 2276						
Number of No Number of Ele Number of Ele Number of Con Included in INs, All Type	des 90 ments 223 sic Loed Cases mbination Load 1 printsur any dela The Whole Stay printsur any nesu UC	ALLARE XI (Teghasi Node TS (Teghasi Baam 13) Datas 20) for tore Name Name	314 2276						
Number of No: Number of Ele Number of Ele Number of Cor Included in Dis All Type Primary Primary Primary	des 95 ments 223 sic Loed Cases misnation Load 1 printsuf are dela The Whole Stor printsuf are resu LIC 1 2 3	AUME DX   Rephasi Node 15   Hephasi Bean 13 Cases 20 Mor. Same LGAD CASE 1-SW LGAD CASE 2-DOW LGAD CASE 3-LCW	314 2276						
Number of No. Number of Ele Number of Cor Number of No. Number of Cor Number of Cor Nu	des 50 ments 223 solution Lead 1 prints of any deta The Whole Stov prints of any ness UC 1 2 3 4	Will Highesi Node           Xil Highesi Node           Zil Highesi Baam           Utas           Stass           Zil           Br           Utas	314 2276						
Number of Not Number of Ele Number of Ele Number of Cor Included in INIs All Primary Primary Primary Primary Primary	des 9: ments 222 minist 222 ministration Load of printed are dete ministration Load of printed are dete ministration Load printed are dete printed are dete 1 1 2 3 4 5	Autor State	314 2276						
Number of Not Number of Ele Number of Ele Number of Ele Number of Co Included in this All Primary Primary Primary Primary Primary Primary	des 9: ments 72: sic Load Ceses mainston Lead 1 prinsul are dets The Whole Stor printod are result 1 2 3 4 5 6	All Highmail Node           12 Highmail Node           13 Highmail Room           10 John	314 2276						
Number of Noi Number of Dis Number of Dis Number of Dis Number of Cor Included in Dis Number of Cor Included in Dis Number Primary Primary Primary Primary Primary Primary Primary	des 5: mants 222 ministra 222 ministration Lead 1 ministration Lead 1 prime while Sch UC 1 1 2 3 4 5 6 7	All Highasi Node           12 Highasi Node           13 Highasi Node           13 Highasi Node           13 Jane           13 Jane           13 Jane           14 Highasi Node           14 Highasi Node           15 Highasi Node           16 Mighasi Node <td>914 2275</td> <td></td> <td></td> <td></td> <td></td>	914 2275						
Humber of Noi Humber of Dis Humber of Dis Humber of Cer Instructed in this All Instructed in this Primary Primary Primary Primary Primary Primary Primary Primary Primary Primary	des 90 ments 222 stic Lead Cases mbination Lead 1 printeur an data The Whole Sav philout an result UC 1 2 3 4 5 6 7 7 8	All Highmail Node           12 Highmail Node           13 Highmail Room           13 Highmail Room           13 Highmail Room           14 Highmail Node           15 Highmail Room           16 Joint Conternation           16 Joint Conternation           10 Joint Conternation	914 2275						
Number of Noi Number of Dis Number of Dis Number of Dis Number of Cor Included in Dis Number of Cor Included in Dis Number Primary Primary Primary Primary Primary Primary Primary	des 5: mants 222 ministra 222 ministration Lead 1 ministration Lead 1 prime while Sch UC 1 1 2 3 4 5 6 7	All Highasi Node           12 Highasi Node           13 Highasi Node           13 Highasi Node           13 Jane           13 Jane           13 Jane           14 Highasi Node           14 Highasi Node           15 Highasi Node           16 Mighasi Node <td>94 2275</td> <td></td> <td></td> <td></td> <td>]</td>	94 2275				]		
Number of Noi Number of Die Number of Die Number of Die Number of Col Included in Ible, All Primary Primary Primary Primary Primary Primary Primary Primary Primary Primary Primary Primary Primary	dea 90 menta 222 bit Lead Cases ministion Lead 1 protect any dela The Whole Stor UC 1 2 3 4 5 5 6 7 7 8 8	Basel         Telephani Node           12         Helphani Node           13         Helphani Node           14         Helphani Node           15         Helphani Node           10         Data           11         Info Instance           12         Helphani Node           13         Info Instance           14         Helphani Node           15         Helphani Node           16         Info Instance	*						
Aumber of No Number of Els Number of Els Number of Els Number of Co Number of Co Number of Co Number of Co Number Primary Prim	des 90 meetu 222 bit Loed Ceses mininsion Lead 1 printeut em dela The Whole Stov UC 1 1 2 3 5 6 7 7 8 8 9 10	All Helphani Node           Si Helphani Node           Si Helphani Node           Si Helphani Node           Bar           Construction           International States           Name           International States           Name           International States           Name           International States	9 9 7 7 7 7 9						
Number of Noi Humber of Dai Humber of Dai Number of Dai Number of Cet Humber of Cet Humber of Cet Holded in Dia Primary Primar	fee 91 and 12 an	All Fliphasi Node           I Fliphasi Node           I Fliphasi Node           I Si Fliphasi Node           I Si Markan           I Si Markan <tr< td=""><td></td><td></td><td></td><td></td><td></td></tr<>							
Number of Noi Number of Noi Number of Da Number of Da Number of Co Internet of Co Internet of Co Internet of Co Internet Primary Prima	fea         91           mania         223           skic Load Cases         mainsion Lead           mainsion Lead         mainsion Lead           phileur an dela         mainsion           Ta         Mainsion           1         3           4         5           6         7           8         8           10         10           11         12           12         13           100         10	AME X   Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi San 1 Tephasi Tephasi Tephasi 1 Tephasi 1 Tephasi Tephasi	9 7 7 7 7 7 7 7 7 7 7 7 7 7						
Number of Noi Humber of Dai Humber of Dai Number of Dai Number of Cer- holured in Dia Ali Primary Prim	Sea         31           manks         272           bit Land Cases         272           bit Land Cases         272           bit Land Cases         272           privery by data         272           bit Tay What Stype         272           1         1           3         6           7         8           8         9           10         11           12         3           10         10           101         101	ALLE         24         1 Septemi Node           21         1 Septemi Node         3           21         Septemi Node         3           21         Septemi Node         3           20         Septemi Node         3           20         Septemi Node         3           20         Septemi Node         Net           10.00         CASE 1 - Styre         Net           10.00         CASE 1 - Octor         Net           10.00         CASE 1 - Weit         Net	9 7 7 7 7 7 7 7 7 7 7 7 7 7						
Number of Noi Number of Noi Number of Da Number of Da Number of Co Internet of Co Internet of Co Internet of Co Internet Primary Prima	fea         91           mania         223           skic Load Cases         mainsion Lead           mainsion Lead         mainsion Lead           phileur an dela         mainsion           Ta         Mainsion           1         3           4         5           6         7           8         8           10         10           11         12           12         13           100         10	AME X   Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi Node 1 Tephasi San 1 Tephasi Tephasi Tephasi 1 Tephasi 1 Tephasi Tephasi	9 7 7 7 7 7 7 7 7 7 7 7 7 7						

Anhalt University of Applied Sciences, Dessau 🛹

C

	Image: Note:         Image: Note:<	www.wisma.belia.owimining.Poor		
Refining Cont           Import to the set of the s	Markardow     Markardow     Markardow     Markardow     Markardow       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001     1001     1001     1001     1001       10001     1001		Ref Fabric R5 By TSM Dale17-Dec-11 Cod TSM	Job Tide W
	Image: Note with the second	<sup>1</sup> Majlis Perbandaran Kuantan		Clent M
	No.         No. <th>Reactions Cont</th> <th></th> <th>Rea</th>	Reactions Cont		Rea
μαρο το	1000000000000000000000000000000000000	Horizonal         Vertical         Moment           Node         LIC         FX         FY         FZ         MX         MY         MZ		Ned
Normal Solution         Normal Solution         Normal Solution         Normal Solution           Normal Solution         Normal Solution	Notes         Notes <th< td=""><td>SLOAD CASE 66.135 -58.071 153.106 61.868 9.505 -0.235</td><td></td><td></td></th<>	SLOAD CASE 66.135 -58.071 153.106 61.868 9.505 -0.235		
	1000000000000000000000000000000000000	710AD CASE \$5,250 -69,519 193,210 64,710 14,191 -0,559		
	1000000000000000000000000000000000000	910AD CASE 124.839 111.614 75.352 463.097 35.831 4.313		
No. 1         No.1         No. 1         No. 1 <thn< td=""><td>Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality</td><td>12LDAD CASI 182.455 127.577 -193.452 -139.717 48.138 -18.937</td><td></td><td></td></thn<>	Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality         Normality         Normality         Normality         Normality         Normality         Normality           Normality	12LDAD CASI 182.455 127.577 -193.452 -139.717 48.138 -18.937		
1000000000000000000000000000000000000	Table 1000         Table 10000         Table 10000         Table 10000         Table 100000         Table 1000000 <td< td=""><td>100:(SW+DCN 51.875 -44.282 197.669 50.200 10.190 0.136</td><td></td><td></td></td<>	100:(SW+DCN 51.875 -44.282 197.669 50.200 10.190 0.136		
	1000000000000000000000000000000000000	1022(SW+DCM 140,232 81,255 47,390 48,843 24,872 4,837 1022(SW+DCM 106,180 -105,718 356,783 115,271 18,035 4,062		
	THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION           THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION           THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION         THE DESCRIPTION           THE DESCRIPTION <td>10435W+DCN 161.319 -43.939 89.749 438.322 29.591 0.742 10535W+DCN 135.770 85.418 248.535 412.535 40.875 4.809</td> <td></td> <td></td>	10435W+DCN 161.319 -43.939 89.749 438.322 29.591 0.742 10535W+DCN 135.770 85.418 248.535 412.535 40.875 4.809		
Number         Number         Number         Number         Number           Number         Number         Number         Number         Number         Number           Number         Number         Number         Number         Number         Number         Number           Number         Number         Number         Number         Number         Number         Number         Number           Number         Nu	Number 1000	187-15W+DCW 07.210 .105.725 358.545 115.285 28.183 .10.122		
Import Mod 1001 1001 1001 1001 1001 1001 1001 10	Normality         <	109:(SW+DCW 56.416 -105.794 338.783 115.529 -1.815 21.219 200:1.4(SW+D 56.247 42.761 267.098 70.424 11.728 0.337		IE
Normality         Normality         Normality         Normality         Normality           Normality         Normality         Norm	Normality of the state of t	202:(SW+DCM 191.952 132.283 -135.775 -144.604 33.283 -1.370		
No.         No.         No.         No.         No.           No.         No.         No.         No.         No.         No.         No.           No.         <	Normality     Normality     Normality     Normality	204:1.2(5W+D 193.582 -100.727 107.698 525.987 35.509 0.691		-
Image: 1000	No. 1000     No. 1000     No. 1000     No. 1000       No. 10000     No. 1000     No. 1000 <tr< td=""><td>205:1.2(5W+D 177.854 97.560 -48.542 -106.623 18.301 20.419 207:1.0(5W+D 131.735 -129.536 434.500 141.174 37.891 -27.039</td><td></td><td></td></tr<>	205:1.2(5W+D 177.854 97.560 -48.542 -106.623 18.301 20.419 207:1.0(5W+D 131.735 -129.536 434.500 141.174 37.891 -27.039		
•••••••••••••••••••••••••••••	100000000000000000000000000000	209:1.0(5W+D 74.610 -129.632 404.867 141.516 -4.078 29.508		808
Normality         Normality         Normality         Normality           Normality         Normality	add cold (1)          add cold (1)         add c	21.0AD CASE -0.239 16.266 28.067 -25.022 -0.294 -0.109		
Normality         Normality         Normality         Normality           1000000000000000000000000000000000000	Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission         Non-transmission           Non-transmission         Non-transmission         Non-transmission         Non-transmission	410AD CASE 39.799 -1.521 29.022 1.734 45.683 0.199 510AD CASE 64.096 58.139 159.812 -98.841 73.233 -0.021		
Number         Number<	No. 2010	71,0AD CASE 92,239 59,597 203,463 -102,366 105,652 0,118	4.	i i i i i i i i i i i i i i i i i i i
Name         Name <th< td=""><td>13325252     1332     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       133325252     1332     1332     1332     1332       133325252     1332     1332     1332     1332       13332525252     1332     1332     1332     1332       13332525252     1332     1</td><td>81.DAD CASE 150.958 32.705 -69.453 -363.593 174.490 -0.385</td><td></td><td></td></th<>	13325252     1332     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       13325252     1332     1332     1332     1332       133325252     1332     1332     1332     1332       133325252     1332     1332     1332     1332       13332525252     1332     1332     1332     1332       13332525252     1332     1	81.DAD CASE 150.958 32.705 -69.453 -363.593 174.490 -0.385		
Numerica	NUMBER     Distance     Distance     Distance     Distance       NUMBER     NUMBER     NUMBER     NUMBER     NUMBER     NUMBER       NUMBER     NUMBER     NUMBER     NUMBER     NUMBER       NUMBER     NUMBER	11:LDAD CASI 86.338 59.809 196.895 -102.429 106.845 19.475 12LDAD CASI 180.855 -127.743 -168.533 219.376 220.058 18.849		
Numerica	Non-Solution         Non-Solution         Non-Solution         Non-Solution         Non-Solution           Name         Name </td <td>121.0AD CASI 41.238 58.576 167.721 -102.648 38.552 -21.065 100:JSW+DCW 49.200 44.352 208.167 -74.451 67.886 -0.306</td> <td></td> <td></td>	121.0AD CASI 41.238 58.576 167.721 -102.648 38.552 -21.065 100:JSW+DCW 49.200 44.352 208.167 -74.451 67.886 -0.306		
Name         Name <th< td=""><td>Signed Solution         Signed Sol</td><td>102(SW+DCN 135.587 -81.390 -23.173 142.906 157.222 0.855</td><td></td><td></td></th<>	Signed Solution         Signed Sol	102(SW+DCN 135.587 -81.390 -23.173 142.906 157.222 0.855		
Name         Name <th< td=""><td>Norm         Norm         <th< td=""><td>15435W+DCV 125.480 -60.414 272.851 411.027 155.754 -5.467 165.75W+DCV 159.358 78.978 110.892 -439.778 185.792 -0.899</td><td></td><td></td></th<></td></th<>	Norm         Norm <th< td=""><td>15435W+DCV 125.480 -60.414 272.851 411.027 155.754 -5.467 165.75W+DCV 159.358 78.978 110.892 -439.778 185.792 -0.899</td><td></td><td></td></th<>	15435W+DCV 125.480 -60.414 272.851 411.027 155.754 -5.467 165.75W+DCV 159.358 78.978 110.892 -439.778 185.792 -0.899		
Numerican services         Numerican servicon servicon services         Numerican services	Number Source 10         Number Source 10<	10525W+DCW 140,755 41,395 -15,850 142,918 155,681 -17,445 10725W+DCW 95,740 105,881 377,539 -178,605 118,947 18,972		
Image: Concern (Incorn Target)         Decision (Incorn Target)         D	District	108;5W+DCM 190,256 41.471 11.812 143.191 232.361 18.344 109;5W+DCM 50.639 105.948 347.866 -178.633 50.455 -21.570		IE
Image: Subject: State         Image: State         Imag	353 358 million     101 36 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 358 million     101 46 million     101 46 million     101 46 million       355 158 million     101 46 million     101 46 million     101 46 million       355 158 million     101 46 million     101 46 million     101 46 million </td <td>2011.4(5W+D 115.429 173.377 534.533 -386.762 134.115 -0.844 20215W+DCN 186.001 -132.455 -104.500 230.542 215.190 1.113</td> <td></td> <td></td>	2011.4(5W+D 115.429 173.377 534.533 -386.762 134.115 -0.844 20215W+DCN 186.001 -132.455 -104.500 230.542 215.190 1.113		
Image of the state         Image o	Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10       Sint Start 10     Sint Start 10     Sint Start 10     Sint Start 10     Sint 10       Sint Start 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint Start 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint Start 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint Start 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint Start 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint 10     Sint 10     Sint 10     Sint 10     Sint 10       Sint 10     Sint 10     Sint 10     Sint 10     S	204:1.2(5W+D 150.578 -72.496 327.421 493.222 188.153 -6.560		
Instrume	Sing Start 100 12000         Disk 10000         Disk 100000         Disk 100000         Disk 100000         Disk 100000         Disk 1000000         Disk 1000000         Disk 1000000         Disk 10000000         Disk 10000000         Disk 1000000000000000000000000000000000000	205:1.2(5W+D 165.918 -87.674 -21.673 171.501 185.818 -20.836		
Image of the state is a state if the state is a state state is a	State Control         State Contro         State Control         State Con	206:1.2(5W+D 226.367 -57.765 13.535 171.828 278.833 22.015 209:1.0(5W+D 67.154 128.819 414.954 -219.692 86.276 -29.996		
Laboration         Laboration <thlaboration< th="">         Laboration         Laborati</thlaboration<>	142000000000000000000000000000000000000	21.0AD CASE -0.199 -7.994 10.825 7.430 -0.489 0.620		
STAD_Prof for Windows 20.07.02.15     Materia Materia       STAD_Prof for Windows 20.07.02.15       Statute Instant Prof       Materia Based Instant Pro	NUMERAL 1733         STAAD.Pro for Windows 20.07.02.15         Proc Number 407         Proc Number 407           Address Lansan Process         Image Number 400 (Second Second	41,0AD CASE 9.825 2.275 -33.968 7.799 -4.958 -12.131		
Production         Production         Duity Decisity         Duity Decisity         Duity Decisity           Majity Pertundenten Kustein         PR 0226-KSP-Rde-Drg.std         Pendenten Kustein         PR 0226-KSP-Rde-Drg.std         Pendenten Kustein           Majity Pertundenten Kustein         PR 0226-KSP-Rde-Drg.std         Pendenten Kustein         House Free Kerner Kerner           Majity Pertundenten Kustein         PR 01106 Compression         Addition         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Majity Decisity         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Majity Decisity         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Frage         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Frage         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Frage         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Frage         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELLS THE WITCH Compression         Frage         Pendenten Kustein         Pendenten Kustein           20 ST PERDING STELS THE WITCH Compression         Frage <th>Prime         Prime         Design (Frack 0) (Checks Cont           16 Pertundamin Kuestan         Prime         Output         Prime         Data         Prime         Prime         Prime         Data         Prime         Data         Prime         Prime</th> <th></th> <th></th> <th></th>	Prime         Prime         Design (Frack 0) (Checks Cont           16 Pertundamin Kuestan         Prime         Output         Prime         Data         Prime         Prime         Prime         Data         Prime         Data         Prime			
Magins Pertundarian Kuantan         Prie Q326+CSP-R4b-Degiste         Marine 10-Jul-2012 10:43           Auk Witz Musel - Witz Musels Michards Mitzin Data Witz Musel - Marine Componential Mitzin Data Witz Musel - Marine Componential Data Witz Musel - Marine Componential Data Musel - Marine Componential Data Witz Musel - Marine Componential Data Musel - Marine Componential Data Witz Musel - Marine Componential Data Musel - Marine Componential Data Musel - Marine Componenia Data Witz Musel - Marine Componentia Data Musel - Marine Comp	Pre-Database Number         Pre-O326+45P-R46-Degstd         Destine 10-ub/2012 16:43           Design (Track 0) Chacks Cont 112 MA = Martin Contact Herits         Martine 10-ub/2012 16:43         S           T12 MA = Martin Contact Herits         Martine 10-ub/2012 16:43         S           T12 MA = Martin Contact Herits         Martine 10-ub/2012 16:43         S           T12 MA = Martin Contact Herits         Martine 10-ub/2012 16:43         S           T12 MA = Martin Contact Herits         Martine 10-ub/2012 16:43         S           T12 MA = Martin Contact Herits         A.33         S         S           T12 MA = Martin Contact Herits         A.33         S         S           T12 MARtin Herits         A.33         S         S         S           T12 MARtin Herits         Martin Herits         A.33         S		TPL40581         a 100         R4b-FAB2           Parkwind speed 32.5 m/s         Parkwind speed 32.5 m/s         R4b-FAB2	6
MAL WITE WATE WITE WITES WITEWAS WITEWAS WITE MALE ARE ALL ALL ALL ALL ALL ALL ALL ALL ALL AL	Table B         Weth Contact method within           Table B         Max B         M		TPL40581         a 100         R4b-FAB2           PwiWind speed 32.5 m/s         R4f Fabric R5	Jas Tris W
Desk         YALE         XETHEY         CHITCLE COMP         MAIN         Leading           23         27 <td< td=""><td>13 ALC - M ALS MARKAN FAMILY THE ATT OLITICAL POINT AND ALL A</td><td>Wisma Belia Swimming Pool</td><td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td><td>Jas Tris W</td></td<>	13 ALC - M ALS MARKAN FAMILY THE ATT OLITICAL POINT AND ALL A	Wisma Belia Swimming Pool	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jas Tris W
32 ST PUPINA         Rest         N=-4,2,2         -6,33         70           24 ST PUPINA         Rest         N=-4,2,2         -6,33         30           24 ST PUPINA         Rest         N=-4,2,2         -6,33         30           24 ST PUPINA         Rest         N=-4,2,2         6,33         30           25 ST PUPINA         Rest         N=-4,2,2         6,34         30           26 ST PUPINA         Rest         N=-4,2,2         6,34         30           26 ST PUPINA         Rest         N=-4,2,1         6,34         30           26 ST PUPINA         Rest         N=-4,2,3         6,34         30           26 ST PUPINA         Rest         N=-4,2,3	IF PHILLS     NI     NI     NI     NI       IF PHILLS     NI     NI     NI     NI       IF PHILLS     NI     NI       IF PHILLS <td>le Wisma Belia Swimming Pool Majitis Perbandaran Kuantan</td> <td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td> <td>Jao Tao y Crant y Ster</td>	le Wisma Belia Swimming Pool Majitis Perbandaran Kuantan	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jao Tao y Crant y Ster
11 10 100000 330000     10-14.2.2     0.2000       13 10 100000 33000     10-14.2.2     0.2000       14 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       16 10 100000 33000     10-14.2.2     0.2000       17 100000 33000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 11 100000 43000     10-14.2.2     0.2000       18 11 100000 43000     10-14.2.2     0.2000       18 11 100000 430000     10-14.2.2     0.2000	18         18<	le Wisma Bela Swimming Pool Majits Perbandaran Kuantan Siteel Design (Track 0) Checks Cont Ma Wutts Ma - NF HETE (Mikel ememiste Hette)	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	de tre u
11 10 100000 330000     10-14.2.2     0.2000       13 10 100000 33000     10-14.2.2     0.2000       14 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       15 10 100000 33000     10-14.2.2     0.2000       16 10 100000 33000     10-14.2.2     0.2000       17 100000 33000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 10 100000 43000     10-14.2.2     0.2000       18 11 100000 43000     10-14.2.2     0.2000       18 11 100000 43000     10-14.2.2     0.2000       18 11 100000 430000     10-14.2.2     0.2000	18         18<	le Wisma Bela Swimming Pool Majis Perbandaran Kuantan Siteel Design (Track 0) Checks Cont Maku unts Ma - NF HETE (Mikel ethematik enter Hober TABLE EXEMPT CHITCH COMP (MATER LEARING) FR (T) (LANDOL COMP (MATER LEARING)	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Child III
31 37 FURDAGE         FMAR         44-5,7,2         5,339         245           34 37 FURDAGE         FMAR         44-5,7,2         5,236         346           35 37 FURDAGE         FMAR         44-5,7,3         5,236         346           35 37 FURDAGE         FMAR         44-5,7,4         5,236         347           35 37 FURDAGE         FMAR         44-5,7,4         5,236         347           35 37 FURDAGE         FMAR         44-5,7         61,337         347           35 37 FURDAGE         FMAR         44-5,7         61,337         5,34           35 37 FURDAGE         FMAR         44-5,7         62,34         5,4           35 37 FURDAGE         FMAR         44-5,7         63,34         5,4           35 37 FURDAGE         FMAR         44-5,7         63,36         5,4           35 37 FURDAGE         FMAR         44-5,7         63,6         5,4           35 37 FURDAGE         FMAR	10         PUBLIC PAGE         PEC-12.2         5.39         PES           15         PUBLIC PAGE         FAS         5.40         1.01           15         PUBLIC PAGE         FAS         5.40         1.01           15         PUBLIC PAGE         FAS         5.40         1.01           16         PUBLIC PAGE         FAS         5.40         1.01           17         PUBLIC PAGE         FAS         5.40         1.01           18         PUBLIC PAGE         FAS         5.40         1.01           18         PUBLIC PAGE         FAS         5.41         1.01           19         FAS         FAS         5.43         1.01           19         FAS         FAS         5.43         1.01           19         FAS         FAS         5.43         1.01           19         FAS         FAS <td>le Wisma Bela Swimming Pool Majis Perbandaran Kuantan Siteel Design (Track 0) Checks Cont Maku unts Ma - NF HETE (Mikel ethematik enter Hober 1Mike Exempt) - Kittoja cemer Mattar (Anamer) Por Port</td> <td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td> <td>Jao Tito y Clash M Ster Att</td>	le Wisma Bela Swimming Pool Majis Perbandaran Kuantan Siteel Design (Track 0) Checks Cont Maku unts Ma - NF HETE (Mikel ethematik enter Hober 1Mike Exempt) - Kittoja cemer Mattar (Anamer) Por Port	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jao Tito y Clash M Ster Att
34 ST FUTURE 4         MAR         H=-1, 10         -2.30         54           37 ST FUTURE 4         MAR         H=-1, 10         -2.30         54           37 ST FUTURE 4         MAR         H=-1, 10         -2.30         54           37 ST FUTURE 4         MAR         H=-1, 12         -2.30         54           37 ST FUTURE 4         MAR         H=-1, 12         -2.30         54           38 ST FUTURE 4         MAR         H=-1, 12         -2.30         54           38 ST FUTURE 4         MAR         H=-1, 12         -2.30         54           38 ST FUTURE 4         MAR         H=-1, 12         -2.30         54           38 ST FUTURE 4         MAR         H=-1, 12         54         54           38 ST FUTURE 4         MAR         H=-1, 12         54         54           38 ST FUTURE 4         MAR         H=-1, 12         54         54           39 ST FUTURE 4         MAR         H=-1, 12         54         54           39 ST FUTURE 4         MAR         H=-1, 12         54         54           39 ST FUTURE 4         MAR         H=-1, 12         54         54           30 ST FUTURE 4         MAR         H=-1, 12	EF FURDLA RES LACT 10 6.20 14 ST FURDLA RES LACT 10 6.20 14	Wilsona Bela Swimming Pool           Majis Perbandaran Kwantan           Sideol Design (Track 0) Checks Cont Aku unsta Ma - Nr Hetz (Mikas minewist mette)           Maker Takk Reserve (Mikas minewist mette)           Tr         Tr           23 27 F173151.0         Bis,227           24 27 F173151.0         Bis,227           24 27 F173151.0         Bis,227           24 27 F173151.0         Bis,227           24 28 7 F173354.0         Bis,22	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jao Tito y Clash M Ster Att
2) 37 97 972314-0         PAS         HL, 2, 2         -3.34         PAS           3) 57 972314-0         PAS         HL, 2, 2         -3.34         PAS           3) 57 972314-0         PAS         HL, 2, 2         -3.34         PAS           3) 57 972314-0         PAS         HL, 2, 3         -5.36         PAS           3) 57 972314-0         PAS         HL, 2, 3         -5.36         PAS           3) 57 972314-0         PAS         HL, 2         -5.36         PAS           3) 57 972314-0         PAS         HL, 2         -5.36         PAS           3) 57 972314-0         PAS         HL, 2         5.31         PAS           3) 57 972314-0         PAS         HL, 2         5.31         PAS           3) 57 972314-0         PAS         HL, 2         5.31         PAS           3) 57 972314-0         PAS         H-L, 3         6.31         PAS           3) 57 97234-0         PAS	IF HUBLEL, REI M-L-L2, L3, 14         1.3           IF HUBLEL, REI M-L-L2, L3, L4, 10         1.3           IF HUBLEL, REI M-L3, L3, L4, 10         1.30           IF HUBLEL, REI M-L3, L3, L5, L5, L5, L4         1.30           IF HUBLEL, REI M-L3, L3, L5, L5, L5, L5, L5, L5, L5, L5, L5, L5		TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Cleat b
M ST PITRING         MAS         H-L, 2, 1 M, 457         0.348 H-L, 2, 1 M, 457         H-L, 2, 1 H-L, 2, 1 M, 457         0.348 H-L, 2, 1 M, 457         H-L, 2, 1 H-L, 2 H, 457         0.348 H-L, 2 H, 457         H-L, 2 H, 457         0.348 H-L, 2 H, 457         H-L, 2 H, 457         M-L, 2 H, 457	IF PRD14.4     PAS     M-4.4.2.1     6.2.8     17       IF PRD24.4     PAS     M-4.1.7     61     6.2.7     14       IF PRD24.4     PAS     M-4.7     61     6.2.7     14       IF PRD24.4     PAS     M-4.7.2     6.2.13     14       IF PRD24.4     PAS     M-4.7.2     6.2.14     1.3       IF PRD24.4     PAS     M-4.7.3     6.2.17     1.3       IF PRD24.4     PAS     M-4.7.3     1.3.17     1.3       IF PRD24.4     PAS <td>Wilsona Bela Swimming Pool           Majib Perbandaran Kuantan           Libed Design (Track 0) Checks Cont Nak wirz Aka - NF wirzt (Micka enkeniste entre)           Star Priziti 4, 8           21 27 Priziti 4, 9           24 arr Prizit 4, 9           24 arr Priziti 4, 9           25 arr Priziti 4, 9           25 arr Priziti 4, 9           26 arr Priziti 4, 9           27 arr Priziti 4, 9           28 arr Priziti 4, 9           29 arr Priziti 4, 9           20 arr Priziti 4, 9  <td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td><td>Cleat b</td></td>	Wilsona Bela Swimming Pool           Majib Perbandaran Kuantan           Libed Design (Track 0) Checks Cont Nak wirz Aka - NF wirzt (Micka enkeniste entre)           Star Priziti 4, 8           21 27 Priziti 4, 9           24 arr Prizit 4, 9           24 arr Priziti 4, 9           25 arr Priziti 4, 9           25 arr Priziti 4, 9           26 arr Priziti 4, 9           27 arr Priziti 4, 9           28 arr Priziti 4, 9           29 arr Priziti 4, 9           20 arr Priziti 4, 9 <td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td> <td>Cleat b</td>	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Cleat b
20         37         18<	IF PRD14.4     PASE     Mark     Mark     Mark     Mark       IF PRD214.4     PASE     Mark     Mark     Mark     Mark       IF PRD214.6     PASE     Mark     Mark     Mark	Wisma Beis Swinning Pool           Magits Pertundarun Kuantan           Leel Design (Track 0) Chacks Cont La wirzs awar in write windes winderie wirds)           Das Wirz Awar in write windes winderie wirds)           Das Tripitski, write winderie wirds)           Das Tripitski, write wirds wirds wirds, write write wirds, write wirds, write write wirds, write write wirds, write	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Add Tala y
30 EF 71722.14.6 PAGE 84-4.7 (cf) 4.713 244 13 EF 71722.14.6 PAGE 84-4.7 (cf) 4.713 4.714 24 EF 71723.14.6 PAGE 84-4.7 (cf) 4.714 4.714 25 EF 71723.14.6 PAGE 84-4.7 (cf) 4.714 4.714 25 EF 71723.14.7 PAGE 84-4.714 4.714 34 EF 71723.14.7 PAGE 84-4.714 34 EF 71723.14.7 PAGE 84-4.714 4.714 34 EF 71723.14.7 PAGE 84-4.7144 4.7144 34 EF 71723.14.7 PAGE 84-5.7144 4.7	121     PUBLIKA     PARI     No.1, 7     -0.10     -0.10       121     PUBLIKA     PARI     -0.1, 7     -0.10     -0.10       121     PUBLIKA     PARI     -0.1, 7     -0	Wisna Bela Swimming Pod           Majis Perbandaran Kuantan           Least Summing Pod	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jab Tala y Cleant k Stop ALL HOR
30 EF 71722.14.6 PAGE 84-4.7 (cf) 4.713 244 13 EF 71722.14.6 PAGE 84-4.7 (cf) 4.713 4.714 24 EF 71723.14.6 PAGE 84-4.7 (cf) 4.714 4.714 25 EF 71723.14.6 PAGE 84-4.7 (cf) 4.714 4.714 25 EF 71723.14.7 PAGE 84-4.714 4.714 34 EF 71723.14.7 PAGE 84-4.714 34 EF 71723.14.7 PAGE 84-4.714 4.714 34 EF 71723.14.7 PAGE 84-4.7144 4.7144 34 EF 71723.14.7 PAGE 84-5.7144 4.7	121     PUBLIKA     PARI     No.1, 7     -0.10     -0.10       121     PUBLIKA     PARI     -0.1, 7     -0.10     -0.10       121     PUBLIKA     PARI     -0.1, 7     -0	Wisna Bela Swimming Pod           Majis Perbandaran Kuantan           Least Summing Pod	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jab Tala y Cleant k Stop ALL HOR
11     17     <	If PDD16.6     PAR     N=1.5.2     5.05     7       If PDD16.6     PAR     N=1.5.2     5.05     1.7       If PDD16.6     PAR     N=1.5.2     5.01     1.7       If PDD16.6     PAR     N=1.5.2     5.21     1.6       If PDD16.6     PAR     N=1.5.2     5.21     1.6       If PDD16.6     PAR     N=1.5.2     1.6     1.67       If PDD16.6     PAR     N=1.5.2     1.6       If PDD16.6     PAR     1.6     1.6       If PDD16.6     PAR     1.6     1.6       If PDD16.6     PAR     1.6     1.6 <td< td=""><td>Wisna Bela Swimming Pod           Majis Perbandaran Kuantan           Least Summing Pod              Least Summing Pod</td><td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td><td>Ана Така и Стана и Ана Така и Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана</td></td<>	Wisna Bela Swimming Pod           Majis Perbandaran Kuantan           Least Summing Pod              Least Summing Pod	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Ана Така и Стана и Ана Така и Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана Ана
32         27         77<	IF PUBLIK 1     Note 1     Note 1     Note 1       IF PUBLIK 2     Note 1     Note 1     Note 1       IF PUBLIK 2     Note 1     Note 1     Note 1       IF PUBLIK 2     Note 1     Note 1     Note 1       IF PUBLIK 2     Note 1     Note 1     Note 1       IF PUBLIK 2     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note 1     Note 1     Note 1       IF PUBLIK 4     Note	Wisna Beis Swinning Pod           Majis Perbandaran Kuantan           teel Design (Track 0) Chacks Cont La wata sac - mi wrtz instas unsanta wrtzi)           assa - mi wrtz instas unsanta wrtzi rei wrtz instas unsanta wrtzi sat. 20 st printik 21 st printik 21 st printik 21 st printik 21 st printik 21 st printik 22 st printik 23 st printik 23 st printik 23 st printik 24 st printik 24 st printik 25 st printik 25 st printik 26 st printik 27 st printik 28 st printik 29 st printik 29 st printik 20 st printik	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	240 Title V Cited A
33 EF FFERENCE MALE NATE 1.1 6.254 34 EF FFERENCE MARE 1.1 6.254 35 EF FFERENCE MARE 1.1 6.254 35 EF FFERENCE MARE 1.1 6.254 35 EF FFERENCE MARE 1.1 6.254 36 EF FFERENCE MARE 1.1 6.254 36 EF FFERENCE MARE 1.1 6.254 36 EF FFERENCE MARE 1.1 6.254 37 EF FFERENCE MARE 1.1 6.254 37 EF FFERENCE MARE 1.1 6.254 37 EF FFERENCE MARE 1.1 6.254 38 EF FFERENCE MARE 1.1 6.254 39 EF FFERENCE MARE 1.1 6.254 30 EF FFERENCE MARE 1.1 6.254 39 EF FFERENCE MARE 1.1 6.254 39 EF FFERENCE MARE 1.1 6.254 31 EF FFERENCE MARE 1.1 6.	17         H70114.5.         PARI         M-4.1.5.2         519         3           17         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.1.2.2         5.216         1.4           18         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           18         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           17         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           18         H7014.6.         PARI         M-5.21         1.2         5.26           18         H7014.6.         PARI         M-5.21         1.2         5.26           18         H7014.6.         PARI	Wisena Bela Swimming Pod           Majis Perbandaran Kuantan           Los Docing Track 0) Checks Cont           Automatic senters           Materia restats embends enters           Materia restats embedde enters           Materia restats embedde enters           Materia restats enters           Materis           Ma	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
3) ET F12134.6 PAGE 44-4.2.2 5.134 3 1.57 51234.6 PAGE 1.1 6.274 5.154 5.177 5.154 5.177 5.154 5.177 5.1555 5.1555 5.155 5.155 5.1555 5.155 5.1	17         H70114.5.         PARI         M-4.1.5.2         519         3           17         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.0         1.49           18         H7014.5.         PARI         M-4.1.2.2         5.216         1.4           18         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           18         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           17         H7014.6.         PARI         M-4.1.2.2         5.26         1.4           18         H7014.6.         PARI         M-5.21         1.2         5.26           18         H7014.6.         PARI         M-5.21         1.2         5.26           18         H7014.6.         PARI	Wisena Belia Swimming Pool           Magita Perbandarun Kuentan           teol Design (Track 0) Checks Cont La with AA = NI with a without a writen bat with AA = NI with a writen and a writen at write AA = NI with a writen and a writen at write AA = NI with a writen a writen at write AA = NI write a writen at at write AA = NI write a write a st write AA = NI write a write a st write AA = NI write a write a write a st write AA = NI write a write a write a write a st write AA = NI write a write a write a write a st write AA = NI write a write a write a write a st write AA = NI write a write a write a write a st write AA = NI write a write a write a write a st write AA = NI write a write a write a write a st write AA = NI =	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
34 ST 1712134.6         PARE         AMGE 1.1         6.3H         134           35 ST 17121314.6         PARE         BA-CL, 2.2         5.266         136           36 ST 17121314.6         PARE         BA-CL, 2.2         5.266         136           36 ST 17121314.6         PARE         BA-CL, 2.7         6.268         146           37 ST 17121314.6         PARE         6.49         5.49         2.47           37 ST 17121314.6         PARE         6.49         5.49         2.47           37 ST 17121314.6         PARE         6.49         5.49         2.47           38 ST 17121314.6         PARE         6.49         5.47         144           37 ST 17121314.6         PARE         6.49         5.47         144           39 ST 17121314.6         PARE         6.49         5.47         144           39 ST 17121314.6         PARE         6.47.1         145         144           39 ST 17121314.6         PARE         6.47.1         146         6.49         6.49	IF     PUBLIKA     PAGE     AMEE     1.1     6.20       IF     PUBLIKA     PAGE     March     1.2     6.20       IF     PUBLIKA     PAGE     March     1.2     1.24       IF     PUBLIKA     PAGE     March     1.21     1.24       IF     PUBLIKA     PAGE     March     1.24     1.24       IF     PUBLIKA	Wisma Beils Swinning Pool           Magits Pertandarus Kuantan           total Design (Track 0) Checks Cont Ak Wiste Me - M HETE WINKES Embodies embodies anten base of the second seco	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
35 BT F121344.0         PM25         M=4-1,2,2         2,34         244           36 BT F121344.0         PM25         M=4-1,2,2         2,34         244           36 BT F121344.0         PM25         M=4-1,2,2         2,34         244           37 BT F122144.0         PM25         M=4-1,2         2,34         2,49           38 BT F121344.0         PM25         M=4-1,2         2,44         2,47           34 BT F121344.0         PM25         M=4-1,2         E1,532         244           39 BT F121344.0         PM24         S=4-1,7         E1,532         244           39 BT F121344.0         PM24         S=4-1,7         E1,632         245           39 BT F121344.0         PM24         S=4-1,7         E1,632         245	FT PIRING     PAGE     M-6.1.2.2     5.716     216       ST PIRING     PAGE     M-6.1.2.2     5.716     216       ST PIRING     PAGE     M-6.1.2     5.706     1.0       ST PIRING     PAGE     M-6.1.2     5.706     1.0       ST PIRING     PAGE     M-6.1.2     5.707     1.6       ST PIRING     PAGE     M-6.1.2     6.707     1.6       ST PIRING     PAGE     M-6.1.2     1.0     1.0       ST PIRING     PAGE     M-6.1.2     1.0     1.0       ST PIRING     PAGE     M-6.1.7     1.6     5.38     1.0       ST PIRING     PAGE     M-6.1.7     1.6     5.38     1.0       ST PIRING     PAGE     M-6.1.7     1.6     5.38     1.0       ST PIRING     PAGE     M-6.1.7     1.0     5.38     1.0       ST PIRING     PAGE     M-6.1.7     1.0     5.48     1.0       ST PIRING     PAGE     M-6.1.7     1.0     5.48     1.0       ST PIRING     PAGE     M-6.1.7     1.0     5.48     1.0	Wisena Beils Swinning Pool           Magin Pertundaran Kuantan           teel Design (Track 0) Chacks Cont Lk witz Andrea Michael Michael Michael Michael Beilt (Strathael Michael Michael Michael 23 Strathael Michael Michael Michael Strathael Michael Michael Strathael Michael Michael Strathael Michael Michael Strathael Michael Michael Strathael Michael Strathael Michael Strathael Michael Strathael Michael Michael Strath	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
144.01 7         -12.47         6.48         6.49           M # #7 H7101.4.6         PMB         84-7, 71         81.43         71           37 # #7121.84.6         PMB         84-7, 71         61.43         2.49           37 # #7121.84.6         PMB         84-47, 142         6.377         146           37 # #7121.84.6         PMB         84-47, 142         6.377         146           37 # #7121.84.6         PMB         84-47, 142         6.377         146           37 # #7121.84.6         PMB         84-47, 142         6.378         147           38 ## #7121.84.6         PMB         84-47, 142         6.398         148           39 ## #7121.84.6         PMB         84-47, 142         6.398         6.49	144,41 7         -41,47         6,48         6,49           57 H70136,4         145,45         1,49         1,49         1,49           17 H70136,4         146,45         -6,49         1,49         1,49           17 H70136,4         146,45         -6,49         1,49         1,49           17 H70136,4         146,45         -6,49         1,49         1,49           17 H70136,4         146,45         1,53         1,64         1,49           17 H70136,4         146,45         -1,51         1,53         1,64           17 H70136,4         146,45         -1,51         1,53         1,64           17 H70136,4         146,45         -1,51         1,53         1,64           17 H70136,4         145,45         1,64         1,64           17 H70136,4         1,645         1,64         1,64           17 H70136,4         1,745         1,645         1,64           17 H70136,4         1,945         1,64         1,64           17 H70136,4         1,945         1,64         1,64	Wisena Beils Swinning Pool           Magits Pertandarum Kuantan           Leel Dasign (Track 0) Chacks Cont Au Wirz Marka emberste entreit           La Wirz Marka emberste entreit           23 27 F/12314.0           24 37 F/12314.0           25 27 F/12314.0           26 37 F/12314.0           28 38 F/12314.0           29 38 F/12314.0           20 38 F/12314.0           21 38 F/12314.0           21 38 F/12314.0           21 38 F/12	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
37 38 11/21/44.6 Not Bit 6-1.7 EC 6.377 396 34 58 71/21/54.6 Not 55 36-1.7 EC 6.387 324 35 58 71/21/54.6 Not 55 36-1.7 EC 6.398 386 35 58 71/21/54.6 Not 55 56-1.7 EC 6.394 36-6 39 58 71/21/54.6 Not 55 56-1.7 EC 6.394 36-6.9	27         17         17         16         3.07         16           27         17         1.0         5.07         16         3.07           27         17         1.0         5.07         16         3.07           27         17.01         1.0         5.07         16         3.07           27         17.01         1.0         5.02         16         3.07           27         17.02         1.07         5.08         3.07         16         5.09           27         17.02         5.01         5.03         5.08         5.08         5.08         5.08         5.09         16         5.09         5.01	Wisma Beis Swinning Pool           Magis Perbandarun Kuentan           Leel Design (Track 0) Checks Cont Lk wirs and - mi werz windes enteurist entrest mer wirst windes enteurist entrest enteurist wirst (State Cont 2 str Pf2314.4 state State Cont 2 str Pf2314.4 str Pf2314.4 str Pf2314.4 state Cont 2 str Pf2314.4 state Cont	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	240 Tron vy Chen y AST AST AST AST AST AST AST AST
34 57 77271546.0 PASS 104-4-7 (2) 0.392 786 (2).52 - 7.29 8.49 3.07 39 57 7271546.0 PASS 104-4-7 (2) 0.394 786 14.90 8.49 0.49 0.49 0.49 0.49	17 797184.6 PAS 18-4.7 10 2-30 104 17 797184.6 PAS 18-4.7 10 2-37 45-8 2-67 17 797184.6 PAS 18-4.7 10 2-37 45-8 17 797184.6 PAS 18-4.7 10 2-37 16 17 797184.6 PAS 18-4.7 10 2-37 17 17 4.6 18 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.	Wilsona Beils Swinning Pool           Magits Perbandarum Kluentan           teol Design (Frack 0) Checks Cont Ak wirts Mac - W wirts (Makamerik): wirtsu mak wirts Mac - W wirtsu mak wirts (Makamerik): wirtsu mak wirts Mac - W wirtsu mak wirts (Makamerik): wirtsu mak wirtsu	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	340 Tion yr 150 Tion yr 160 Male 160 Ma
31 17 772154.6 PASS \$4-4-7 (2) 5.392 254 (2).35 -7.25 5.49 3.07 39 27 7727354.6 PASS 55-4-7 (2) 6.394 264 (4).49 (4).49 (5) -9.41 5.49 6.49	17 797184.6 PAS 18-4.7 10 2-30 104 17 797184.6 PAS 18-4.7 10 2-37 45-8 2-67 17 797184.6 PAS 18-4.7 10 2-37 45-8 17 797184.6 PAS 18-4.7 10 2-37 16 17 797184.6 PAS 18-4.7 10 2-37 17 17 4.6 18 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.	Wisena Breis Swinning Pool           Magits Perbandaran Kuentan           teel Design (Track 0) Checks Cont Lk wits AAR - Bit Witz (Micka endewist wits)	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
39 57 929296.0 PASS 85-4.7 [C] 0.334 284 340.89 c -9.65 0.00	57 121214.6 1945 15-4.7 162 4.234 274 57 121214.6 1945 15-4.7 162 4.234 274 57 121214.6 1945 15-4.7 162 4.233 744 57 121214.6 1945 15-4.7 162 4.338 744 57 121214.6 1945 15-4.7 162 4.348 744 57 121214.6 1945 15-4.7 162 4.348 744 5.4 144 144 144 144 144 144 144 144 144 1	Wisena Beile Swinning Pool           Magis Perbandarun Kuentan           teol Design (Track 0) Checks Cont Internet State (Control of the Stat	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
340,59 C -9,65 0.00 0.50	17 HIDHA HAN BALT, HE 6.20 266 17 HIDHA HAN HAT, HA 1, HA 1	Wisena Beis Swinning Pod           Magin Pertundaran Kuantan           teel Design (Track 0) Chacks Cont Lk witz witz witz witz witz witz witz witz	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
	я ланы мал на	Wisena Beis Swinning Pod           Magis Perbandaran Kuantan           teel Design (Frack 0) Checks Cont La wirzs and the sentence entrait           23 st Pirilat.4           13 st Pirilat.4           24 st Pirilat.4           25 st Pirilat.4           25 st Pirilat.4           26 st Pirilat.4           26 st Pirilat.4           26 st Pirilat.4           27 st Pirilat.4           28 st Pirilat.4           29 st Pirilat.4           20 st Pirilat.4           20 st Pirilat.4           20 st Pirilat.4           21 st Pirilat.4           22 st Pirilat.4           23 st Pirilat.4           24 st Pirilat.4           25 st Pirilat.4           26 st Pirilat.4           27 st Pirilat.4           28 st Pirilat.4           29 st Pirilat.4           20 st Pirilat.4           21 st Pirilat.4           22 st Pirilat.4	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
40 ST P1P2136.0 PAGS 85-4.7 (C) 0.328 266 256.96 C -7.82 8.60 8.00	ST F1P2196.0 FAGS 85-4.7 (C) 0.283 201 315.86 C -3.85 0.00 0.00	Wisena Bris Swinning Pod           Magis Perbandaran Kuantan           teel Design (Track 0) Checks Cont La wirs and the sentence wirst rest of the sentence wirst rest of the sentence rest of the sentence rest of the	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
41 3T F1F2194.0 FASS 85-4.7 (C) 0.365 286 331.87 C -4.58 0.40 0.00	ST F1P2196.0 FAGS 85-4.7 (C) 0.283 201 315.86 C -3.85 0.00 0.00	Wisena Bris Swinning Pod           Magis Perbandaran Kuantan           teel Design (Track 0) Checks Cont La wirs and the sentence wire; Data Track 0) Checks and the sentence wire; Data Track 0, 100 (100 (100 (100 (100 (100 (100 (1	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
		Wilsona Beild Surieming Pool           Magib Perbandarum Kuentan           La wirsz Adal - ali wirsz enkosta enkonta entrepi temesi enkosta enkonta	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	Jao Tito y Clash M Ster Att
	ST F1F2196.0 FASS ANNUE T.1 0.391 206	Wisma Beis Swinning Pool           Magis Perbandaram Kuantan           teel Design (Track 0) Checks Cont La wirs and a set wirs indust enternit enterin entering the set of the	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
43 st p1p2154.0 pASS ANNEX 1.1 0.255 256		Wisena Beis Swinning Pod           Magis Perbandaran Kuantan           teel Design (Frack 0) Checks Cont La wirzs and the sentence wrest extension of the sentence with the sentence with the sentence extension of the sentence with the sentence wit	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
(J 57 7)72354.6 9945 AMSE [1,] 0.391 744 234.55 € -45.56 15.58 -	228.26 C -4.59 11.59 - 	Wisena Beis Swinning Pod           Magin Pertundaran Kuantan           teel Design (Track 0) Chacks Cont Lk witz witz (Missa embandis enter)           Data Status Pertundaran Kuantan           ta witz witz (Missa embandis enter)           Data Status Pertundaran Kuantan           ta witz (Missa embandis enter)           Data Status Pertundaran Kuantan           ta witz (Missa embandis enter)           ta witz (Missa embandis enter)           ta status Pertundaran Kuantan	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
43 ST 7171354.0 PA35 ANGER 1.1 6.391 294 51.41 C 4.43 11.61 0 -	238.26 C -4.50 18.50 -	Wisma Baria Swimming Pool           Majis Perbandaran Kuantan           eel Design (Track 0) Checks Cont Laura Autor Michael Internet Interne	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	
43 27 7 171254 - PASS - SMEE 1.3 6.393 - 746 23.27 7 17254 - 0.53 - 0.53 - 15.58 44 58 7 17254 - 0.54	21.3 f c -4.36 11.50 - 57 9192364.6 PASS 58-4.7 (C) 6.377 281 30.6 c -3.46 6 -4.6	Wissna Bels Swinning Pod           Magis Perbandaran Kuantan           Seel Dasign (Track 0) Chacks Cont La wats de - M. Hitte (Notest ententie Notest Part (1993)         La wats de - M. Hitte (Notest ententie Notest Part (1993)           Status Name         Restrict (Status ententie Notest Part (1993)         Restrict (Status ententie Notest Part (1993)         La wats de - M. Hitte (Notest ententie Notest Part (1993)         La wats de - M. Hitte (Notest ententie Notest Part (1993)         La wats de - M. Hitte (Notest ententie Notest Part (1993)         La wats de - M. Hitte (Notest ententie Notest Part (1993)         La wats de - M. Hitte (1993) <th< td=""><td>TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM</td><td></td></th<>	TPL40581         a 100         R4b-FAB2           Parlwind speed 32.5 m/s         Ref Fabric R5           By TSM         Dalit17.Dec-11         Del TSM	

 ${\mathcal B}$ 

			Jab No TPL40581	Sheet No	a 101	Rev R4b-FAB
5						
Title Wisma Belia Swimming Pool			Partwind speed 32 Raf Fabric R5	.5 m/s		-
wisma Belia Swimming Pool			By TSM	Dale 17-D		TSM
	1					
Majlis Perbandaran Kuantan			File Q326-KSP-R4	b-Deg.std	Date/Time 10-J	Jul-2012 15:43
Steel Dealer (Teach 0) Charles Co						
Steel Design (Track 0) Checks Co ALL WITS ARE - KN HETE (UNLESS OTHERWISE						
HENRER TABLE RESULT/ CRITICAL		LOADING/				
гх нт	H2	LOCATION				
45 ST P2P2196.0 PASS 85-4.7	(C) 0.300	265				
	0.00	0.00				
46 57 P1P2196.0 PAIS 85-4.7 349.99 C -5.7	(C) 0.321 0.00	205				
***************************************						
370.84 C -4.1	IC) 0.340 IS 0.00	205				
48 ST P1P2196.0 P353 85-4.7	IC) 0.356	205				
48 ST P1P2196.0 PASS 85-4.7 387.72 C -5.1	17 0.00	8.00				
45 57 9192196.0 PASS 85-4.8.2. 298.17 7 -24.4	2 0.590	204				
	0.00	1.78				
30 ST PIP2196.0 PASS 85-4.8.2 280.19 T -25.7	2 0.596	204				
51 ST PIP2196.0 PASS 85-4.8.2. 274.25 T -6.5	2 0.336	204				
52 57 P1P2196.0 PASS 85-4.8.2.	2 0.288	204				
	6 0.00	1.78				
53 ST PIPEIS6.0 PASS \$5-4.8.2.	2 0.320	204				
217.02 7 -9.2	3 0.00					
54 57 P1P2154.0 PASS 85-4.8.2. 100.10 T -14.7	2 0.360	204				
55 ST PIP2196.0 PASS 85-4.8.2. 251.60 T -3.5	2 0.281					
56 57 P1P2196.0 PA35 85-4.8.2. 267.41 7 -3.3	2 0.287	205				
267.41 7 -3.3	9 0.00	1.78				
57 ST PIP2196.0 PASS 85-4.8.2. 315.40 T -17.0	2 0.331	201				
	1 0.00	1.70				
54 ST PIP2196.0 PASS 85-4.8.2. 128.50 T -16.8	2 0.333	201				
59 57 P1P2194.0 PASS 85-4.8.2. 274.21 7 -3.5	2 0.235 2 0.00	206				
40 57 PIP2194.0 PASS 85-4.8.2. 242.93 T -4.0		206				
242.93 T -4.0	2 6.00	0.00				
41 5T P1P2196.0 PASS 85-4.8.2. 206.26 T -11.6	2 0.342	205				
		1.78				
42 ST PIP2196.0 PASS 85-4.8.2. 248.85 T -6.2	2 0.308	205				
43 ST PIP2196.0 PASS 85-4.8.2. 281.48 7 -5.2		205				
44 ST P1P2196.0 PASS 85-4.8.2.		205				
44 ST P1P2196.0 PASS 85-4.8.2. 293.32 T -5.4	5 0.00	0.00				
65 ST PIP2194.0 PASS 85-4.8.2.	2 0.594	205				
211.05 7 -24.9	6 8.00	1.78				
66 57 P1P2196.0 PASS 85-4.8.2. 200.92 T -25.2	0.598	205				
200.92 7 -25.2	£ 0.00	0.00			×	
Time/Dele: 11/07/2012 17:28	STAAD Dra	for Windows 20.0	7 02 16			Print Run 3 of 10

STAAD Bra for Windows 20 07 02 1

 ${\mathcal B}$ 

Rev R4b-FAB2

TPL40581

Prizonial Vertical Momen FY FZ MX MY DNI (DNI (DNm) (DNm)

a 97

 P#stylid speed 32,5 m/s

 P#f spind speed 32,5 m/s

 P#f spind speed 32,5 m/s

 P/f TSM

 P/ TSM

 P/r Sold Sectors

 P/r Co25-KSP-R4b-Dog.old

 Distributes

 Distributes

Rav R4b-FAB2

......

TPL40581 Sheet No a 96

-	6						L	TPL40581		a 98	
-	Soltwar	e licensed to Tr	anserve Pile Lid	6			1	Parlwind speed 3	2.5 m/s		
ob Tile W	isma Be	ila Swimmin	g Pool				1	Ref Fabric R5			
						and server		BY TSM	Dale17-D	lec-11 Chi	TSM
Dieni Majiis Perbandaran Kuanlan						5	* Q326-KSP-R	4b-Deg.std	Date/Time 10-	ul-2012 16:4	
Rea	ction S	Summary		orizonial			ement				
-	No	e UC	FX	FY	Vertical FZ	MX	MY	a			
Max	FX 80	0 208:1.2(5	(LN)	[LN] 63 97.854	(LM) -23,855			um) 2.129			
Min I	FX 78	2 206:1.2(5	W+D -232.5	86 97.637	-23.505	-106.971	40.596 2	0.386			
Max I				87 228.469 16 -228.757		-773.536		3.081			
Max				16 -228.757		245.624		1.534			
Min I		S 12LOAD	CASI 39.0	75 155.698	-378.413	-108.569		0.702			
Max P				62 -110.379 87 228.469				1.775			
Max		2 208:1.2(5	W+D 228.3	07 -97.765	13,925	171.825 2	78.833 2	2.013			
Min A		4 206:1.2(5	W+D -228.8	4 -17.713		171,582 -2		9.767			
Max P							27.835 12	4.287			
Read	ction E	Hartze		enical	Mome.	nt .	I	-			
NCCO	Env	(LN)	DND	(AN)	(aNm)	(kNm)	(Nm)				
776	+10	5.549					122,951				
775	14	Losd: 207	Losd: 202	-375.413	Load: 204	Less: 201	Load: 205	-			
776		Lose: 206		Lord: 12	Losd: 205	-	Load: 207	-			
778	110	10.238	153.732	351.121			43,821	1			
778	**	Losd: 207		Load: 201 -375,208	Load: 204	Load: 201	Laad: 207	-			
778		Load: 206	Losd: 202	Load: 12	Losd: 205		Lord: 205	1			
782	***	0.336	132.279 Losd: 202				25.715	1			
782	100	Losd: 2	-173.162		Losd: 204	Load: 11 -60.596	Load: 208	4			
782		Losd: 206	Loed: 201	Load: 5		Load: 205	Losd: 207	1			
784	*ve	0.393	173,478	535.367 Load: 201	493.687	0.356	31.651	-			
784		-228.844					-25.106	1			
784	-18	Losd: 205	Load: 202	Losd: 5	Losd: 205	Load: 205	Load: 209	1			
788	110	0.065		568.764 Losd: 201			27,141 Lead: 209	4			
788	-10	-55.216	-228.757	-265.682	-453.533	-23.013	-29.545	1			
788		Load: 206		Load: 8	Load: 205	Load: 205	Load: 207 30.581				
790	-18	0.121	Load: 201		Losd: 8	0.302 Load: 2	10.541	1			
790	-10	-30.532	-132.653	-275.450	-773.535	-08.380	-26.562	1			
750		Load: 206	Load: 12 137.535	Losd: 12 471.322		Load: 208	Load: 209 28,231	-			
794	*18	54.593 Load: 208		4/1.322 Load: 201		24,324 Load: 208	28.231 Load: 209	1			
754	-18	-0,118		-289.686	-474.062	-12.662	-28,482	1			
794	-10	Losd: 2 30.164		Lead: 6 450,721		Losd: 209 87.234	Losd: 207 27.730	1			
796	***	Losd: 208	Load: 201	Losd: 201	Losd: 8	Load; 208	Losd: 207	1			
795	-10	-0.164						1			
795	-10	Losd: 2 232,063			Losd: 201 525,987	Load: 2 62.379	Losd: 209 29.508	1			
800	**8	Losd: 208	Losd: 202	Load: 201	Load: 204	Load: 208	Load: 209	1			
800	-18	-0.281	-173.132 Lost: 201				-27.039	4			
602		228.307	173.377	534,933	493.232	278.833	26,763	1			
802	-16	Lead: 208		Load: 201	Load: 204	Load: 208	Load: 207	1			
802	-12	-0.299	-132,455 Load: 202	-203.318 Losd: 5	-527.734 Lesd: 205	-0.294	-29.996 Losd: 209	-			
802		63.709	160.512	340,493	495.806	0.000	41.828	1			
805	140			Load: 201		•	Load: 209	1			
606	-18	-5.133 Losd: 209		-378.822 Losd: 10	-388.010 Load: 205	-35,386 Lead: 201	-124.972 Lead: 208	1			
805	++0	63.227	194,001		383.222	0.000	124,287	1			
808	410			Losd: 201	Land: 204		Load: 208	1			
		-9.634	-160.560	374.646	-497,308	-35.024	-42.019				
806			Load: 202		Load: 205	Last 201	Lead: 209	1			

2					Job No TPL40581	Sheet No	a 102	Rev R4b-FAB
Software licens	ed to Transarva I	Ta Lid			Partwind speed	32.5 m/s		
the Wisma Bella Sw	imming Pool				Ref Fabric R5			
					BY TSM	Dale17-D		
ent Majlis Perbanda	ran Kuantan				F# Q326-KSP-	R4b-Deg.std	Date/Time 10-Jul-	2012 16:43
Steel Design (								
HENDER TABLE		CRITICAL COND/	NATIO/	LOADING/				
67 57 P1P2190	412.12 C	85-4.7 (C) -7.14	0.378	204				
64 ST P1P2196	.0 FASS	85-4.7 (C) -5.09	0.350	204				
69 ST P1P2196			0.333	204			1	
76 57 9192196			0.307	204				
			0.00	1.78				
71 57 9192196		85-4.7 (C) -3,32	0.00	1.78				
72 57 9192196	235.99 C	ANNEX 1.1 -8.85	0.400	206				
73 ST #1#2196	.0 PASS 309.67 C	85-4.7 (C) -3.55	0.384 0.00	201				
74 ST PIP2196		85-4.7 (C) -6.29	0.303	206				
75 ST PIP2196	.0 PASS	85-4.7 (C) -7.67	0.328	296				
76 57 9392196		#5-4.7 (C) -9.59	0.332	206				
	359.10 C		0.00	2.07				
77 ST P1P2196			0.00	0.00				
78 ST P1P2196	0 PASS 220.61 C	85-4.7 (C) -3.55	0.204	201 0.00				
75 57 9192196		85-4.7 (C) -0.85	0.176	201 0.00				
10 ST P102196	0 PASS 203.57 C		0.187	201 0.00				
#1 57 P1P2196	0 PASS 264.81 C	85-4.7 (C) -3.19	0.243	201 0.00				
#2 ST #1#2196	0 PASS	85-4-7 (C)	0.222	205				
	241.76 C	-1.75	0.00	205				
83 ST 9392196			0.00	0.00				
BC 57 P1P2196		83-4.7 (C) -2.83	0.315	205				
45 ST P1P2196	0 PASS 377.14 C	85-4.7 (C) -3.93	0.346	205				
86 ST P1P2196	0 PASS 330.21 T	85-4.8.2.2 -6.06	0.375	204				
47 ST PIP2196	0 PASS	15-4.9.2.2 -5.96	0.401 0.00	204				
HL 57 P1P2196	• PASS	85-4.1.2.2	0.394	284				
	346.54 T	-6.02	0.00	0.00				
Time/Dele: 11/07/2012 17:	9		TAAD.Pro f	or Windows 20	.07.02.15			Print Run 4 of 10

STAAD.Pro for Windows 20.07.02.15



2	Job No TPL40581	Sheel No a 99	Rev R4b-FAB
Software Reensed to Transerve Pie Ltd	Partwind speed 32.	5 m/s	
Wisma Bella Swimming Pool	Ref Fabric R5		
	By TSM	Dale17-Dec-11	Chd TSM
Majlis Perbandaran Kuantan	Fte Q326-KSP-R4	b-Deg.std Date/Time	10-Jul-2012 16:43

ALL UNITS	ARE - KR	HETE (UNLE	SS OTHERWISE NOTED!		
HEHBER	TABLE	RESULT/	CRITICAL COND/	NATIO/	LGADING LOCATIO
1 1	T P1P2196.0	7355 415.44 C	85-4.7 (C) -7.43	0.00	206
					206
2 5	T_PIP2196.0	103.14 C	85-4.7 (C) -3.38	0.373	0.0
3 5	T PIP2196.0	PASS 250.08 C	35-4.7 (C) -3.14	0.231	206
		7555		0.263	204
• 5	T P1P2396.0	104.68 T	83-4.4.2.2 -12.65	0.00	1.7
				0.314	216
22	T PIP2196.0	71.77 C	ANNEX 1.1 -1.33	20.36	
4 5	T FIF2196.0	PASS 168.10 T	85-4.8.2.2 -5.80	0.229	0.0
		1745	85-4.4.2.2	0.748	
7 5	T P1P2196.0	187.75 T	-5.87	0.00	0.0
				0.257	
15	F P1P2196.0	7855 201.74 T	85-4.8.2.2 -5.59	0.00	1.7
		PASS	85-4.7 (C)	0.300	205
12	FIF1194.0	326.64 C	-2.37	0.00	0.0
	P1P2196.9	PASS	85-4.7 (C)	0.342	205
10 5	F P1P2196.0	372.03 C	-2.40	0.00	0.0
			85-4.7 (C)	0.380	205
11 5	F P1P2196.0	7355 414.78 C	-3.40	0.00	0.0
	P1P2196.0	PASS	85-4.6.2.2	0.371	204
12 3	F P1P2196.0	142.45 T	-10.20	0.00	0.0
	F1P2196.0	PASS	81-4.6.2.2	0.292	204
33.5	1 111110.0	176.00 T	-9.95	0.00	1.7
	PIP2196.0	PA15	85-4.8.1.2	0.284	204
		204.48 T	-7.43	0.00	0.0
	P1P2196.0	7455	85-4.0.2.2	0.292	204
		225.21 T	-4.65	0,00	1.7
	P122195.0	PASS	85-4.8.2.2	0.357	204
		210.11 T	-12.54	0.00	0.0
	F1P2196.0	PASS	85-4.8.2.2	0.286	
		215.50 T	-6.86	0.00	1.7
	PIP2196.0	PASS	85-4.4.2.2	0.303	209
		220,73 T	-7.77	0.00	0.0
	P1P2196.0	PASS	85-4.8.2.2	P.380	205
19 51	P1P2196.0	214.49 T	-13.96	0,00	1.7
	P1P2196.0	73.55	85-4.4.2.7	0.378	209
20 51	F174136.0	212.31 T	-13.94	0.00	0.01
	P1P2196.0	PA35	85-4.8.2.2	0.300	209
11 51		217.75 7	-7.72	0.00	1.76
	P1P2196.0	PASS	85-4.8.2.2	0.284	209
11 51	Faralse	211.74 1	-6.94	0,00	0.61

Print Time/Dal

STAAD.Pro for Windows 20.07.02.15

Print Run 1 of 10

2	Job No TPL40581	Sheet No a	103	Rev R4b-FAB
Software Roensed to Transarve Pie Ltd	Partwind speed 32.	5 m/s		
Job Title Wisma Bella Swimming Pool	Ref Fabric R5			
	By TSM	Dele17-Dec	-11 Chd 7	ISM
Client Majlis Perbandaran Kuantan	File Q325-KSP-R4t	Deg.sid	Deterime 10-Jul	-2012 16:43

ALL UNITS	ARE - INI	HETE INHLE	SS OTHERNISE HOTED	•	
HEHBER	TABLE	NESULT/	CASTICAL COND/	RATIO/	LOCATION
	*********			**********	

89 ST 9192196.0	PASS 395.47 C	85-4.7 (C) -5.24	0.363	205
56 ST P1P2156.0	PASS 347.54 C	85-4.7 (C) -4.32	0.337	205
91 ST PIP2196.0	PASS 329.07 C	83-4.7 (C) -4.05	6.302	205
52 57 P1P2196.0	PASS 200.05 C	85-4.7 (C) -3.64	0.258 0.00	205
93 57 P1P2196.0	PASS	85-4.7 (C) -3.68	0.205	205
94 ST #1#2196.8	223.63 C	85-4.7 (C)	0.154	206
85 ST F1F2186.0	169.26 C	-1.81	0.00	0.00
	173.86 C	-1.56	0.00	0.00
36 ST PIP2196.0	PASS 170.68 C	85-4.7 (C) -1.42	0.157 0.00	1.78
97 ST PIP2196.0	PASS 158.70 C	#5-4.7 (C) -1.67	0.146 0.00	206
58 ST 9192196.0	PASS 192.97 C	85-4.7 (C) -2.46	0.177 0.00	204
99 ST PIP2196.0	PASS 248.64 C	85-4.7 (C) -3.42	0.228	204
100 ST PIP2196.0	PASS 251.32 T	85-4.8.2.2 -4.74	0.190 0.00	205
101 ST PIP2196.0	PASS 296-13 T	85-4.8.2.2 -6.53	0.356	205
102 ST P192196.0	PA55 316.44 C	85-4.7 (C) +5.05	0.354	204
103 ST 9192196.0	PASS 421.03 C	85-4.7 (C) -4.54	0.306	204
104 ST P1P2196.0	PASS	AS-4.7 (C) -5.86	0.410	204
105 ST P1P2196.0	PASS 434.11 C	83-4.7 (C) +3.91	0.398	204
106 ST 9192196.0	PASS 109.77 C	85-4.7 (C) -4.82	0.375	204
107 ST P1P2196.0	PA55 370.52 C	85-4.7 (C) -3.18	0.340 0.00	204
108 ST P1P2196.0	PASS 320.54 C	#5-4.7 (C) -2.52	0.294	204
105 ST P1P2196.0	PASS 262.61 C	85-4.7 (C) -1.53	0.241	201
110 ST #1#2196.0	PASS 274.25 C	85-4.7 (C) -2.87	0.252	201
	4/4.25 C	-2.67	4.00	1.78

Print Time/Date: 11/07/2012 17:2

STAAD.Pro for Windows 20.07.02.15

Print Run 5 of 10



$ \ge $						TPL40581	a 105	Rev R4b-FAB
2	amfrand	to Transerve P	-114			Parlwind speed 32.5	m/s	
nde Wisma f						Ref Fabric R5		
						BY TSM	Date 17-Dec-11 Che	TSM
Majiis Pr	rbandara	Kuantan				Fie Q326-KSP-R4b		
			hecks Cont					
	TABLE		CRITICAL COND/	AATIO/	LOADING/			
			нт	HI	LOCATION			
133 57	P1P2196.0	PASS	85-4.7 (C)	0.153	205			
		164.85 C	-1.80					
		7355 161.42 C	85-4.7 (C) -1.67	0.148	205			
135 ST	PIP2196.0	PASS 150.83 C	85-4.7 (C) -1.54	0.138	200			
			-1.54	8.00	1.78			
136 ST	PIP2196.0	PASS 173,46 C	85-4.7 (C) -2.39	0.159	204			
	P1P2134.0		85-4.7 (C) -3,16	0.210	204			
128 57	P122186.0	PASS 225.72 T	15-4.4.2.2	0.243	205			
		225.72 T	-4.45	0.00	1.49			
139 57	P1P2196.0	PA55 260.47 T	35-4.3.2.2	0.319	205			
•••••					****			
140 ST	PIP2196.0	PASS 366.36 C	85-4.7 (C) -4.95	0.337	204			
				0.397	205			
			85-4.4.2.2 -10.25	0.00	1.78			
142 57	*192196.0	PASS 429.41 C	85-4.7 (C) -5.84	0.394	204			
				0.00				
143 57	P1P2196.0	7A55 419.07 C	85-4.7 (C) -3.42	0.384	1.78			
		PASE	85-4.7 (C)	0,364	204			
		396.57 C	85-4.7 (C) -3.90	0.00	1.74			
145 ST 1	P1P2196.0	PASS 361.34 C	85-4.7 (C) -3.10	0.331	204			
	192196.0		85-4.7 (C) -2.48	0.208	204			
			85-4.7 (C)	0.240	201			
	192196.0	261.83 C	-1.52	0.00	1.78			
140 ST 1	192196.0	PASS	85-4.7 (C) -2.45	0.250	201			
		272.63 C		0.00	1.74			
	192196.0	PASS 195.69 C	85-4.7 (C) -1.40	0.100	201			
	192196.0	PASS	85-4.1 (C)	0.173	201			
		187.37 C	-0.78	0.00	2.07			
151 ST #	192196.6	PASS	85-4.7 (C)	0.133	201			
••••••		214.67 6	-3, 68	0.00	2.07			
	1P2156.0	PASS 218.05 C	85-4.7 (C) -0.21	0.202	201 2.07			
	192196.0	PASS	85-4.7 (C)	0.293	201			
	192196.0	316.94 C	85-4.7 (C) -0.31	0.293	0.00			
	192196.0	PASS	85-4.7 (C) -5,68	0.249	201			
		312.38 C	-5.68	8,00	0.00			

TPL40581				2
Parl wind speed 32.5		ie Lid	censed to Transarve P	Solwara license
Ref Fabric R5				Job Tide Wisma Bella Swi
BY TSM		1.4.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		
File Q326-KSP-R4b-			ndaran Kuantan	Client Majüs Perbandar
BY TSM	1 130 130 130 130 130 130 130 130 130 13	H PREMILE RETE           CHITCAL CONF           H-1-1           H-1	daran Kuantan 1 (Track 0) Cl 30 Here (100) 2 A parter (100) 2 A parter (100) 3	CENI Magip Perbandar Steel Dasign (1) Nala bitta XA - so Nala bitta XA - so Nala bitta XA - so 155 57 7172134. 155 57 7172134. 165 57 7172134. 175 57 7
		Million 2014 1012	Ancks Cont           16 OREMULE RETER           16 -1, 161           1, 161      <	an Kuantan Track O Dichocks Cont MERT: 04456 OREMULE HUTEN MERT: 04456 OREMULE HUTEN ACENT, 04156 OREMULE HUTEN 0 17425 04-13, 100 0-323 0 17425 04-13, 100 0-325 0 17455 04-13, 100 0-355 0 17455 04-14, 100 0-355 0 17455 04-14, 100 0-355 0 17455 04-14, 100 0-355 0

2					TPL40581	sheel No a 108	Rav R4b-FAE
Software license	d to Transerve A	Tie Lid			Partwind speed 32.5	5 m/s	
Tile Wisma Belia Swi	mming Pool				Rel Fabric R5		
					BY TSM		TSM
Majils Perbandan	an Kuantan				File Q326-KSP-R4b	-Deg.std Detertime 10-J	lul-2012 16:43
Steel Design (7							
HEHRER TABLE	AESULT/	CAITICAL COND/	EATIO/	LOADING/			
	rx	ЯТ	H2	LOCATION			
199 ST P3P2196.	0 PASS 315.97 C	85-4.7 (C) -4.07	0.363	205			
200 ST P1P2196.		85-4.7 (C)	0.385	205			
			0.405				
201 57 9192194.	441.95 C	85-4.7 (C) -6.72	0.00	6.00			
202 ST 9392196.	426.41 C	85-4.7 (C) -4.76	0.331	205 0.00			
203 ST PIP2196.			0.369	205			
204 57 9392196.			0.336	205			
	344.30 C	-4.29	0.00	0.00			
205 ST PIP2136.	119.66 C	85-4.7 (C) -3.97	0.293	205			
206 ST PIP2136.		85-4.7 (C)	0.243	205			
		-3.30	0.00				
287 57 9192196.		15-4.4.2.2 -4.46	0.203	204			
208 ST P3P2196.0	PASS 124.78 T	85-4.8.2.2 -2.63	0.150 0.00	201			
205 ST #172156.		85-4.8.2.2 -4.35	8.174	201			
	128.64 7						
210 ST P2P2156.0		85-4.8.2.2 -4.57	0.173	201 0.00			
211 ST P1P2194.0	PASS 150,35 C	#5-4.7 (C) -1.75	0.138	12 0.00			
712 ST P192156.0		85-4.8.2.2	0.154	205			
		-2.55	0.00	1.78			
		85-4.4.2.2 -3.21	0.212	205			
214 ST 9192196.0	PASS 231.23 T	85-4.8.2.2	0.294	205			
215 57 9192194.0		\$5-4.8.2.2	0.351	205			
		-7.99	0.00	1.44			
216 57 9192196.0	PASS 374.34 C	85-4.7 (C) -4.81	0.343	204			
217 ST 9192196.0	PASS		0.385	204			
			0.418	204			
218 ST PIP2196.0	455.28 C	-4.13	0.00	1.78			
219 57 9392196.0	PASS 443.52 C	85-4.7 (C) -3.52	0.457	204 1.78			
220 ST P1P2196.0			0.385	204			
	424.01 C	-4.17	0.00	1.78			

2			TPL40581	Sheel No	a 109	Rev R4b-FAB
Sphware licensed in Transerve Pie Lid			Parlwind speed 32.	5 m/s		-
to Trile Wisma Belia Swimming Pool			Ref Fabric R5	5 1123		
-			By TSM	Dale17-D	ec-11 Chd	TSM
Int Majlis Perbandaran Kuantan			F# Q326-KSP-R4			
Steel Design (Track 0) Checks Cont						
	MT10/	LOADING/				
221 ST FIF2194.0 FASS 85-4.7 (C) 381.89 C -3.33	0.360	204			*	
347.27 C -2.73	0.319	204				
343.86 C -2.89	0.315	201				
224 ST F1F2196.0 PASS 85-4.7 (C)	0.325	201				
225 ST #1#21#4,0 #A55 85-4,7 (C)	0.228	201				
	0.222	203				
239.86 C -1.03	0.00	2.07				
	0.256	201 2.07				
	0.260	201 2.07				
229 57 P1P2194.0 PASS 85-4.7 [C] 256.47 C -0.27	0.237	201				
230 57 7572396.0 7855 85-4.7 (C)	0.234	201				
	0.00	201				
197.46 C -0.90	6.00	0.00				
- 207.33 C -2.14	0.150	101 0.00				
233 ST PIP2196.0 PASS 85-4.7 (C) 242.14 C -2.79	0.222	201				
234 ST PIP2194.0 PASS 85-4.7 (C) 231.29 C -1.70	0.212	205				
235 ST P1P2194.0 PASS 85-4.7 (C)	0.245	205				
	0.00	0.00				
234 31 7172394,0 7A23 8344,7 (C) 335.64 C -2.71	0.00	0.00				
369.89 C -3.82	0.00	205				
238 57 F1F2196.0 FASS BS-4.7 (C) 395.38 C -4.31	0.363	205 0.00				
239 57 PIP2196.0 PASS 85-4.8.2.2 326.02 T -8.46	0.408	204				
	0.405	204				
241 ST P1P2196.0 PAGS 85-4.7 (C)	0.357	205				
	0.00	0.00				
242 ST PJP2194.0 PASS 85-4.7 (C) 363.24 C -4.26	0.00	0.00				

TAN SIEW MOI

P	TPL40581	Sheet No a 110	Rev R4b-FA
Solware licensed in Transeve Pie Ltd	Partwind speed 32.5	mle	
teb Tile Wisma Bella Swimming Pool	Ref Fabric R5	o nva	
	BY TSM	Dele17-Dec-11	Child TSM
Majlis Perbandaran Kuantan			* 10-Jul-2012 16:43
		o contro	10 0012012 10.40
Steel Design (Track 0) Checks Cont			
ALL UNITS ARE - KH " HETE (UNLESS OTHERWISE HOTED)			
HORSER TABLE RESULT/ CRITICAL COND/ NATIO/ LOADING/			
TX HT HE LOCATION			
243 57 P1P2196.0 PASS 85-4.7 (C) 0.296 205 322.43 C -3.98 0.00 0.00			
*******			
244 5T P1P2196.0 PASS 85-4.7 (C) 0.251 205 273.82 C -3.52 0.00 8.00			
245 57 P3P2196.0 PAS5 85-4.7 (C) 0.196 265 216.20 C -2.54 0.00 0.00			
246 ST P1P2196.0 PASS BS-4.7 (C) 0.151 206			
145.04 C -1.75 0.00 0.00			
242 ST 0102186 A 0855 06-4 2 101 A 162 104			
147.03 C -1.77 0.00 0.00			
248 ST P192196.0 PASS 85-4.7 (C) 0.148 206			
141.73 C -1.59 0.00 1.78			
245 ST P1P2196.0 PASS 85-4.7 IC1 0.137 205 149.27 C -1.53 5.00 1.78			
250 ST P1F2196.0 FASS B5-4.7 (C) 0.159 204 172.92 C -2.40 0.00 1.78			
251 ST P1P2196.0 PASS 85-4.7 (C) 0.210 204 225.09 C -3.17 0.00 1.78			
252 57 P3P2196.0 PASS 85-4.4.2.2 0.267 205			
228.91 7 -4.49 0.00 1.49			
253 ST P1P2196.0 PASS 85-4.0.2.2 0.326 205			
254 ST P1F2194.0 PASS B5-4.7 (C1 0.338 204 359.63 C -4.53 0.00 1.78			
349.43 C -4.33 0.60 1.78			
235 5T 9392196.0 PASS 85-6.8.2.2 0.381 205 300.10 T -0.19 0.00 1.78			
256 57 F3F2196.0 FA55 85-4.7 (C) 0.396 204 432.18 C -5.79 0.00 1.78			
257 ST PIP2196.0 PASS 85-4.7 ICI 0.287 204 421.45 C -3.82 8.68 1.78			
254 ST PIP2194.0 PASS B5-4.7 (C) 0.365 264 294.29 C -3.52 0.68 1.78			
255 ST #1#2196.0 #885 85-6.7 (7) 0.333 264			
342.54 c -3.12 0.00 1.70			
260 ST 9192196.0 9455 85-4.7 (C) 0.289 204			
315.00 C -2.49 0.00 1.76			
261 ST P1P2196.0 PASS 85-4.7 (C) 0.253 201 276.30 C -1.62 0.00 1.78			
242 57 P1P2194.0 PASS 85-4.7 (C) 0.242 201 245.18 C -2.45 0.60 1.78			
243 ST P172196.0 PASS 85-4.7 ICI 0.185 201 201.99 C -1.20 0.00 1.78			
264 57 P1P2196.0 PASS 85-4.7 (C) 0.179 201 193.22 C -0.67 0.00 2.07			

8 Solvey a Kanasa la Tansan Pa Lis	Job No TPL40581	Sheel No	a 107	Rev R4b-FAB
	Panwind speed 32.5 m/s			
Jeb Tile WIsma Beila Swimming Pool	Ref Fabric R5			
	BY TSM	Dale17-D	ec-11 Cha	TSM
Client Majilis Perbandaran Kuanlan	FI4 Q326-KSP-R4	-Deg.std	Date/Time 10-J	ul-2012 16:43

# Steel Design (Track 0) Checks Cont.

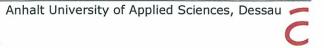
			hecks Cont		
	ARE - IOI		SS OTHERWISE NOTED		
Sta	TABLE	NESULT/	CAITICAL COND/	HATIO/	LOADING/
	PIP2196.0	PASS		0.359	205
177 51	P1P2196.0	279.14 T	85-4.8.2.2 -7.95	0.00	1.04
178 57	P1P2196.0	PASS	85-4.7 (C)	0.347	204
		378.73 C	-4.54	0.00	1.78
179 57	PIP2196.0	73.55 423.46 C	85-4.7 (C) -5.34	0.388	204
160 57	P3P2196.0	PASS 459.19 C	85-4.7 (C) -6.15	0.421 0.00	204
101 57	P122196.0	7A55 447.12 C	85-4.7 (C) -3.55	0.410	204
	P172196.0	PASS	85-4.7 (C)	0.197	204
		427.24 C	-4.20	0.00	1.78
183 57	PIP2196.0	PASS	85-4.7 (C)	0.362	204
		394.84 C	-3.35	0.00	1.78
184 57	PIP2196.0	PASS	85-4.7 (C)	0.321	204
		349.74 C	-2.75	9.00	1.70
185 ST	P1P2196.0	PASS 345.97 C	85-4.7 (C) -2.31	0.317	203
		345.57 L	-7.11		
186 ST	P1P2196.0	PASS 356.64 C	85-4.7 (C) -3.53	0.327	201
			-9.19		
167 57	P1P2196.0	PASS 250.88 C	85-4.7 (C) -1.58	0.230	201
148 57	P1#2156.0	7455 240.68 C	85-4.7 ICI	0.223	201 2.07
169 57	P1P2194.0	277.68 C	85-4.7 (C) -4.80	0.257	201 2.07
			85-4.7 (0)	0.241	201
190 21	P117134.0	PASS 292.01 C	85-4.7 (C) -0.20	0.60	2.07
101 17	P1P2196.0	PASS	85-4.7 (C)	0.253	241
		316.30 C	-0.37	6.00	0.00
192 ST	P172196.0	PASS	85-4.7 (0)	0.208	201
		311.79 C	-5.72	0.00	0.00
193 ST	P192196.0	7355	85-4.7 ICI	0.223	201
		241.68 C	-1.05	0.00	0.00
194 ST	P1P2196.0	PASS	85-4.7 (C)	0.228	201
		248.85 C	-2.43	0.00	0.00
195 ST	P1P2196.0	PA55 297.61 C	85-4.7 (C) -2.58	0.273	203
196 57	PIP2156.0	PASS 273.45 C	85-4.7 (C) -1.53	0.251 0.00	201
197 ST	P1P2196.0	PASS 318.21 C	85-4.7 ICI -2.40	0.292	205
194 ST	PIP2196.0	FASS 363.10 C	85-4.7 (C) -2.97	0.00	205

Bolivere Element to Tenestry Pie LLd	Job No TPL40581	Sheet No a 111	Rev R4b-FAB		
	Partwind speed 32.5 m/s				
Job Tile Wisma Bella Swimming Pool	Ref Fabric R5				
	BY TSM	Dale17-Dec-11	Che TSM		
Class	Eta anna una a	in Internet			

el	Design	(Track	0)	Checks	Cont	

ALL UNITS	NAE - KN	HETE IUNLE	SS OTHERNISE NOTED	1	
HEHBER	TABLE	NESVLT/	CRITICAL COND/	HATIO/	LOADING
245 1	ST PIP2194.0	PASS 222.20 C	85-4.7 (C) -3.75	0.206	201 2.0
					*******
266 1	T PIP2196.0	PASS 225.41 C	85-4.7 (C) -0.23	0.209	201 2.0
267 5	T P3P2196.0	7A55 255.34 C	85-4.7 (C) -0.32	0.236	201
268 5	T P2P2196.0	232.04 C	81-4.7 (C) -4.64	0.233	203
269 5	T P1P2196.0	PASS	85-4.7 (C)	0.143	201
		197.27 C	-0.85	8.00	0,0
276 4	T P1P2196.0	PASS	85-4.7 (0)	0.189	201
		206.25 C	-2.21	0.00	0.0
271 5	T PIP2196.0	PASS 239.42 C	05-4.7 IC) -2.60	0.220	201
272 5	T P1F2194.0	PASS	85-4.7 (C)	0.212	205
		230.86 C	-1.66	0.00	0.0
		19.55	85-4.7 (C)	0.265	285
273 5	T PIP2196.0	218.47 C	-2.18	0.245	205
		*******			
274 5	T P1P2196.0	7855	85-4.7 (C)	0.307	205
		334.24 C	-2.77	0.00	0.0
			85-4.7 (0)	0.338	205
275 5	T P1P2194.0	PASS 348.92 C	-3.80	0.00	0.0
276 3	T \$1\$2196.0	PASS 317.48 T	\$5-4.8.2.2	0.368	204
		317.48 T	-6.09	0.00	1.0
272 5	T P1P2196.0	PASS	M-4.8.2.2	0.406	204
		341.93 T	-7.25	0.00	1.7
278 5	T PIP2196.0	PASS 333.54 T	#5-4.9.2.2 -7.48	0.401	204
279 5	T P1P2196.0	PASS	85-4.7 (C)	0.358	205
		389.59 C	-5.24	0.00	0.01
	T PIP2196.0	FASS	85-4.7 (C)	0.333	
		362.97 C	-4.26	0.00	0.00
					245
201 5	T P1P2196.0	PASS 325.43 C	85-4.7 (C) -4.02	0.235	0.00
242 5	T P1P2196.0	PASS 278.10 C	85-1.7 (C) -3,57	0.255	205
			-7.57		
283 5	T P1P2194.0	PASS	85-4.7 (C)	0.203	205
		221.83 C	-3.62	0.00	0.00
					208
284 5	T P1P2194.0	PASS 170.51 C	85-4.7 (C) -1.85	0.156	0.00
285 5	T PIP2196.0	PASS 173.77 C	85-4.7 (C)	0.159	205

STAAD.Pro for lows 20.07.02.15



8	TPL40581	Sheel No	a 112	Rav R4b-FAB		
Software licensed to Transerve Pie Lid	Partwind speed 32.5	m/s				
ob Title Wisma Bella Swimming Pool	Ref Fabric R5					
	BY TSM	Dale17-D	ec-11 CMT			
<sup>lant</sup> Majlis Perbandaran Kuantan	Fla Q325-KSP-R4b	Deg.std	Date/Time 10-Jul-	2012 16:43		
Steel Design (Track 0) Checks Cont ALL UNITS ARE - IN HETE (WALES OTHERMISE HOTED) HEMBER TABLE REDVET CATTOR COMP. MATCH LOADING!						
IX NT XZ DOCYTON						
155.64 C -1.61 8.00 1.78						
101.27 C -2.51 0.00 1.78						
289 57 FIF2156.0 PASS 85-4.7 [C] 0.217 254 236.76 C -3.27 0.00 1.78						
290 ST P1P2196.0 PASS 85-4.8.2.2 0.272 205 233.75 T -4.55 0.00 1.49						
291 57 F1P2195.0 FASS 85-4.8.2.2 0.334 205 274.92 7 -6.40 0.00 1.64						
292 ST P1P2196.0 PASS 85-4.7 (C) 0.343 204 374.44 C -4.99 0.00 1.78						
293 57 P1P2156.0 PASS 85-6.8.2.2 0.377 205 313.91 7 -7.06 0.00 1.78						
294 ST PIP2196.0 PA35 B1-4.7 (C) 0,400 204 435.95 C -5.83 0.60 1.78						
255 5T P1P2194.0 PASS 85-4.7 (C) 0.385 204 424.38 C -2.84 0.10 1.78						
296 ST P1P2196.0 PASS 85-4.7 (C) 0.367 204 (0.44 C -3.93 0.00 1.78						
297 ST P1P2196.0 PASS 85-4.7 (C) 0.314 704						
288 ST P1P2186.0 PASS 85-4.7 (C) 0.289 204						
299 57 PIP2196.0 PA55 85-4.7 (C) 0.251 701						
274,17 C -1.40 0.40 1.19 308 57 9392194.0 PASS 55-4.7 [C] 6.255 201 282.66 C -2.72 8.60 1.19						
242.44 C -2.72 6.60 1.78						
303 57 PIP2196.0 PASS 85-4.7 (C) 0.184 201 200.22 C -1.34 0.00 1.78						
362 57 P1P2196.0 PASS 85-4.7 (C) 0.178 201 192.57 C -0.85 0.60 2.07						
303 57 F1F2194.0 FA55 85-4.7 [C] 0.205 201 221.32 C -3.75 0.00 2.07						
264 57 7772196.0 PASS 85-4.7 (C) 0.208 201 224.66 C -0.27 0.60 2.67						
205 57 FJF2196.0 FASS 85-4.7 (C) 0.207 201 223.79 C -0.16 0.00 0.00						
306 ST P1P2196.0 PASS 85-4.7 (C) 0.266 201 220.74 C -3.99 0.60 0.00						
387 57 7272194.0 PASS 85-4.7 (C) 0.177 201 190.85 C -0.72 0.00 0.00						
346 ST P1P2396.0 PASS 85-4.7 (C) 0.187 201 283.46 C -3.87 0.00 0.05						

STAAD Bra (as Windows 20 07 02 45

Pdat Bus 14 af 104

Solvare Scansed to T					TPL40581	a 113	R4b-FAB
					Parlwind speed 32.5	5 m/s	
					Ref Fabric R5		Rev Rdb-FAB2 TSM -2012 16:43
					BY TSM	Osle17-Dec-11 Ch	TON
<sup>mt</sup> Majlis Perbandaran Ki	unation					-Deg.std Date/Time 10-J	
majis r cipalica al ri	Variati				Gozo-Kor-Kep	-Deg.5(0	0-2012 16:43
	TE (UMLES	CRITICAL COND/	RATIO/	LOADING/ LOCATION			
305 ST PIP2156.0	7355 65.33 C	85-4.7 (C) -3.14	0.243 0.00	201			
310 ST P1P2196.0		85-4.7 (C) -1.39	0.222	201 0.00			
311 ST PIP2194.0	PASS 94.37 C	85-4.7 (C) -2.31	0.278	205			
312 ST PIP2196.0	PASS 6.83 C	85-4.7 (C) -2.46	0.305	205			
313 ST P192196.0 30	PASS 68.26 C	85-4.7 (C) -3.63	0.338	205			
314 ST P3P2196.8	PASS 10.50 C	85-4.7 [C] -1.35	0.358	205			
315 ST PIP2196.0	PASS 0.53 T	83-4.8.2.2 -10.08	0.404	204			
316 ST P1P2196.0 29		83-4.8.2.2 -10.71	0.405	204			
317 ST PIP2196.0 37	PASS 9.25 C	85-4.7 (C) -5.08	0.348	205			
318 ST F1F2196.0	PASS 0.36 C	85-4.7 (C)	0.321	205			
315 ST F1F2196.0	PASS 1.00 C	85-4.7 (C) -3.86	0.285	205			
320 ST 9192196.0 26	7A55 1.52 C	85-4.7 (C) -3.39	0.245	205			
121 ST PTP2186 A	PASS 4.03 C	85-4.7 (C) -2.81	0.107	205			
322 ST P1P2196.0	PASS I. E) C	85-4.7 (C) -1.68	0.146	205			
323 ST P1P2196.0	PASS 2.05 C	85-4.7 (C) -1.80	0.149	206			
	8.66 C	85-4.7 (C) -1.67	0.146	206			
325 ST P1P2186.0	PA38 0.36 C	95-4.7 (C) -1.52	0.136	106			
326 ST P1P2196.0	PASS	85-4.7 (C) -2.38	0.158 0.00	204			
327 ST PIP2196.0	PASS	85-4.7 (C) -3.14	0.209	204			
328 ST P1P2196.0	PASS	85-4.1.2.2 -4.45	9.263	205			
329 57 P1P2196.0	PASS	85-4.8.2.2 -6.30	0.319	205			
234 ST P1P2196.0		83-4.7 (C) -4.95	0.336	204			

2			TPL40581
Software licensed to Transerve Pie Lid			Partwind speed
Jeb Tite" Wisma Belia Swimming Pool			Ref Fabric R5
			BY TSM
Clent Majlis Perbandaran Kuantan			Fle Q326-KSP-
Steel Design (Track 0) Checks Con ALL UNITS ARE - IN HETE (UNLESS OTHERWISE			
		LONDING/	
FX HY	ĸt	LOCATION	
331 57 PIP2196.0 PASS 85-4.8.2.2 186.85 T -10.27	0.396	205	
***************************************		1.70	
332 ST P1P2196.0 PASS B5-4.7 0 425.50 C -5.83	C) 0.394 0.00	204	
233 ST PIP2194.0 PASS 85-4.7 0 415.41 C -3.62	CI 0.285		
		1.75	
	C) 0.354 0.00	204	
		204	
J#2.13 C -J.12	6.00		
336 57 9392196.0 PASS 85-4.7 (0 315.30 C -2.45	C) 0.289	204	
337 ST PIP2196.0 PASS 85-4.7 (0 263.76 C -1.54	C) 0.242 0.00	201	
338 ST PIP2196.8 PASS 85-4.7 10	0.252	201	
***************************************			
		201	
340 ST P1P2196.0 PASS B5-4.7 (C 180.84 C -0.79	6,00	201 2.07	
341 ST P1P2196.0 PASS 85-4.7 [C 215.75 C -3.67	c) 0.200 0.00	201	
342 ST P3P2196.0 PASS 85-4.7 (C 219.00 C -0.17		201 2.07	
143 ST 0103186 0 0855 03-4-7 10	0.205	201	
222.90 C -0.43	0.00	0.00	
		201	
345 ST P1P2194.0 PASS B5-4.7 IC 190.09 C -0.05	0.176 0.00	201	
	0.00	201	
	1 0.241 0,00	201	
		205	
297.85 C -2.32	1 0.273 0.00	0.00	
350 ST PIP2196.0 PASS 85-1.7 (C	0.315	205	
342.00 C -2.03	0.00	0.00	
351 ST P1P2196.0 PASS 85-4.7 (C 376.81 C -3.50	0.346 0.00	205	
352 ST P1P2156.0 PASS 85-4.4.2.2 330.88 T -6.05		204	
230.86 7 -6.05	0.00	1.04	

2						Job No TPL40581	shael No a 116	Rev R4b-FAB
2	Itware licensed	In Transerve P	te Lui			Partwind speed 32.	5 m/s	
	Bella Swim					Ref Fabric R5		
						By TSM		TSM
Majlis	Perbandarar	Kuanlan				File Q326-KSP-R4	-Deg.sid Data/Time 10-	Jul-2012 16:43
ALL UNITS	AAE - KH TABLE	HETE (UNLE RESULT/	hecks Cont ss отисянияс нотер скитисы соне/ нт	AATIO/	LOADING/			
			85-4.7 (C) -1.52	0.239	201			
	T PIP2196.0		83-4.7 (C) -2.71	0.250 0.00	201			
	T P3P2196.0		85-4.7 (C) -1.43	0.179 0.00	201			
	7 9192156.0		85-4.7 (C) -0.85		201 2.07			
379 5	T #1#2196.0	PASS 214.27 C	85-4.7 (C) -3.44	0.19# 0.00	201 2.07			
3 0 0 6	T P3P2396.0	PASS 217.44 C	-0.34	0.201 0.05	201 2.07			
		PASS (18.52 C	85-4.7 (C) -7.33		208			
342 5	F PIP2156.0	PASS 402.16 C		0.372	208			
383 57	PIP2196.0	PASS	85-4.7 (C)	0.231	208			
384 51	FIP2196.0	PASS 104.19 T	MS-4.4.2.2 -12.54	0.252	208			
385 57	*1P2156.0	PA55 72.55 C	AMEX 1.1 -8.31	6.387 20.34	208			
386 51	P1P2156.0	PASS 167,70 T	45-4.4.2.2	0.228				
			85-4.8.2.2					
			85-4.8.2.2 -5.83	0.247	0.00			
288 57	P3P2194.0	PASS 286.67 T		0.235 0.60	1.71			
				0.293	205			
350 51	P1P2196.0	171.44 C	NS-4.7 (C) -2.35	0.343	205			
	P1P2194.0	PASS (13.46 C	85-4.7 (C) -2.48	0.375	205 0.00			
392 57	P1P2196.0	PASS 143.92 T	15-4.8.2.2 -18.15	0.372 0.00	204 0.00			
393 51		PASS 178.21 T		6.293 0.00	204			
394 57		PASS 207.52 T	85-4.8.2.2 -7,40	0.246 0.00	204			
355 57	P172196.0	PASS	85-4.4.2.2	0.296	204			
396 57	P172196.0	PASS		0.262	204			

Print Time/Date: 11/07/2012 17:2

	2					Job No TPL40581	Sheel No	a 117	Rev R4b-FAB
	Software Ecensed	In Transmer P	-			Partwind speed 3	2.5 m/s		_
Job Title	Wisma Beila Swin					Rel Fabric R5			
						BY TSM	Dale17-D	ec-11 Ord	TSM
Client	Majlis Perbandara	n Kuantan				Pa Q325-KSP-R			
	teel Design (T								
	LL UNITS ARE - IN								
	CHBER TABLE	TX	CRITICAL COND/ HY	HATIO/	LOCATION				
	397 ST P1P2196.0	PASS 221.52 T	85-1.8.2.2 -6.88	0.292 0.00	207				
	398 ST P1P2196.0		#5-4.#.2.2 -1.77	0.309 0.00	207				
	355 ST #1#2156.0	PASS	85-4.8.2.2	0.388	207				
-		222.59 7	-14.00	0.00	1.70				
	400 ST PIP2196.0	PASS	83-4.8.2.2	0.385	207				
-									
	401 ST P1P2196.0	224.62 7	85-4.8.2.2	0.306	1.74				
-	402 ST #1#2196.0	PASS	85-4.8.2.2	0.290	207				
-		217,76 T	-6.96	0.00	0.00				
	483 ST P1P2196.0	PASE 203.38 T	85-4.0.2.2	0.313	205				
	404 ST P1P2196.0	214.90 7	85-4.8.2.2 -4.88	0.255	205				
	405 ST P1P2196.0	PASS	85-4.9.7.2	0.261	205				
-		195.22 7	-6.34	0.00	1.24				
	406 57 9392195.0	PASS 290.04 C	85-4.7 (C) -2.72	0.265	204				
	407 ST PIP2196.0	PASS 131.99 T	AS-4.8.2.2 -17.73	0.355	205				
	408 ST P1P2156.0	PASS	83-4.8.2.2	0.367	209				
		156.44 7	-16.90	0.00	0.00				
	409 ST P2P2196.0	PASS 359,77 C	85-4.7 (C) -4.35	0.322	204				
		*********							
	410 57 2122196.0		85-4.7 (C) -2.43	0.283	204				
	411 ST PIP2196.0	PASS	85-4.4.2.2	8.244	,				
		188.47 7	-5.53	6.00	0.00				
	412 ST P2P2196.0	PASS 177.27 T	85-4.0.2.2	0.234	1.78				
	413 ST P1P2196.0	PASS 160.54 T	85-4.8.2.2 -5.54	0.220	1.78				
	414 ST 9192196.0		ANDX 1.1	0.394	208				
			-8.48	20.68					
	415 ST PIP2196.0	PASS	85-4.8.2.2	0.245	208				
	416 ST P1P2196.0		85-4.7 (C) -5.10	0.235	208				
	412 ST P10214E A	****	#5-4.7 (C)	0.376	208				
	417 ST P1P2196.0		-3.48	0.00	2.07				
	418 ST 9192196.0	PASS	65-4.7 (C) -7.01	0.391	208				
		422.46 C	-7.01		2.67				

					TPL40581	Sheel No	a 118	Rev R4b-FAB
Software Scenard	In Transma (	tal M			Partwind speed 32.5	m/s		
ab Tile Wisma Bella Swim		10 6.00			Ref Fabric R5			
					By TSM	Opie17-D	ec-11 Chi T	SM
Majlis Perbandaran	Kuantan				Ple Q326-KSP-R4b			
Steel Design (Tr								
		CAITICAL COND/		LOADING/				
		HT		LOCATION				
419 ST P1P2196.0		85-4.7 (C) -9.44	0.334 8.00	208				
428 ST 9192194.0	PASS 357.38 C	85-4.7 (C) -7.78	0.331 0.00	208				
421 ST P1P2196.0	PASS 330.50 C	85-4.7 (C) -6,48	0.306	208				
422 ST 9392194.0	PASS		0.292	201				
423 ST 9192194.0		AMMEX 1.1 -8.51	0.390	208				
424 57 9192196.0		85-4.7 (C) -3.62	0.275 0.60	203				
425 ST P1P2136.0			6.299	205				
426 ST 9392196.8	326.25 C	85-4.7 (C)	0.00	0.00				
	349.24 C		0.00	0.00				
427 57 9192196.8		-4.41	0.00	0.00				
428 ST PIP2196.0		85-4.7 (C) -5.81	0.335	205				
429 ST P1P2196.0		15-4.1.2.2 -24.47	0.588 0.00	204				
436 57 PIP2196.0		85-4.8.2.2 -25.64	0.554 0.00	204				
431 ST P1P2196.0	PASS 272.69 T	85-4.8.2.2 -6.57	0.334 0.00	204				
432 ST P172196.0	PASS 251.22 T	85-4.8.2.2 -4.44	0.285	204				
433 ST 9192196.0	PASS	85-4.4.2.2	0.318	204				
434 ST P192196.0	PASS 177.51 T	85-4.8.2.2 -14.84	0.358	204				
(15 ST PIP2196 0		85-4.8.2.2 -3.99	0.277	208				
436 ST P172196.0		85-4.8.2.2	0.282	209				
437 ST \$192186.0		\$5-4.8.2.2	0.00	201				
	112.34 7	-17.04	0.00	1.70				
438 ST P1P2194.0	117.02 T	85-4.8.2.2 -16.87	0.331 0.00	203				
439 ST P1P2196.0	PASS 269.37 T	\$5-4.8.2.2 -3.50	0.250 0.00	208 0.00				
440 ST P172186.0	PASS 254.52 T	85-4.8.2.2 -4.00	0.288	208				
ni Time/Dale: 11/07/2012 17:28			TAAD Bro fe	r Windows 20.0	07 02 16			fel Run 20 of 104

a 114

Dale17-Dec-11 CM TSM b-Deg.sld DeleTime 10-Jul-2012 16:43

Rev R4b-FAB2

Vini Run 15 of 104



2	TPL40581	a 115	Rev R4b-FAB:
Software licensed to Transerve Pie Ltd	Parlwind speed 32	5 m/s	
Wisma Balla Swimming Pool	Raf Fabric R5		
	By TSM	Dete17-Dec-11 C	hd TSM
Majilis Perbandaran Kuantan	File Q326-KSP-R4	b-Deg.std Date/Time 10	Jul-2012 15:43

### gn (Track 0) Checks Cont...

	Jesign (Ti ts xxt - tor		SS OTHERWISE NOTES	15	
8EX	TABLE	ALSULT/	CRITICAL COMO/	NATIO/ ML	LOADING/ LOCATION
353	ST 9192196.0	PASS 355.81 T	85-4.8.2.2 -5.90	0.400 0.00	204
354	57 P1P2196.0	7355 347.10 T	85-4.8.2.2 -6.00	0.394 0.00	204 0.00
355	ST PIP2196.0	PASS 395.54 C	85-4.7 (C) -5.24	0.363 0.00	205
356	37 PIP2196.0	PASS 367.78 C	85-4.7 (C) -4.32	0.337 0.00	205
357	37 P1P2196.0	PASS 329.46 C	85-4.7 (C) -4.10	0.302 0.00	205
358	ST 71P2196.0	PASS 201.39 C	85-4.7 (C) -3,65	0.258 0.00	205
259	ST \$1\$2196.0	7355 224.31 c	85-4.7 (C) -3.03	0.206 0.00	205 0.00
360	ST 9192196.0	PASS 170.81 C	85-4.7 (C) -1.34	0.157	208
361	ST \$1\$2196.0	PA35 176.69 C	83-4.7 (C) -1.55	0.162	208
362	57 P1P2196.0	PASS 173.51 C	85-4.7 (C) -3.42	0.159	208
363	ST 9192196.0	PASS 161.24 C	NS-4.7 (C) -1.69	0.148 0.00	208
364	ST 9392196.0	PASS 194.69 C	85-4.7 (C) -2.63	0.179 0.00	264
345	ST 9392194.0	PASS 250.66 C	85-4.7 (C) -3.44	0.225	204 1.78
366	ST 9192196.0	PASS 251.41 T	85-4.8.2.2 -4.74	0.291 0.00	205
367 :	ST PIP2196.0	PASS 296.48 T	85-4.1.2.2 -6.59	0.356 0.00	205 1.04
368 1	ST <b>P1P2196.0</b>	PA35 384.92 C	85-4.7 (C) -5.06	0.355 0.00	204
369 1	FT P1P2196.0	PASS 421.20 C	85-4.7 (C) -1.94	0.386	204
370 :	FT PIP2196.0	PA35 (46.80 C	85-4.7 (C) -5.87	0.410	204
371 1	T P1P2196.0	PASS 433.79 C	85-4.7 (C) -3.90	0.358 0.00	204 1.78
372 1	T P1P2196.0	#A33 408.23 C	85-4.7 (C) -4.01	0.374 0.00	204
373 1	T P1P2196.0	PA55 369.74 C	85-4.7 (C) -3.16	0.335	204
374 1	T P1P2196.0	PA55 319.51 C	85-4.7 (C) -2.50	0.293	204

Edel TempfDale: 1107/2012 17

20.07.03

2	TPL40581 Shasi No a 119 R4				
Software Roomand to Transerve Pile Lid	Part wind speed 32.5 m/s				
eb Tille Wisma Bella Swimming Pool	Ref Fabric R5				
	By TSM 0	17-Dec-11 D	d TSM		
Client Majils Perbandaran Kuantan	F% Q326-KSP-R4b-De	std Detertime 10-	Jul-2012 16:43		

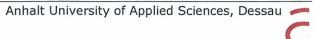
1	De	esic	i.	1	rack	0) Ch	ecks Co	nt
ж	175	AAE	•	101	NETE	IUNLESS	OTHEAHISE	NOTEDI

442 57 443 57 444 57 444 57 445 57 445 57 445 57 446 57	P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0 P1P2194.0	PX PASS 264, 21 T PASS 247, 65 T PASS 280, 67 T PASS 280, 67 T PASS 280, 67 T PASS 280, 67 T PASS 280, 61 T PASS 281, 22 T PASS 284, 21 T	NY 85-4, 8, 2, 2 -11, 73 85-4, 8, 2, 2 -4, 22 -5, 22 85-4, 8, 2, 2 -5, 22 85-4, 8, 2, 2 -5, 23 85-4, 8, 2, 2 -5, 23 -5, 24 -5, 25 -5, 25 -5	H2 6.341 6.346 6.336 0.223 8.60 0.593 8.60 0.593 8.60 0.593 8.60 0.593 8.60	LOCATION 205 1.74 205 205 1.04 205 205 1.74 205 0.00 205 1.74 205 0.00 205 1.74 205 0.00 205 1.74 205 0.01 0.01 0.0
442 57 443 57 444 57 444 57 445 57 445 57 445 57 446 57	P3P2134.0 P1P2134.0 P1P2134.0 P1P2134.0 P1P2134.0 P1P2134.0	204, 21 T PASS 247, 69 T PASS 280, 67 T PASS 292, 22 T PASS 288, 92 T PASS 288, 91 T PASS 218, 41 T PASS 218, 41 T	-11.73 85-1.4.2.2 -5.23 85-4.8.2.2 -5.23 85-4.8.2.2 -5.43 85-4.8.2.2 -5.43 85-4.8.2.2 -24.96 85-4.8.2.2 -24.96 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28 85-4.8.2.2 -25.28	e.00 e.386 e.00 e.323 e.00 e.327 e.60 e.543 e.60 e.543 e.60 e.543 e.60 e.543 e.60 e.543 e.60 e.543 e.60 e.543 e.60 e.545 e.60 e.555 e.60	1,74 205 0,04 205 1,04 205 0,00 205 1,74 205 0,00 205 0,00 205 204
443 57 444 57 445 57 446 57 446 57 447 57	P1P2194.6 P1P2194.6 P1P2194.6 P1P2194.6 P1P2194.6	247.69 T PASS 280.07 T PASS 292.32 T PASS 288.32 T PASS 288.41 T PASS 410.35 C	-6.22 85-4.4.2.2 -5.22 85-4.1.7.2 -5.43 85-4.4.2.2 -24.95 85-4.4.2.2 -24.95	0.00 0.323 0.00 0.537 0.60 0.557 0.60 0.597 0.60 0.377	0.04 205 1.04 205 0.00 205 1.74 205 0.00 204
444 57 445 57 446 57 447 57	P1P2196.0 P1P2196.0 P1P2196.0 P1P2196.0	PASS 280.07 T PASS 292.32 T PASS 288.22 T PASS 288.41 T PASS 410.35 C	85-4, 8, 2, 2 -5, 23 85-4, 8, 2, 2 -5, 43 85-4, 4, 2, 2 -24, 95 85-4, 4, 2, 2 -25, 28 85-4, 4, 2, 2 -25, 28	0.323 0.00 0.337 0.00 0.593 0.593 0.597 0.50 0.377	205 1.0 205 0.00 205 1.70 205 0.00 204
444 57 445 57 446 57 447 57	P1P2196.0 P1P2196.0 P1P2196.0 P1P2196.0	210.07 T PASS 292.32 T PASS 288.32 T PASS 288.41 T PASS 410.35 C	-5.22 85-4.1.2.2 -5.43 85-4.4.2.2 -24.95 85-4.4.2.2 -24.95 85-4.4.2.2 -25.29 81-4.7 (c)	0.337 0.50 0.593 0.597 0.50 0.597 0.50	1.04 205 0.00 205 1.74 205 0.00
445 57 446 57 447 57	P1P2196.0 P1P2196.0 P1P2196.0	PASS 292.32 T 285.52 T PASS 288.32 T PASS 288.41 T PASS 410.35 C	85-4.8.2.2 -5.43 85-4.4.2.2 -24.95 85-4.4.2.2 -25.20 85-4.7 (5)	0.337 0.60 0.593 8.00 0.597 0.50 0.337	205 0.00 205 1.70 205 0.00 204
445 57 446 57 447 57	P1P2196.0 P1P2196.0 P1P2196.0	292.32 T PASS 288.31 T PASS 288.41 T PASS 410.55 C	-5.43 B5-4.4.2.2 -24.85 B5-4.8.2.2 -25.20 B5-4.7 (5)	0.50 0.593 8.00 0.597 0.50	205 205 205 205 205 204
446 ST 447 ST	P1P2196.0	PASS 201.22 T PASS 210.41 T PASS 410.95 C	-24.95 85-4.4.2.2 -25.20 85-4.7 (C)	0.557 0.50 0.377	205 0.00 204
446 ST 447 ST	P1P2196.0	288.32 T PASS 218.41 T PASS 410.55 C	-24.95 85-4.4.2.2 -25.20 85-4.7 (C)	0.557 0.50 0.377	205 0.00 204
447 57	P1P2136.0	200.41 T PASS 410.95 C	-25.20	0.50	0.00 204
447 57	P1P2136.0	200.41 T PASS 410.95 C	-25.20	0.50	0.00 204
		410.95 C	85-4.7 (C) -7.13	0.377	
		410.95 C	85-4.7 (C) -7.13	0.377	
448 ST	P1P2196.0		****************		1.74
448 ST	P1P2196.0				
		PASS 389.09 C	85-4.7 [C] -5.05	0.357	204
449 ST	P1P2196.0	PASS 341.94 C	85-4.7 (C) -4.51	0.332	204
450 ST	P3P2396.0	PASS 332.77 C	85-4.7 (C) -5.03	0.305	200
451 57	P1P2196.0	203.48 C	85-4.7 (C) -3.25	0.278	201
	P1P2196.0	73.55		0.400	264
452 51	P1P2196.0	234.25 C	ANNEX 1.1 -0.00	18.61	200
	PIP2196.0	PASS	85-4.7 (C)	9.243	201
		308.03 C	-3.65	0.00	1.70
	192196.0	PASS	85-4.7 (C)	0.302	208
		327.22 C	-6.41	0.00	2.07
455 57	P1P2196.0	7455	85-4.7 (C)	0.329	208
		355.21 C	-1.72	0.00	2.07
456 57	P172196.0	PASS	85-4.7 ICI	0.332	208
		359.34 C	-9.43	4.00	2.07
457 57	*1+2736.0	73.55	85-4.8.2.2	0.331	202
		384.69 T	-12.81	0.00	1.54
434 ST 1		****	85-4.8.2.2	0.526	202
		576.93 7	-12.81	0.00	0.00
459 ST 1		PASS	85-4.8.2.2	0.558	202
		573.93 T	-16.82	0.00	1.54
	1172736.0	PASS	85-4.4.2.2	0.848	202
		569.38 7	-51.37	0.00	1.54
(6)	192236.0	PASS	85-4.4.2.2	0.906	262
		(83.65 7	-65,43	0.00	6.00
	192736.0	PASS	85-4.8.2.2	0.617	282

Pdni Time/Dale: 11/07/2012

STAAD.Pro for Windows 20.07.02.15

Print Run 21 of 10



Job Tite Wilson Beals Swimming Pool         Jef F           Other         Magin Parbandarun Kuantan         Pie C           Steel Design / Track 0) Checks Conf         Auk with Auk - Hill Here (Muscle enterpite write)           Madin Track 0) Checks Conf         Auk with Auk - Hill Here (Muscle enterpite write)           Madin Track 0) Checks Conf         Made (Strephylon (Stre		Dale 17-D	Ise-11 Ф4 Т  ОН47549 10-Jul	
Witsma Bolis Swieming Pool         Mr/s         Mr/s <th< th=""><th>abric R5 'SM</th><th>Dale 17-D</th><th></th><th></th></th<>	abric R5 'SM	Dale 17-D		
Magine Perhandrame Kuundan         Pre           Steel Design (Track 0) Checks Cont Makunta Akt - NN HET (Musici entements Herris) Herris (1997) - 10000 - 10000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 10				
Sitel Design (Track 0) Checks Conf           ALK UNIT ALK - NOI HEITE (MULLI ORDMULL HEITE)           HEIDEN TOLE AND ALK DISTRICT ORDMULL HEITEN           HEIDEN TOLE AND ALK DISTRICT ORDMULL HEITEN           (10 FF 107716.4 PARK BA-14.2.2 6.11.1 20.0 0.000000000000000000000000000	3226-KSP-R46	-Deg.std	Date/Tore 10-Jul	-2012 16:43
ALL GUITA ALT - ARI MET, GUIDALE GENERIE METERIE           Memory Table         Network Control Conserve Meteries           400 MET 2017/L-4         Meteries Control Conserve Meteries           401 MET 2017/L-4         Meteries Control Control Conserve Meteries           401 MET 2017/L-4         Meteries Control Contr				
R         H				
(D).4 T         -1.6         4.6         5.6           (61 ST PR73).4 [03.7]         (03.7]         (-4.1.2)         (-1.7)         (-1.7)           (63 ST PR73).4 [03.7]         (-1.2)         (-1.7)         (-1.7)         (-1.7)           (63 ST PR73).4 [03.7]         (-1.2)         (-1.7)         (-1.7)         (-1.7)           (44 ST PR73).4 [03.7]         (-1.7)         (-1.7)         (-1.7)         (-1.7)           (44 ST PR73).4 [03.7]         (-1.7)         (-1.7)         (-1.7)         (-1.7)           (44 ST PR73).4 [03.7]         (-1.7)         (-1.7)         (-1.7)         (-1.7)           (45 ST PR73).4 [03.7]         (-1.6)         (-				
46 37 10773.4         Mail         Ho-4.2.3         6.2.4         Ho           46 37 10773.4         Mail         Ho-4.2.3         6.2.4         1.2.4         1.2.4           46 37 10773.4         Mail         Ho-4.2.3         6.2.4         1.2.4         1.2.4           47 37 10773.4         Mail         Ho-4.2.3         6.2.4         1.2.4         1.2.4           47 37 10773.4         Mail         Ho<4.2.2				
46 87 F12723.6         Mar.         B=-4.2.2         6.46         Mar.         B=-4.2.2           473 87 F12723.6         Mar.         B=-4.2.2         6.46         32           473 87 F12723.6         Mar.         B=-4.2.2         6.46         32           443 87 F12723.6         Mar.         B=-4.2.2         6.46         1.34           443 87				
40         37         211         10         41         10         41         10         41         10				
OF F10703.4         Mag         ModE 1         Long         Long <thlong< th="">         Long         Long</thlong<>				
401 ST P10716.4         Page         Pagee         Page				
40 FF 7127314.3         Mark         Mark f. J.         J.         L.         St.         St.<         St.<         St.<         St.<         St.<         St.<         St.<         St.<         St				
05 57 1912/36.8         Mass         19-6,1,2,3         1.55         1.55           •11 17 1917/36.4         Mass         19-6,4,2,3         6.08         1.75           •11 17 1917/36.4         Mass         19-6,4,2,3         6.08         1.75           •12 17 1917/36.4         Mass         19-6,4,2,3         6.08         10           •12 17 1917/36.4         Mass         19-6,4,2,3         6.08         10           •13 17 1917/36.4         Mass         19-6,4,2,3         6.08         10           •13 17 1917/36.4         Mass         19-6,4,2,3         6.03         10           •13 17 1917/36.4         Mass         19-6,4,2,3         6.03         10           •13 17 1917/36.4         Mass         19-6,4,2,3         6.03         10           •15 60 7         19-6,4,2,3         4.04         1.76           •15 60 7         19-6,4,3,2         4.03         1.78           •15 17 1917/36.4         Mass         19-6,4,3,2         4.03         1.78           •15 60 7         19-6,4,3,2         4.03         1.78         1.78           •15 60 7         19-88         19-6,4,3,2         4.03         1.78           •15 11 7         19-88         19-6				
01, 37 812734.8         Mass         M-4,3,2,3         5,439         M-4           01, 37 812734.8         Mass         M-4,3,2,3         6,03         5,56         5,56           01, 37 812734.6         Mass         H-4,6,2,3         6,03         34         5,56           01, 37 812734.6         Mass         H-4,6,2,3         6,03         34         5,56           01, 37 812734.6         Mass         H-4,6,2,3         6,04         5,56         5,56           01, 37 812734.6         Mass         M-6,1,2,3         6,04         1,66         16,6           01, 37 812734.6         Mass         M-6,1,2,3         6,02         1,78           01, 57 812734.6         Mass         M-6,2,3         6,03         1,78           01, 57 812734.6         Mass         M-6,3,3         6,03         1,78				
01 ST 919731-6         PASS         DF-LA,2         0.03         A-1				
473 57 9797354.8 985 88672 1.1 4.446 735 4.02 5 - 46.27 4.34 - 4 .03 57 9797354.8 985 91-4.5.2, 4.422 309 134,97 91-2154.9 14-4.5.2, 4.422 309 134,97 917234.8 985 91-4.5.2, 4.423 149 435,97 917234.8 985 91-4.5.2, 4.43 4.44 134,97 917234.8 985 91-4.5.2, 4.44 4.44 134,97 917234.8 985 91-4.5.2, 4.44 4.44 134,147 917234.8 914 4.44 4.44 4.44 4.44 4.44 4.44 4.44				
C14 57 F172326.0 PAS5 B3-61.5.7 0.022 209 138.64.7				
475 87 F122736.0 PASS 85-4.8.2.2 0.423 205 131.12 T -42.14 0.00 0.00				
476 5T P1P2736.0 PASS MONEX 1.1 0.665 207 88.94 C -45.94 31.50 -				
477 3T P1P2736.0 PASS ANNEX 3.1 0.645 207 88.53 C -45.54 31.80 -				
478 ST P1P2736.0 PASS 83-4.8.2.2 8.621 209 131.12 T -41.94 8.09 1.79				
479 57 9192736.0 PASS ANNEX I.1 0.768 205 0.05 C -44.67 45.75 -				
410 57 P1P2736.0 PASS ANNEX 1.1 0.654 205 0.25 c -65.31 34.61 -				
441 ST P1P2734.0 PASS 85-4.8.2.2 0.656 205 126.43 T -66.47 0.69 0.80				
442 5T P1P2324.0 PASS 85-4.8.2.2 0.581 202 212.20 T -50.33 0.60 1.78				
443 5T PIP2736.0 PASS 85-4.8.7.2 0.580 202 310.22 7 -50.33 0.00 0.00				
444 87 P1P2734.0 PX55 XMEX 1.1 0.677 207 31.45 C -24.43 54.77 -				

STAAD Pro for Windows 20 07 02 15

Print Run 22 el 104

0		TPL40581	Sheet No	a 121		Rev R4b-FAB
Software Econsed to Transerve Pie Lid		Partwind speed 32	5 m/s		_	-
The Wisma Belia Swimming Pool		Ref Fabric R5				
		By TSM	Dale17-D		Chd TS	
Malle Dechanderes Kunsten						
Majils Perbandaran Kuantan		Fle Q326-KSP-R4	b-Deg.sld	Cherman	10-Jul-	2012 16:43
Steel Design (Track 0) Checks Cont						
HDIER TABLE RESULT/ CRITICAL COND/ RATIO/	LOADING/					
TX HY HI	LOCATION					
445 ST P1P2736.0 PASS ANNEX 1.1 0.873	208					
5.01 C -44.17 50.51						
486 ST F1F2736.0 FAIS 85-4.8.2.2 0.503	202					
192.74 T -42.80 0.00	1.78					
487 ST PIP2736.0 PASS 85-4.8.2.2 0.506	202					
196.86 T -42.80 0.00	0.00					
488 ST P192734.0 PASS 85-4.8.2.2 0.715 199.59 T -47.12 0.00	202					
499 ST P1P2736.0 PASS 85-4.8.2.2 0.847 471.75 T -64.28 0.00	262					
450 57 PJP2736.0 PASS 85-4.8.2.2 0.489 475.47 7 -31.25 0.00	202					
491 ST PIP2736.0 PASS 85-4.4.2.2 0.616 484.45 7 -33.25 8.00	202					
484.45 T -33.25 0.00	0.00					
492 ST P1P2736.0 PR55 85-4.8.2.2 0.899	202					
405.75 T -64.46 0.00	1.70					
493 ST PIP2736.0 PASS 85-4.8.2.2 0.843 571.07 T -50.59 0.40	202					
571.07 T -50.59 0.60	0.00					
494 ST F1F2736.0 FASS 85-4.8.2.2 0.555 575.70 T -16.78 0.00	202					
495 ST PIP2736.0 PASS 85-4.8.2.2 0.527 578.83 T -12.75 0.50	202					
				1		
496 ST P1P2736.0 PASS B5-4.8.2.2 0.533 586.53 T -12.79 0.80	202			1		
497 57 P1P2736.0 PASS 85-4.4.2.2 0.529	202					
542.95 7 -12.63 0.40	0.00					
496 ST F1F2734.0 FASS 85-4.8.2.2 0.538 578.50 T -13.17 0.00	202					
	1.54					
499 ST P1P2734.0 PASS B5-4.8.2.2 0.559 572.81 T -17.00 0.00	202					
572.81 7 -17.00 0.00	1.54					
500 ST PIP2736.0 PASS 85-4.8.2.2 0.844 569.57 T -50.85 0.00	202					
501 ST P1P2736.0 PASS 85-4.4.2.2 0.859 494.42 T -64.54 0.00	202					
502 ST P1P2736.0 PASS 85-4.8.2.2 0.667	102					
481.15 T -30.49 0.00	1.70					
	202					
475.57 7 -30.45 0.60	0.50					
504 ST P1P2736.0 PASS 85-4.8.2.2 0.892	202					
468.21 T -65.21 0.00	1.78					
505 ST 9192736.0 PASS 85-4.8.2.2 0.727 205.51 7 -44.06 0.00	202					
506 ST P1P2736.0 PASS 85-4.8.2.2 0.504 138.35 T -42.46 0.00	202					

TAAD Pro for W

20 07 02 1

2						TPL40581	sheet No a 122	Rev R4b
2.	livers Fornsed	i la Transerva P	'le Lid			Parlwind speed 32.	5 m/s	
Job Title Wisma	a Belia Swin	ming Pool				Ref Fabric R5		
						By TSM	Dale17-Dec-11 C	M TSM
Ctent Majlis	Perbandara	n Kuantan				File Q326-KSP-R45	-Deg.std Date/Time 10-	Jul-2012 1
ALL UNITS	ARE - KH TABLE	HETE IUNLE	hecks Cont	:0)	LOADING/			
507 5	T P1P2736.0	PASS	AS-4.8.2.2 -42.46	0.504	202			
	T P1P2736.0		AMMER 1.1 -(1.56	0.847 57.75	205			
549 5	T P1P2736.0	PASS	B5-4.8.2.2 -67.54	0.672	204			
			-67,34 B3-6.8.2.2 -50.67	0.505	202			
	T P1P2736.0			0.00	1.78			
				0.00	0.00			
			85-4.8.2.2 -63.48	0.00	1.76			
	F P1P2736.0				205			
514 5	F P172736.0	PASS 135.28 T		0.631 0.00	207			
	F \$1\$2736.0		85-4.8.2.2 -62,70	0.631	207			
	P1P2736.0		ANNEX 1.1 -45.15	0.660 32.01	205			
517 51	* \$1\$2736.0	PASS 85.14 C	ANNEX 1.1 -45.19	0.660 32.02	209			
518 51	* *1*2736.0	PASS 136.00 T		0.629	207			
519 57	P3P2734.0	PASS 135.29 T	85-4.8.2.2 -62.46	0.628	207			
520 57	P1P2736.0	PASS 133.41 T	85-4.8.2.2	0.583	202			
\$21 ST	P172736.0	PASS 125.54 T		0.435	205			
522 57	P1P2736.0	PASS 214.05 T	85-4.8.2.2 -50,60	0.585	202			
523 57	P1P2734.0	PASS 212.65 T	85-4.8.2.2 -50.60	0.584	202			
	P1P2736.0			0.667	209			
525 ST	P1P2736.0			0.850	206			
526 57	P1P2736.0		85-4.8.2.2	0,505	202			
527 57	P1P2736.0	197.50 T PASS	85-1.8.2.2	0.00	202			
	P1P2736.0	197.24 T	-42.42	0.00				
	P1P2736.0	204.38 T	85-4.0.2.2 -67.91	0.00				

Jeb Tile Wisma Bella Swimming Pool R	TPL40581 Wind speed 32: Teshda RS TSM Q326-KSP-R4	5 m/s <sup>Dele</sup> 17-Di	R4b-FAE
Note:         Disk         Witzma Bells Swinning Pool         R           Steel         Magis Perbandaran Kuantan         P           Steel         Destant (Track 0) Checks Cont Att. Wortz Ak - Nor Yet: Workt Schwarzs Berten Hondes Takk Apple / Control (Schwarz) State (Track 0) Checks Cont Att. Wortz Ak - Nor Yet: Workt Schwarzs Berten State (Track 0) Checks Cont State (Track 0) Checks Cont Att. Wortz Ak - Nor Yet: Workt Schwarzs Berten State (Track 0) Checks Cont State (	Fabric R5 TSM	Dele17-Di	
Steel Evolution         F           2844         Majik Perbanduran Kuuntan         PK           Steel Evolution         700           Alk W17 Safer (Track 0) Checks Cont Alk W17 Safer (Track 0) Checks Cont Safer (Track 0) Chec	TSM		
Steel Design (Track 0) Checks Cont           ALK WITZ AND TARK 0 CHECKS Cont           310 ET FIRDUSLA PARK NACK 1 CHECKS Cont           311 ET FIRDUSLA PARK 0 CHECKS Cont           312 ET FIRDUSLA PARK 0 CHECKS Cont           313 ET FIRDUSLA PARK 0 CHECKS Cont           313 ET FIRDUSLA PARK 0 CHECKS Cont           314 ET FIRDUSLA PARK 0 CHECKS Cont           315 ET FIRDUSLA PARK 0 CHECKS Cont           316 ET FIRDUSLA PARK 0 CHECKS Cont           317 ET FIRDUSLA PARK 0 CHECKS Cont           318 ET FIRDUSLA PARK 0 CHECKS Cont           318 ET FIRDUSLA PARK 0 CHECKS Cont           318 ET FIRDUSLA PARK 0 CHECKS Cont           319 ET FIRDUSLA PARK 0 CHECKS Cont           310 ET FIRDUSLA PARK 0 CHECKS Cont           311 ET FIRDUSLA PARK 0 CHECKS Cont           312 ET FIRDUSLA PARK 0 CHECKS Cont           313 ET FIRDUSLA PARK 0 CHECKS Cont           314 ET FIRDUSLA PARK 0 CHECKS Cont           315 ET FIRDUSLA PARK 0 CHECKS Cont           316 ET FIRDUSLA PARK 0 CHECKS Cont <th>Q326-KSP-R4</th> <th></th> <th></th>	Q326-KSP-R4		
Steel Design (Track 0) Checks Cont           MALE UNLES INDER INTER           MORES TABLE INTER INTER           MORES TABLE INTER			
BALE, DUTE, AME, - NOP, MEET, INVESTIGATION, DUTE, MEET, MEET, CHITTOL, GRAW, METH, MARTHER, MEET, CHITTOL, GRAW, MITH, MARTHER, AND MARTH			
PARSE         TATLEX         PARSE         Control of the second			
F         F         F         E         DOUBLE           39 JF FEDDALA         PARE         46.94.7         46.94.7         46.94.7           39 JF FEDDALA         PARE         86.44.7.1         5.36.8         5.38           39 JF FEDDALA         PARE         86.44.7.1         5.36.8         5.38           39 JF FEDDALA         PARE         86.44.7.1         5.31.8         5.38           39 JF FEDDALA         PARE         86.44.7.2         5.31.8         5.38           30 JF FEDDALA         PARE         86.44.7.2         5.30.8         10.4           314 JF TERDALA         PARE         86.44.7.2         5.30.8         10.4           314 JF TERDALA         PARE         86.44.7.2         5.30.8         10.4           314 JF TERDALA         PARE         86.44.7.2         6.30.8         10.4           314 JF TERDALA         PARE         86.44.7.2         6.31.9         10.4           314 JF TERDALA         PARE         86.44.7.2         6.41.3         10.4           314 JF TERDALA         PARE         86.44.7.2         6.41.3         10.4           314 JF TERDALA         PARE         86.44.7.2         6.41.3         10.4           314 JF TER			
0.0.17         -5.36         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           354 17 7079.304.5 APAE         7-5.31         5.26         5.00         30           354 17 7079.304.5 APAE         7-6.31         5.20         30         30           354 17 7079.304.5 APAE         7-6.4         5.21         5.20         30           354 17 7079.304.6 APAE         8-64.5,21         5.20         30         30           354 17 7079.304.7 APAE         8-64.5,21         5.20         30         30         30           354 17 7079.304.7 APAE         8-64.5,21         6.31         30<			
0.0.17         -5.36         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           353 17 7079.304.5 APAE         7-5.31         5.26         5.00         5.00           354 17 7079.304.5 APAE         7-5.31         5.26         5.00         30           354 17 7079.304.5 APAE         7-6.31         5.20         30         30           354 17 7079.304.5 APAE         7-6.4         5.21         5.20         30           354 17 7079.304.6 APAE         8-64.5,21         5.20         30         30           354 17 7079.304.7 APAE         8-64.5,21         5.20         30         30         30           354 17 7079.304.7 APAE         8-64.5,21         6.31         30<			
17.3 T         -2.4         6.6         6.6           50 37 7779.3.0.4         33.6         7         6.4.3         5.3         6.5         6.6           35.6         77 779.3.0.4         30.6         7         6.4.3         6.3         6.6           35.6         77 779.3.0.4         30.6         7         6.4.3         6.3         6.6           35.6         77 779.3.0.4         30.6         7         6.4.4         6.3         6.6           35.6         77 779.3.0.4         30.6         7.6         5.3         6.6         6.6           35.6         77 779.3.0.4         8.6         6.4.3         6.6         6.6         6.6           35.6         77 779.3.0.4         8.6         6.4.3         6.6         6.6         6.6           35.6         77 779.3.0.4         8.7         8.6 - 6.3.2         6.3         8.6         6.6           350         77 779.3.0.4         7.64         8.6         6.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.6			
353 FT         FT P1P9-3.14: _ 30.20         10-4: 3.2: _ 5			
D. 0.1 Y         -1.0 //         6.0 //           34 JT JT JTHS.34.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JT JTHS.34.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JT JTHS.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JTHS.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JTHS.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JTHS.4 AGS         10.4 T         -1.6 //         1.6 //         1.6 //           34 JT JTHS.4 AGS         10.4 T         -1.1 //         1.6 //         1.6 //           34 JT JTHS.4 AGS         10.4 //         -1.1 //         1.6 //         1.6 //           35 JT JTHS.3 //         AGS         10.4 //         1.6 //         1.7 //           35 JT JTHS.1 //         AGS         10.4 //         1.6 //         1.7 //           36 JT JTHS.1 //         AGS         10.4 //         1.6 //         1.7 //           36 JT JTHS.1 //         AGS         10.4 //         1.6 //         1.7 //           36 JT JTHS.1 //         AGS         10.4 //         1.6 //         1.7 //			
314 ET FURD.34.6         RAST         84-6.7.2         6.36         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.36         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.30         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.30         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.31         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.33         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.34         24.9           315 ET FURD.34.6         RAST         84-6.7.2         6.34         1.9           316 ET FURD.34.6         RAST         84-6.7.2         6.34         1.9           316 ET FURD.34.6         RAST         84-6.7.2         6.34         1.9           316 ET FURD.34.6         RAST         84-6.7.2         6.34         1.9           <			
35 57 777233-5         0.001         0-4.5.3.4         6.01         30           35 57 77793-374.5         0.001         0-4.5.3.4         6.01         30           35 57 77793-374.5         0.001         0-4.5.3.4         6.01         30           357 57 7793-374.5         0.001         0-4.5.3.4         6.01         30           357 57 7793-374.6         0.001         0-4.5.3.2         6.201         30           357 57 7793-374.6         0.001         0-4.5.3.2         6.203         30           359 57 7793-374.6         0.001         0-4.5.3.2         6.203         30           359 57 7793-374.6         0.001         0-4.5.3.2         6.203         30           359 57 7793-374.6         0.001         0.001         0.001         1.00           359 57 7793-374.6         0.001         0.001         0.001         1.00           359 57 7793-374.6         0.001         0.001         0.001         0.001         0.001           360 57 7793-374.6         0.001         0.001         0.001         0.001         0.001           360 57 7793-374.6         0.001         0.001         0.001         0.001         0.001           360 57 7793-374.6         0.001 <td< td=""><td></td><td></td><td></td></td<>			
L.4.1         -1.3.1         5.2.1         -           34 ET 1775.34.7.4 AUX H-4.1.7.1         5.3.6         5.4         5.4         5.4         5.4           35 ET 1775.34.7 AUX H-4.1.7.1         5.4.7			
345 ET 17995.3X.4         MAR         H=C.1.2.2         C.241         346           357 ET 17955.3X.4         MAR         H=C.1.2.2         C.241         347           357 ET 17955.3X.4         MAR         H=C.1.2.2         C.241         347           357 ET 17955.3X.4         MAR         H=C.1.2.2         C.241         347           358 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         347           359 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         347           359 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         348           350 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         348           350 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         348           360 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         346           360 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         346           361 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         346           361 ET 17955.3X.4         MAR         H=C.1.2.2         C.243         347           362 ET 17955.3X.4         MAR         H=C.1.2.2         S.248         347			
1.1.4         -1.4         5.4         5.8           307         77         798.3         797.4         -5.4         5.8           307         77         798.3         797.4         -5.4         5.8         6.8           307         77         798.3         797.4         -5.4         5.8         6.8           307         77         797.4         7.4         -5.3         6.8         1.70           307         77         797.4         7.4         -5.3         6.8         1.70           308         77         797.6         7.4         -5.3         6.3         1.70           308         77         797.7         7.4         7.3         7.4         1.70           308         77         797.7         7.4         7.4         1.70         1.70           308         77         797.7         7.4         7.5         7.4         1.70           308         77         797.7         7.4         7.5         7.4         1.70           308         77         797.7         7.4         7.5         7.4         1.6           3017         797.7         7.4         7.5			
50 17         1793-384.5         348         16-4.3.2         6.30         36.3           318 37         1793-384.5         1644         34.4         36.4         36.3           318 37         1793-384.5         1644         34.4         36.4         36.3           319 37         1793-384.5         1644         34.4         36.4         36.3           319 37         1793-384.5         1644         1.3         36.4         36.4           319 37         1793-384.6         1644         1.3         36.4         36.4           319 37         1793-384.6         1645         1.3         36.4         36.4           319 37         1793-384.6         1645         1.3         36.4         36.4           319 37         164.6         1645         1.3         1.5         1.5         1.5           310 37         154.6         1647         1.4         1.6         37         1.5           310 37         164.7         164.8         1.4         1.6         37         1.5           310 37         164.7         164.8         1.6         1.5         1.5         1.5         1.5           310 37         164.7         <			
39 87 17195-316-4         M42, 84-4,5,2         6-13         34           39 87 17195-316-3         M43, 84-4,5,2         6-13         34           39 87 17195-316-4         M43, 84-4,5,2         6-13         34           39 87 17195-316-4         M43, 84-4,5,2         6-13         34           30 87 17195-316-4         M43, 84-4,5,2         6-13         34           30 87 17195-316-4         M43, 84-4,5,2         6-13         34           30 87 17195-316-4         M43, 84-4,5,2         6-13         6-14           30 87 17195-316-4         M43, 84-4,5,2         6-14         6-16           30 87 17195-316-4         M44, 84-6,5,2         6-16         6-16           30 87 17195-316-5         M44, 84-6,5,2         6-16         6-16           30 87 17195-316-6         M44, 84-6,5,2         6-16         6-16           30 87 17195-316-7         M44, 84-6,5,2         6-16         6-16           30 87 17195-316-7         M45, 84-6,5,2         6-16         6-17			
24.64         -0.07         6.68         1.78           50 FF 177133.4         20.07         16-16.2.1         5.03         16.03           10 FF 177133.4         20.07         16-16.2.1         5.03         16.03           10 FF 177133.4         20.07         16-16.2.2         5.03         16.03           10 FF 177133.4         20.07         16-16.2.2         5.03         16.03           10 FF 177133.4         20.07         16-16.2.2         5.03         16.03           10 FF 177134.5         P.08         16-16.2.2         5.01         16.03           10 FF 177134.5         P.08         16-16.2.2         5.01         16.03           10 FF 177134.5         P.08         16-16.2.2         5.03         16.03           10 FF 177134.5         P.08         16-16.2.2         5.04         16.03           10 FF 177134.5         P.08         16-16.2.2         16.03         107           10 FF 177134.5         P.08         16-16.2.2         16.04         107           10 FF 177134.5         P.08         16-16.2.2         16.04         107           10 FF 177134.5         P.08         16-16.2.2         16.04         107           10 FF 177154.5			
30 BF PEPIDIA 0         PAGE 10 BF         B-1-(3,2,2) (3,3)         5,31 (3,3)         30 (3,3)           160 BF         PEPIDIA 0,4,7         PAGE 10,3)         B-1-(3,2,2) (3,3)         5,31 (3,3)         30 (3,3)         1,30 (3,3)         1,30 (3,3)         1,30 (3,3)         1,30 (3,3)         1,30 (3,3)         1,30 (3,3)         1,30 (3,4)         1,			
36 37 H705.30.4 PM3         8-4.5.2.2 -1.53         6.18 -1.53         10.6 -1.53           36 37 H705.30.4 PM3         8-4.5.2.2 -1.53         6.11 -1.53         36 -1.53           36 37 H705.30.4 PM3         8-4.5.2.2 -1.53         6.11 -1.53         36 -1.53           36 37 H705.30.4 PM3         8-4.5.2.1 -1.53         5.13 -1.53         36 -1.53           36 37 H705.30.4 PM3         8-4.5.2.1 -1.53         5.14 -1.53         36 -1.53           36 37 H705.30.4 PM3         8-4.5.2.1 -1.53         5.14 -1.53         36 -1.53           36 37 H705.30.4 PM3         RM4.4.5.21         5.53         26 -1.53           36 37 H705.30.4 PM3         RM4.4.5.21         6.53         27 -1.53           36 37 H705.30.4 PM3         RM4.4.5.21         6.53         27 -1.53           36 37 H705.30.4 PM3         RM4.4.5.21         5.53         80 -1.53           36 37 H705.30.4 PM3         RM4.4.5.21         5.53         80 -1.53           36 37 H707.30.4 PM3         RM4.4.5.21         5.63         80 -1.53           36 37 H707.30.4 PM3         RM4.4.5.21         5.61         74 -1.53           36 37 H707.30.4 PM3         RM4.4.5.21         5.61         74 -1.53			
Mid BT FIFFE.BLG.F BASS         Bi-6-1.2.2         5.10         7.64           15.35         -1.25         6.10         6.65           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.11         7.64           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.11         7.64           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.13         7.64           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.13         7.64           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.13         7.64           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.16         2.77           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.16         2.74           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.16         2.74           36: 57         FIFFE.BLG.F         Bi-4.5.2.1         6.16         2.74           36: 57         FIFFE.BLG.F         B			
30. 57         F1795-324-4         PASE         Be-4-5-2.2         6314         234 <td></td> <td></td> <td></td>			
36 37 H7H35,374,3 PA8         86-4,5,2,2 -2,3         5,33         26           36 37 H7H35,374,3 PA8         86-4,5,2,2 -2,3         5,33         7,43         7,43           36 37 H7H35,374,3 PA8         AB8         86-4,5,2,2 -4,34         6,13         247           36 37 H7H35,374,3 PA8         AB6,4,5,2,2 -3,34         6,163         247           36 37 H7H35,374,3 PA8         Be-1,6,2,2 -3,34         6,163         247           36 37 H7H35,314,4 PA8         Be-1,6,2,2 -3,34         6,36         207           36 37 H7H35,314,4 PA8         Be-1,6,2,2 -3,34         6,36         207           36 37 H7H35,314,4 PA8         Be-1,6,2,2 -3,44         6,13         246           36 37 H7H35,314,4 PA8         Be-1,6,2,2 -3,44         6,13         246           36 37 H7H35,314,4 PA8         Be-1,6,2,2 -3,44         6,13         246			
36         37         PHIDS.2X.4         PASS         84-4.5.2.2         5.331         244           353         27         2.33         6.34         6.35         2.35         6.36         6.36           353         27         21.35         2.4         6.35         2.37         2.35         7.3			
16.017         -2.32         6.48         6.49           363.37         F107335.6         FA03         840         7.43         6.49           364.37         F107335.6         FA03         840         6.57         7.57           364.37         F107335.6         FA03         840         7.69         7.69         7.69           364.37         F1073.54.6         FA03         840         7.69         7.69         7.69         7.69           364.37         F1079.53.64         FA03         840         7.69			
Si3 SF P17138.5         PART         MME 1.1         6.13         191           181.3         -6.34         6.35         6.37         1.3           364 SF F1719.324.6         PASE         86-4.5.2         6.58         127           364 SF F1719.324.6         PASE         86-4.5.2         6.59         127           365 SF F1719.36.4.6         PASE         86-4.5.2         6.38         127           365 SF F1719.36.4.7         PASE         86-4.5.2         6.39         127           365 SF F1719.36.4.7         PASE         86-4.5.2         6.39         295           37.85         7         -2.48         6.49         264			
344 37 F1049.324.4 FM4         Be-(.3.2.2         6.369         207           3.37         3.24         6.86         207           3.46 37 F1049.324.6 FM45         Be-(.3.2.2         5.06         207           3.46 37 F1049.324.6 FM45         Be-(.3.2.2         5.06         207           3.46 37 F1049.324.6 FM45         Be-(.3.2.2         5.019         206           3.46 37 F1049.324.6 FM45         Be-(.4.2.2         5.019         206           3.46 37 F1049.324.6 FM45         Be-(.4.2.2         5.019         206           3.46 37 F1049.324.6 FM45         Be-(.4.2.2         5.019         206			
10.30 T         -3.54         6.68           465 JT 5179-J344,6 19.053         36-4,-1,2,3         6.588         207           2000         2000         2000         2000           366 ST 9779-J344,6 19.054         86-4,-1,2,2         6,419         204           366 ST 9779-J344,6 19.054         86-4,-1,2,2         6,419         204           366 ST 9779-J344,6 19.054         86-4,-1,2,2         6,419         204			
545 57 5795.124.0 PAES 85-4.8.2.2 6.568 207 22.11 7 -3.27 6.68 1.78 556 57 \$7795.124.6 PAES 85-4.6.2.2 6.419 206 17.01 7 -2.48 6.00 6.00			
22.83 T -3.37 0.00 1.70 566 5T 91999.1X4.0 PASS 85-4.8.7.2 0.415 204 17.01 T -2.48 0.00 0.00			
566 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.419 206 17.01 T -2.88 0.00 0.00			
567 ST P1P2726.0 PASS 85-4.8.2.2 0.348 202			
Jul. 32 T =13.22 0.00 0.00			
548 ST P1P85.1X4.0 PASS 85-4.8.2.2 0.296 202 18.67 -1.86 0.00 0.00			
18.67 7 -1.86 0.00 0.00			
549 ST P1P89.124.0 PAdS 85-4.8.2.2 0.250 206 40.85 T -0.88 0.00 1.70			
570 57 FIFES.1X4.0 FASS 85-4.8.2.2 0.415 204 55.97 T -1.75 0.60 1.70			
\$71 ST P1P49.1X4.0 PASS 85-6.8.2.2 0.555 206			
14.59 T -4.02 0.00 1.70			
572 57 PIP49.1X4.0 PASS 83-4.8.2.2 0.523 206 23.77 7 -3.80 0.00 0.00			

Print Time/Dala: 11/07/2012 17:3

8	TPL40581	Sheet No	a 125	Rav R4b-FAB
Sofware licensed in Transave Pie Lid	Parlwind speed 32	5 m/s		
teb Title Wisma Bella Swimming Pool	Raf Fabric R5			
	By TSM	Dale 17-D	ec-11 Chd T	SM
Clieni Majilis Perbandaran Kuantan	File Q326-KSP-R4	b-Deg.std	Date/Time 10-Jul-	2012 16:43
Steel Design (Track 0) Checks Cont				
HEMBER TABLE RESULT/ CRITICAL CONS/ RATIO/ LOADING/ FX NY HE LOCATION				
573 ST FIF1355.0 FASS 83-4.0.2.2 6.545 206 20.37 T -12.72 6.00 6.00				*3
574 57 51827336.0 PASS 85-4.8.2.2 0.253 202 338.02 7 -0.88 8.80 3.70				
575 57 FIF89.124.0 PASS 85-4.8.2.2 0.087 207 16.34 T -0.24 0.00 1.70				
576 ST PIP89.1X4.0 PASS 85-4.8.2.2 0.152 207 38.78 T -0.16 0.00 1.70				
577 3T P1P49-124.0 PAIS 85-4.8.7.2 0.212 201 50.42 T -0.05 5.00 8.00				
578 57 FIF85.124.0 PASS 85-4.4.3.2 0.156 207 31.73 7 -0.38 8.06 8.08				
575 57 PIP89.1X4.0 PASS 85-4.4.2.2 0.147 207 25.55 T -0.46 0.00 0.00				
580 57 P1P85.1X4.5 PASS 85-4.8.2.2 0.158 207 24.20 7 -0.25 0.46 1.70				
541 57 F1F69.1X4.0 FASS 85-4.8.2.2 8.163 205 26.30 T -0.58 6.00 8.00				
542 5T PIPES.1X4.0 PASS 85-4.8.2.2 6.155 205 22.17 -0.43 0.00 0.00				
543 57 F1F43.1X4.0 FA55 B5-4.8.2.2 0.134 105 18.02 - 0.41 0.00 1.70				
584 57 71712355.0 PASS 85-4.7 (C) 0.510 204 285.30 - 1,02 0.68 0.69				
545 5T P1P85.1X4.0 PAGS 85-4.8.2.2 0.128 205 37.15 T -0.05 5.00 1.70				
586 57 FIF49.1X4.0 PASS 85-4.0.2.2 0.151 205 40.77 7 -0.10 0.00 0.00				
587 57 FIP89.124.0 FASS 85-4.8.2.2 0.148 205 38.30 7 -0.14 0.00 0.00				
548 57 PIPH5.124.0 PAS5 85-4.8.2.2 5.145 205 34.147 -0.17 5.80 5.60				
549 ST FIP89.124.0 FAES 85-4.8.2.2 0,127 206 25.55 T -0.39 0.00 1.70				
390 ST PIPHS.124.0 PASS 85-4.8.2.2 0.150 206				
591 57 PIPHD-1X4.0 PAGS 85-4.8.2.2 0.148 206				
592 57 9591385.0 PASS 85-4.7 (C) 0.352 207 396.75 C -0.60 0.80 0.60				
393 ST PIPES.1X4.0 PASS 85-4.8.2.2 0.148 204				
354 57 F1F65.1X4.0 FASS 85-4.8.2.2 0.155 206				
25.41 T -0.50 0.00 0.00				

TAAD Pro for Wing

Status Results Triance Paul         PM-whold speed 32.5 m/s           Art Mar Wittens Bella Dokeming Pad         Mr Paulor 83           Mr Markens Mr Markens Mr Markensen Ma	D			Job No TPL40581	sheet No a 126	Rev R45-FAB
Norm Bels Swinning Pool         Magic Partones         Magic Partones           Dew         Magic Partoneanan Kuantan         Magic Partoneanan Kuantan         Magic Partoneanan Kuantan           Steel Dasign (Track 0) Checks Cont Mu bits Marton Kuantan         Magic Partoneanan Kuantan         Magic Partoneanan Kuantan           Steel Dasign (Track 0) Checks Cont Mu bits Marton Kuantan         Magic Partoneanan Kuantan         Magic Partoneanan Kuantan           Steel Dasign (Track 0) Checks Cont Mu bits Marton Kuantan         Magic Kaster (Control Compared Steel (	$\bigcirc$			Participal entered and	5 m/r	_
Pri TBM         Design (Trace 60)         Pri TBM         Design (Trace 60)         Design (Trace 60) <thdesign (trace<="" th=""><th></th><th>4</th><th></th><th></th><th>o m/s</th><th></th></thdesign>		4			o m/s	
Dime         Magile Perbandenn Kunntan         Par 0328-KSP.Rds-Deg.ad         Dustines 10-Jul-2012 16           Steel Design (Track 0) Checks Cont Aut. Witz MK - 100 KET (MARIS STRUMLED KONF) Mark 1004K 1004K 1004K1 004K15 Mark 100 101 ST FIFELLA PAR MARK STRUMLED KONF 101 ST FIFELLA PAR MARK STATUS 101 ST FIFELLA PAR					Delta Dec.11 Chd	TEM
Steel Design (Track 0) Checks Cont           MAX SWITZ MX - W MTT (WHAT SWIMPHIE HTEN)           MOMM         NAME         MATT (WHAT SWIMPHIE HTEN)           100 ST 1993.04         MATT (WHAT SWIMPHIE HTEN)         Locating           100 ST 1993.04         MATT (WHAT SWIMPHIE HTEN)         Locating           101 ST 1993.04         MATT (WHAT SWIMPHIE HTEN)         Locating             101 ST 1993.04         MATT (	Int Malls Perhandaran Kuanlan					
All SUIT AN - 0         NEEK CONTROLES PRESE           MARK TAK - 0         NEEK CONTROLES PRESE         NEEK CONTROLES PRESE         NEEK CONTROLES PRESE           39 ST F1793-18.4 - 0.33         10 - 0.3, 2         0.33         0.34         0.34         0.34           39 ST F1793-18.4 - 0.33         10 - 0.3, 2         0.35         0.34         0.34         0.34           39 ST F1793-18.4 - 0.33         10 - 0.3, 2         0.34         0.34         0.34         0.34           39 ST F1793-18.4 - 0.33         10 - 0.3, 2         0.31         0.34         0.34         0.34           39 ST F1793-18.4 - 0.34         10 - 0.3, 2         0.31         0.34         0.34         0.34           39 ST F1793-18.4 - 0.34         10 - 0.4, 2         0.34         0.34         0.34         0.34           39 ST F1793-18.4 - 0.34         10 - 0.4, 2         0.34         0.34         0.34         0.34           40 ST F1799-18.4 - 70.37         10 - 0.4, 2         0.34         0.34         0.34         0.34           40 ST F1799-18.4 - 70.37         10 - 0.4, 2         0.34         0.35         0.34         0.34           40 ST F1799-18.4 - 70.37         10 - 0.4, 2         0.34         0.35         0.34         0.34           <				- discontion - new	-bugala 10-01	0-2012 10.43
HORE         HORE <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td></th<>						
99 T F FFFF.34.5         7.4.7         6.33         6.34         7.4.7           99 T F FFFF.34.5         7.4.7         6.3.6         6.34         7.4.7           99 T F FFFF.34.6         7.4.7         6.4.7         7.4.7         7.4.7           99 T F FFFF.34.6         7.4.7         6.4.7         7.4.7         7.4.7           99 T F FFFF.34.6         7.4.7         6.4.7         7.4.7         7.4.7           91 T F FFFF.34.6         7.4.7         6.4.7         7.4.7         8.4.7           91 T F FFFF.34.6         7.4.7         6.4.7         7.4.7         8.4.7           91 T F FFFF.34.7         7.4.7         6.4.7         7.4.8         8.4.7           91 T F FFFF.34.7         7.4.7         7.4.7         8.4.8         8.4.7           91 T F FFFF.34.6         7.4.7         6.4.6         8.4.8         8.4.8           91 T F FFFF.34.6         7.4.7         6.4.6.7         8.4.8         8.4.7	HORER TABLE RESULT/ CP	TTICAL COND/ AATIO	LOCATION			
30         17         18         17         17         18         17         17         18         17         17         18         18         17         17         18         18         17         17         18         18         18         18         18         18         18         18         18         18         18         18         18         18         18<	25.67 T	-0.39 0.1	00 0.00			
10         17         17         17         18<	596 ST PIPES.184.0 PASS 8	5-4.8.2.2 0.13 -0.15 0.1	4 204 00 0.00			
30         97         109	597 ST P1P89.1X4.0 PASS 8 31.92 T	5-4.8.2.2 0.12 -0.12 0.1	3 704			
30         37         70003.06.9         86.4         6.46         6.46           40         57         7003.06.9         86.4         6.46         6.46           40         57         7003.06.9         86.4         6.46         6.46           40         57         7003.06.9         86.4         6.46         6.46           40         57         7003.06.9         86.4         6.47         80.4           40         57         7003.06.9         86.4         6.47         80.4           40         57         7003.06.9         86.4         6.47         80.4           40         57         7003.06.9         86.4         6.47         80.4           40         57         7003.06.9         86.4         6.43         8.46           40.37         7003.06.9         7004.06.2         6.38         8.46         8.7           40.37         7003.06.9         7004.06.2         7004.06         8.7         8.7           40.37         7003.06.9         7004.06.2         8.68         8.7         8.7           40.37         7003.06.9         7004.06.2         8.7         8.7         8.7           40.37	594 ST PIPES.1X4.0 PAIS 8	5-4.8.2.2 0.13	0.0			
40. 37. 2019, 30.4         38.         44-4,3,2         4.47.         39.           40. 37. 2019, 30.4         38.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.31.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.32.           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.32.           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.33.           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33. </td <td></td> <td>5-4.8.2.2 0.130</td> <td>204</td> <td></td> <td></td> <td></td>		5-4.8.2.2 0.130	204			
40. 37. 2019, 30.4         38.         44-4,3,2         4.47.         39.           40. 37. 2019, 30.4         38.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.31.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.32.           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.32.           40. 37. 2019, 30.4         39.         44-4,3,2         4.32.         4.33.           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         44-4,3,2         4.38.         1.3           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33.           40. 37. 2019, 30.4         39.         34-4,3,2         4.38.         1.33. </td <td>400 ST PIP1395.0 PASS 8 293.45 C</td> <td>5-4.7 (C) 0.500 -0.66 0.0</td> <td>00.0</td> <td></td> <td></td> <td></td>	400 ST PIP1395.0 PASS 8 293.45 C	5-4.7 (C) 0.500 -0.66 0.0	00.0			
102 ST 10795-344-6         7.02         6.17         102           103 ST 10795-344-6         7.02         6.17         102           103 ST 10795-344-6         7.02         6.16         27           103 ST 10795-344-6         7.02         6.16         27           104 ST 10795-344-6         7.02         6.16         27           105 ST 10795-344-6         7.02         6.16         27           105 ST 10795-344-6         7.02         6.12         6.12           105 ST 10795-344-7         7.02         6.12         6.12           105 ST 10795-344-7         7.02         6.12         6.12           105 ST 10795-344-7         7.02         6.12         6.16           105 ST 10795-344-7         7.02         6.12         6.16           105 ST 10795-344-7         7.02         6.12         6.16           104 ST 10795-34-7         7.02         6.16         7.02           104 ST 10795-4         7.02         6.12         6.13         7.02           104 ST 10795-6         7.02         6.15         7.02         6.15           104 ST 10795-6         7.02         6.15         7.02         6.15           105 ST 10795-14         8.04	401 ST P1P49.1X4.8 PASS & 20.49 T	5-4.8.2.2 0.147 -0.60 0.5	203			
40         37         17<		s-4.8.2.2 0.176 -0.62 0.0	209			
MIL BY PUPULA.         MAX         M=4-1,2,2         -2,33		-4.8.2.2 0.164 -0.58 0.0	207			
463 57         21993.316.4         328.5         34.53         34.54         3.55           463 57         21994.316.4         742         34.54         3.55         3.55           471 57         21994.316.4         742         3.54         3.55         3.55           481 57         1994.316.4         742         3.54         3.55         3.55           481 57         1994.316.4         742         3.55         3.55         3.55           181 57         1994.316.4         742         5.55         5.55         3.55           181 57         1994.36.4         743         5.45         5.55         5.55           181 57         1994.36.4         743         5.45         5.55         5.55           105 77         1994.36.4         743         74.45         5.55         5.55           104 57         1994.36.4         743         5.45         5.66         5.55           104 57         1994.3         54.64         5.55         5.66         5.66           104 57         1994.36.4         743         54.51         5.66         5.66           104 57         1994.36.4         5.64         5.66         5.66         5.66 <td>604 ST P1P2736.0 PASS B: 330.91 T</td> <td>5-4.8.2.2 0.251 -0.74 0.0</td> <td>202</td> <td></td> <td></td> <td></td>	604 ST P1P2736.0 PASS B: 330.91 T	5-4.8.2.2 0.251 -0.74 0.0	202			
48.47         21993.03.45         84-4.1.2         6.14         16.9           49.37         21.267         6.24         6.30         5.0           49.37         21.947         6.44         5.0         5.0           49.37         21.947         6.44         5.0         5.0           49.37         21.947         6.44         5.0         5.0           49.37         21.947         6.44         5.0         5.0           49.37         21.917         5.44         5.0         5.0           49.37         21.916.04.04.05         3.04         6.45         5.0           49.37         21.916.04.04.05         3.04         6.45         5.00         5.0           49.37         11.916.04.04.05         3.04         6.45         5.00         5.0         5.0           49.37         11.916.04.05         A.14         5.00         5.0         5.0         5.0           49.37         11.917.04.04         A.94         5.0         5.0         5.0         5.0           49.37         11.917.04.04         A.94         5.0         5.0         5.0         5.0           49.37         11.917.04.04         5.0         5.0 <td>605 ST P1P89.1X4.0 PASS 8:</td> <td>5-4.8.2.2 0.009</td> <td>207</td> <td></td> <td></td> <td></td>	605 ST P1P89.1X4.0 PASS 8:	5-4.8.2.2 0.009	207			
417 37 70793.03.6 7033         10-4.7.7.2         6.318         6.30           101 37 70793.03.6 7033         10-4.7.7.2         6.316         107           101 37 70793.03.6 7033         10-4.7.7.2         6.316         107           101 37 70793.03.6 7033         10-4.7.7.2         6.316         107           101 37 70793.04.6 7033         10-4.7.7.2         6.316         107           101 37 70793.04.7 703         10-4.7.7.2         6.316         107           101 37 70793.04.7 703         10-4.7.7.2         6.316         107           101 37 70793.04.7 703         10-4.7.7.2         6.316         103           101 37 70793.04 704         7045         10-4.7.7.2         6.316           101 37 70793.04 704         7045         10-4.7.7.2         6.317           101 37 70793.04 704         7045         10-4.7.7.2         6.317           101 37 70793.04 704         7045         10-4.7.7.2         6.317           101 37 70793.04 704         10-4.7.7.2         6.317         10-3           101 37 70793.04 704         10-4.7.7.2         6.317         10-3           101 37 70793.04 704         10-4.7.7.2         6.318         10-3           101 37 70793.04 704         10-4.7.7.2         6.318 <td></td> <td>-4.1.2.2 0.144</td> <td>205</td> <td></td> <td></td> <td></td>		-4.1.2.2 0.144	205			
401 57 1979-3.13.05         7.03         5.23         5.24         5.26           403 57 1979-3.14.6         7.02         6.23         5.26         5.26           403 57 1979-3.14.6         7.02         6.23         5.26         5.26           415 57 1979-3.14.6         7.02         6.23         5.26         5.26           415 57 1979-3.14.6         7.02         6.23         5.26         5.26           415 57 1979-3.14.6         7.02         6.23         5.26         5.26           413 57 1977-3.16         7.03         7.4-1.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           413 57 1977-3.16         7.03         104-4.2         5.26         5.26           414 57 1978-3.16         104-4.2         5.26         5.26         5.26           414 57 1978-	407 ST P1P#9.1X4.0 PASS 8: 63.01 T	-4.8.2.2 0.219	201			
48) 37 12193-124.5         PAG         16-4.5.2         4.10         17           48) 37 12193-124.5         PAG         16-5.2         4.10         17           48) 37 12193-124.5         PAG         16-5.2         4.10         127           48) 37 12193-124.5         PAG         16-5.2         4.10         127           413 37 12173-124         PAG         16-5.2         4.10         128           413 37 12173-124         PAG         16-4.3         4.50         126           413 37 12173-124         PAG         16-4.3         4.50         126           413 37 12173-124         PAG         16-4.3         127         127           413 37 12173-124         PAG         16-4.3         127         127           413 37 12173-124         PAG         16-4.4         127         13           413 37 12173-124         PAG         16-4.4         127         13           413 37 12173-124         PAG         16-4.4         1.4         14           413 37 12173-124         16-4.4         1.4         1.4         14           414 37 12174         16-4.4         1.4         1.4         1.4           414 37 1218         16-4.4         1.4	408 ST P1P89.184.0 PASS 8: 31.93 T	-4.4.2.2 0.154 -0.38 0.0	207			
46 57         P1095.106.4         PAS         86-14         2.2         4.155         127           411 57         P1075.4.6         PAS         86-14         2.3         4.3         4.5           411 57         P1075.4.6         PAS         86-14         2.3         13         51         61           411 57         P1075.4.6         PAS         86-14         1.3         6.3         1.5           412 57         P1076.1.6.4         PAS         86-14         2.3         1.5         1.5           413 57         P1076.1.6.4         PAS         86-14         2.3         1.5         1.5           413 57         P1076.1.6.4         PAS         86-14         1.5         1.5         1.5           413 57         P1076.1.6.4         PAS         86-14         1.5         1.5         1.5           414 57         P1076.1.6.4         PAS         86-14         1.5         1.5         1.5           51.67         P1076.1.6.6         PAS         86-14         1.5         1.5         1.5           51.67         -5.3         5.45         5.46         5.46         5.45         5.45           51.67         -5.35         5	609 ST P1P89.1X4.0 PASS 35 25.88 T	-4.8.2.2 0.343 -0.48 0.0	207			
01         57         77         74.2         6.23         107           61         57         77         6.24         6.26         6.43           61         57         77         6.24         6.26         6.43           7.7         7.7         6.24         1.02         1.02           613         57         177         6.24         1.02           614         57         177         6.24         1.02           614         57         177         6.44         1.02           614         57         177         1.02         1.02           614         57         177         6.44         1.02           614         57         177         6.44         1.02           614         57         177         6.45         1.02           614         57         177         6.44         1.02           7.47         6.44         1.02         1.02         1.02           615         57         177         6.44         1.02         6.02           614         77         1.04         20         2.02         2.02	410 ST PIP89.1X4.0 PASS 81 24.36 T	-4.8.2.2 0.159 -0.55 0.0	207			
62 FF FFFF0.LK.4         FMA         H-4.1.2.2         6.4.07         10           71.2         7.2.4         7.2.4         7.2.4         1.2           61.2 FF         FFF.LK.6         FAS         B-4.4.2.2         6.10         1.2           61.2 FF         FFF.LK.6         FAS         B-4.4.2.2         6.10         1.2           61.2 FF         FFF.LK.6         FAS         B-4.4.2.2         6.10         1.2           61.4 FF         FFF.HMALEA         FAS         B-4.4.2.2         6.10         1.2           61.4 FF         FFF.HMALEA         FAS         B-4.4.2.2         6.10         1.4           61.5 FF         FFF.HMALEA         FAS         B-4.4.2.2         6.14         2.6         6.4           61.4 FF         FFF.HMALEA         FFF.HMALEA         FFF.HMALEA         FFF.HMALEA         FFF.HMALEA         FFF.HMALEA	411 ST PIP2734.0 PASS 8: 339.34 T	-4.8.2.2 0.252	202			
0.3 27 F7F0-13C-5 PAS 18-(-1,2,2 4,3) 0.3 47 - 4,65 4,64 1,75 14.4 7 - 4,65 4,64 1,75 14.4 7 - 4,64 4,75 18,56 4.4 7 - 4,64 4,75 8,56 15.5 7 F7F9-33C-5 PAS 18-(-1,2,2 4,1) 15.5 7 F7F9-35C-5 F7F9-35C-5 F7F9-5	612 ST PIPe9.1X4.0 PASS 85	-0.71 0.0	267			
G4 57         F1799-134.4         PASS         85-4,8,2,2         6,136         261           G5 57         F1999-134.4         PASS         85-4,8,2,2         6,136         277           G5 57         F1999-134.4         PASS         85-4,8,2,2         6,156         287           G5 57         F1999-134.4         PASS         85-4,8,2,2         6,156         287           G6 57         F1999-134.4         PASS         85-4,8,2,2         5,164         287           G6 57         F1999-134.4         PASS         85-4,8,2,2         5,164         287           G6 57         F1999-134.4         PASS         85-4,8,2,2         5,164         287	413 ST PJP89.1X4.0 PASS 85 61.54 T	-4.8.2.2 0.218	201			
65 97 9799.30.4 985 85-4.5.2 6.365 977 3.67	414 ST PIPES.1X4.0 PASS 85	-4.8.2.2 0.194	203			
616 57 P1P49.1X4.0 PASS 85-4.8.2.2 8.348 207 25.71 7 -0.48 8.00 0.00		-4.9.2.2 0.154 -0.38 0.0	207			
	614 57 P1P49.1X4.0 PASS 85 25.71 T	-4.1.2.2 0.140	207			
	614 57 91949,1X4.0 9A55 85 22.71 T					

Job Tills W ....

Client Ma ----..... .....



3	Job No TPL40581 a 123 R4b-FAI					
Software Deensed to Transerve Pta Ltd	Partwind speed 32.	5 m/s				
Wisma Belia Swimming Pool	Ref Fabric R5					
	By TSM	Dale17-Dec-11 Ch	TSM			
Majlis Perbandaran Kuantan	File Q326-KSP-R4b	Deg.std OsleTime 10-	Jul-2012 16:43			

ALL UNITS	NR - XN	HETE IUNLE	SS OTHERMISE NOTED!		
HEHBER	733LE	NESULT/	CRITICAL COND/	AATIO/ HZ	LOADING LOCATIO
529 5	T P1P2736.0	PASS 470.40 T	13-4.1.2.2 -65.04	0.893	202
538 5	7 9192736.0	PASS 478.29 T	65-4.8.2.2 -30.67	0.608 0.00	202
531 5	7 9192736.0	PASS	15-4.1.2.2	0.412	202
	T P1P2736.0	483.45 T	-30.87	0.00	202
	·····	486.67 1	-44.01	0.902	202
533 5	T P1P2736.0	PASS 572.11 T	85-4.8.2.2 -51.36	0.450	202
534 5	F P1P2736.0	PASS 575.26 T	85-4.4.2.2 -16.82	0.559	202
535 5	F #1#2736.0	PASS 580.98 T	85-4.8.2.2 -13.10	0.531	202
536 53	P1P2736.0	FASS	85-4.8.2.2	0.529	202
	P1P2736.0	515.43 T	-12.47	0.00	1.5
		303.32 T	-15.44	0.00	0.0
538 51	*****	0 PASS 18.76 T	85-4.8.2.2 -1.88	0.300	202
535 51	P1993.1X4	0 PASS 40.95 T	85-4.8.2.2 -0.90	0.252 0.00	206
540 57	PIPP9.1X4	0 FASS 56.72 T	85-4.8.2.2 -1.74	0.411	205
541 57	P1P09.184		85-4.8.2.2 -3.93	D.544 0.00	206
542 57	P1P89.1X4.		M-4.4.2.2	0.505	205
		13.69 1	-3.69	0.00	0.00
540 57	PIP1395.0	PASS 19.37 T	85-4.8.2.2 -12.00	0.514	205
544 ST	P1P19.1X4.	0 PASS 20.21 T	85-4.1.2.2 -2.68	0.405 0.00	207
545 ST	P3789.3X4.	0 PASS 20.53 T	85-4.8.2.2 -3.32	0.486	267
546 ST	P1P#9.1X4.	0 PASS 18.02 T	85-4.8.2.2 -3.25	0.470	207
547 ST	P3P1395.0	PASS 255.14 C	ANNEX 1.1 -6.87	0.541	204
548 ST	P1009.1X4.	0 FASS	85-4.8.2.2	0.385	206
545 57	PIPER. 184.	14.01 T	-2.46	0.00	206
	*****	17.10 T	-2.33	8.60	1.70
550 ST	P1P89.184.	PASS 15.42 T	85-4.8.2.2 -1.73	0.270	205

STAAD Pro for Windows 20 07 02 15

Idal Due 25 al 1

8	Job Ne TPL40581 Sheet Ne a 127 R4					
Software licensed to Transerve Pie Ltd	Parlwind speed 32	.5 m/s				
Jee Tille Wisma Bella Swimming Pool	Ref Fabric R5					
	By TSM	Dale17-Dec-11 C	M TSM			
Clini Mails Perhandaran Kuantan	File 0326-KSP-R4	h Des rid Deleffine so	- bil 2012 16:42			

	ARE - ION	HETE IUNLE	SS OTHERMISE NOTED	1. C	
HEHREA	TABLE	MESULT/	CATTICAL COND/	MATIO/	LOADING
617 3	F P1P09.1	26.26 T	85-4.8.2.2	0.158	207
£18 S	* *****	26.17 T	85-4.0.2.2	0.162	207
619 5	F 91999.1	X4.0 PA33	85-4.1.2.2	0.147	207
•17 5		20.46 T	-0.61	0.60	1.1
620 5	P1789.1	14.0 PASS	85-4.1.2.2	0.133	207
		17.25 7	-0.59	0.60	8.6
621 57	*171395.	0 PASS	85-4.7 (C)	0.507	204
		282.93 C	-0.41	0.00	0.0
622 ST		X4.0 PASS	85-4.4.2.2	0.141	205
		37.42 7	-0.10	0.00	1.7
623 51		X4.0 PASS	85-4.4.2.2	0.149	205
		40.39 T	-0.07	0.00	1.1
624 51	PIPES.1		85-4.8.2.2	0.141	205
		38.35 7	-0.08	0.00	0.0
625 53	* *1***.1		85-4.8.2.2	0.134	285
		36.34 7	-0.08	0.60	8.0
626 53	PIP49.1	K4.0 PASS	85-4.1.2.2	0,120	205
		24.21 7	-0.30	0.00	1.7
627 57	P1969.1	14.0 PASS	85-4.8.2.2	0.133	205
		20.66 7	-0,49	0.00	0.0
620 ST	P1P49.1		85-4.8.2.2	0.136	206
		24.27. T	-0.42	0.00	1.7
629 57		PASS	85-4.7 (0)	0.331	207
		184.55 C	-0.66	0.00	0.0
630 ST	P1989.31		85-4.4.2.2	0.134	205
		24.08 7	-0,43	0.00	1.7
631 ST	P1999.11		85-4.8.2.2	0.138	205
		25.55 T	-0.41	0.00	
632 57	P1789.13	4.0 1355	85-4.8.2.2	0.125	206
		25.39 7	-0.31	0.00	6.6
633 ST	P1289.13		85-4.8.2.2	0.120	204
		33.10 T	-0.06	0.00	0.0
624 57	P1289.13	4.0 PASS	85-4.8.2.2	0.114	:
		31.50 T	-0.05	0.00	0.0
635 57	P1PP9.13	4.0 2455	85-4.8.2.2	0.125	204
		36.06 T	-0.05	0.00	0.0
636 57	P1P49.13	4.0 PASS	85-4.4.2.2	0.137	204
		38.14 7	-0.05	0.00	0.0
637 ST	P1P1395.0	PASS	85-4.7 (0)	0.497	205
		277.40 C	-0.12	4.00	5.0
	P1245.13	4.0 PASS	85-4.9.2.2	0.149	207

Print Time/Dale: 11/07/2012 17:2



0			Job No TPL40581	Sheel No.	a 128	Rav R4b-FAB
Solware licensed in Transerve Pie Lid			Partwind speed 32.5	m/s		
The Wisma Bella Swimming Pool			Ref Fabric R5			
			BY TSM	Dale17-D	ec-11 Chd T	SM
ent Mallis Perbandaran Kuantan			FM Q326-KSP-R4b	-Deg.std	Detertime 10-Jul-	2012 15:43
Steel Design (Track 0) Checks Cont						
HEMBER TABLE RESULT/ CRITICAL COND/ R	NT10/	LOADING/				
435 ST 72785.124.0 7A55 85-4.8.2.2 25.17 7 -0.63	0.164	207				
640 57 P1203.1X4.0 PASS 85-4.0.2.2 27.63 7 -0.55	0.168	207				
641 ST P1P2736.5 PASS BS-4.8.2.2 335.48 T -0.75	0.249	202 0.57				
	0.00	207				
643 ST P1P89.124.0 PASS 85-4.8.2.2	0.152	203				
	0.264	201 0.00				
	0.160	207				
	0.151 0.00	207 0.00				
	0.163	207				
548 ST PIP2736.0 PASS 85-4.8.2.2	0.255	202				
649 ST P1P89.3X4.0 PASS 85-4.8.2.2 0 17.34 T -0.20	0.00	209				
	0.00	201				
451 ST PIP49.1X4.0 PASS 85-4.8.2.2 0 46.62 T -0.16	.178 6.00	207				
	.153 6.00	207				
	.146 0.00	207				
654 ST FIFES.1X4.0 PASS 85-4.8.2.2 5	0.157	267				
455 ST P1P89.1X4.0 PAIS 85-4.8.2.2 0 25.86 T -0.60	.163	207				
456 ST P1P09,1X4.0 PASS 85-4.8.2.2 6	.153	207				
657 57 P1P89,1X4.0 PAS5 85-4.8.2.2 8 17.60 7 -0.61	.137	207				
454 ST P2P1395.0 PASS 85-4.7 IC1 0	.508	204				
459 ST P1P89.1X4.0 PASS 85-4.8.2.2 0	-130 0.00	205 0.00				
660 ST PIPES,184.0 PASS 85-4.8.2.2 0	.147	205				

CTAND Des for Mile

-----

			Job No TPL40581	Sheel No	a 132	Rev R4b-FAB
5			Parlwind speed 32.5	m/s		
The Wisma Bella Swimming Pool			Rel Fabric R5	nva -		
en lander anderskingen men die steren in			By TSM	Dele17-D	tc-11 Chd	TSM
Majlis Perbandaran Kuantan			File Q326-KSP-R4b		Deletime 10-Ju	
Steel Design (Track 0) Checks Cont						
ALL UNITS ANE - NH HETE UNLESS OTHERNISE NOTED						
MEMBER TABLE MESULT/ CRITICAL COMD/ TX HY	NIT NI	LOADING/				
727 57 #1##9.1X4.0 #A55 85-4.8.2.2 12.77 T -2.78	0.510	200				
728 ST P2P1395.0 PASS B5-4.4.2.2 19.13 T -12.01	0.514	208				
729 ST PIP89.1X4.0 PASS 85-4.8.2.7 20.35 T -2.67	0.405	203				
730 ST P1P49.1X4.0 PASS 85-4.8.2.2 20.44 T -3.29	0.483	205				
731 ST F1P49.1X4.0 PASS 85-4.8.2.2 18.06 T -3.23	0.466 9.00	205 1.70				
732 ST P1P1395.0 PASS ANNEX 1.1 259.61 C -6.84	0.543 2.32	204				
733 ST FIP49.1X4.0 PASS B3-4.8.2.2 14.86 T -2.68	0.387 0.60	208				
734 ST PJP85.1X4.0 PA35 B5-4.8.2.2 17.16 T -2.35	0.352 0.00	200				
725 ST P1789.1X4.0 PASS 85-4.8.2.2 15.47 T -1.75	0.272	208				
736 57 9191355.0 PASS B5-4.8.2.2 41.01 T -5.56	0.293 8.00	254 0.00				
737 ST PIP49.1X4.0 PASS 85-4.4.2.2 27.77 7 -2.15	0.364 0.00	205				
730 ST PIPAS.1X4.0 PASS 85-4.8.2.2 22.64 T -2.34	0.371 0.00	205				
735 ST PIP89.1X4.0 PASS 85-4.4.2.2 12.06 T -2.05	0.303 0.00	205				
	0.423 5.34	203				
741 57 PIP49.1X4.0 PASS 83-4.8.2.2 11.45 7 -1.62	0.242 0.00	264 0.00				
742 ST P1P49.1X4.0 PASS B5-4.8.2.2 22.20 T -2.46	0.384	204 6.00				
743 ST P1785.1X4.8 PASS 85-4.8.2.2 24.64 T -2.57	0.413 0.00	204				
744 ST P1P1395.0 PASS 85-4.8.2.2 23.60 T -4.77	0.312	204				
745 ST P1209.1X4.0 PA35 85-4.8.2.2 12.62 T -1.81	0.243	205				
746 ST P1P89.1X4.0 PASS 85-4.8.2.2 15.71 7 -2.10	0.316	205				
747 ST #2##9.1X4.0 MAS 85-4.8.2.2 15.02 T -2.30	0.340	208				
748 57 929395.0 PASS ANNEX 1.1 358.54 C -6.72	0.613 6.03	209				

$\mathcal{D}$				Job No TPL40581	Sheet No	a 129	Rev R4b-FAB2
$\supset$				Partwind speed 32	5 m/s		
Software licensed to Tran 8 Title Wisma Bella Swimming				Ref Fabric R5			
				By TSM	Dale 17-D	lec-11 Che TS	SM
ent Majils Perbandaran Kua	intan			Fle Q326-KSP-R4			
Steel Design (Track	0) Checks Cont						
ALL UNITS ARE - KN HETE	INNLESS OTHERWISE NOTE	D)					
HEHBER TABLE RE	SULT/ CRITICAL COND/	NATIO/	LOADING/				
********							<i>X</i> .
661 ST P1989.1X4.0	PASS 85-4.8.2.2 .37 T -0.07	0.140 0.00	205				
642 ST P3P89.3X4.0	PASS BS-4.8.2.2	0.133	205				
36	.24 7 -0.08	0.00	1.70				
643 ST PIPES.1X4.0	PASS 85-4.8.2.2	0.125	208				
464 ST P3P85.124.0 1	7A55 85-4.8.2.2 .23 7 -0.43	0.143	208				
665 ST PIPES.124.0	PASS 85-4.8.2.2	0.140	208				
24.	.62 T -0.45	0.00	0.00				
666 ST P191395.0 184	PASS 85-4.7 (C)	0.330	205				
		0.00	0.00				
667 ST P1789.1X4.0 1	ASS 85-4.8.2.2	0.135	208				
		0.141	209				
448 ST P2P89.3X4.0 1 25.	ASS BS-4.8.2.2 .82 T -0.42	0.00	1.70				
449 ST P1P49.384.0 1	135 15-4.8.2.2	0.127	208				
25.	.56 7 -0.32	0.00	1.70				
670 ST #1849.1x4.0 1	-0.07	0.123	204				
	1455 15-4.4.2.2	0.115	204				
671 ST P1P89.3x4.0 31.	#1 T -0.04	0.00	1.42				
672 ST P1989.1X4.0 1	ASS 85-4.8.2.2	0.135	204				
	.65 7 -0.85	0.60	0.99				
673 ST P1P89.1X4.0 P		0.135	204				
		0.457	205				
674 ST F1F1395.0 F	ASS 85-4.7 (C) 49 C -0.28		0.00				
475 ST P2P89.1X4.0 #		0.150	207				
21.	27 7 -0.62	0.00	1.70				
676 ST PIP49.1X4.0 P	ASS 85-4.8.2.2 32 T -0.64	0.173	207				
		0.169	207				
677 ST PIPS.184.0 P 27.		0.00	0.00				
678 ST P1P2736.0 P 339.	ASS 85-4.8.2.2	0.252	202				
	46 T -0.75	0.00	0.42				
679 ST P1P89.1X4.0 P		0.005	207				
	••••••						
600 ST P1P09.1X4.0 P 36.	ASS 85-4.8.2.2 54 T -0.14	0.142	207				
441 ST PIPEP.1X4.0 P	835 85-4.4.2.2	0.774	201				
		0.00	0.00				
442 ST P1P89.1X4.0 P		0.157	207				
Time/Date: 11/07/2012 17:29		STAAD Pro f	or Windows 20.	07.02.15		Pr	fint Run 31 of 10

2				TPL40581	a 133	Rev R4b-FAB
Software licensed to Transe	rve Pis Lid			Partwind speed 32.5	5 m/s	
Tite Wisma Belia Swimming P				Ref Fabric R5		
				BY TSM	Dale17-Dec-11 Ch	TSM
Majilis Perbandaran Kuant	an			Fie Q326-KSP-R4b	-Deg.std Date/Time 10-	Jul-2012 16:43
	UNLESS OTHERWISE MOTER LT/ CRITICAL COND/	MATIO/	LONDING/			
x	лт	82	LOCATION			
745 57 92989.334.0 PA	55 65-4.4.2.2 6 7 -3.52	0.507	205			
750 ST PIP09.124.0 PA	55 BS-4.8.2.2 2 T -3.35	0.437 0.00	209			
751 ST #12#89.184.0 PA 16.9	9 7 -2.89	0.420 0.00	208			
752 ST P1P2734.0 PA	55 85-4.8.2.2 2 7 -15.15	0.347 0.00	202			
753 ST 92989.1X4.6 PA	55 B5-4.8.2.2 FT -1.84	0.294 0.00	202			
754 57 PIP49.1X4.0 PA	55 85-4.8.2.2	0.245 0.00	208 1.70			
755 ST #1#89.184.0 PA	T -1.80	0.415	204 1.70			
756 ST PJP89.1X4.0 PA	15 85-4.4.2.2 1 7 -4.62	0.555 0.00	208			
757 ST PIP49.124.0 PA	S 85-4.8.2.2	0.523	208			
758 ST P2P1395.0 PA	15 15-4.4.7.2	0.545	209			
759 ST P1P1398.0 PA	15 ANHER 1.1 C -1.55	0.776 20.05	204			
740 ST P1P1398.0 PA: 14.5	5 85-4.4.2.2 7 -20.74	0.559	206			
761 ST P1P1398.0 PA1 30.34	C -1.66	0.775 27.91	206			
762 ST P1P1398.0 PA	15 15-4.4.2.2	0.559	206 0.00			
763 ST P1P1398.0 PA	15 83-4.8.2.2 1 T -1.15	0.245	207 0.85			
744 ST P1P1398.0 PAG 29.47	15 15-4.4.2.2	0.235	203			
765 ST P1P1358.0 PA3 25.41	T -7.85	0.234 0.00	207 0,85			
766 ST P1P1398.0 PA	5 35-4.1.2.2	0.227 0.00	207			
767 ST P3P3398.0 PA3 30.00	T -8.42	0.253	207			
766 ST PIP1330.0 PA3 30.22	5 85-4.8.2.2 7 -7.95	0.243 0.00	205			
769 ST P3P1398.0 PA	IS 85-4.8.2.2	0.251	209 0.85			
170 ST PIPI398.0 PA		0.254 0.00	207			

STAAD Pro for Windows 20.07.02.15

Comparison in the second to Transver Part Let      Comparison in the second to Transver Part Let      Comparison in the second term of	P#*wind speed 32.5 Ref Fashic R5 P* 155M P*8 Q326-KSP-R4b	Dalk17-Dec-11	<sup>4</sup> TSM Jul-2012 16:43	
196         Wilsons Befla Swimming Pool           Millions Befla Swimming Pool           Millions Befla Swimming Pool           State Design (Track 0) Checks Conf ALL WITS MA - No Hert (INLESS INTRODUCT WITS' Loggithy	Ref Fabric R5 By TSM	Dalk17-Dec-11		
Steel Design (Track 8) Checks Cont ALL NOTS NA - NN KET (INLESS FIREWILL ROTED)           ROTE: NAME OF THE INLESS FIREWILL ROTED ROTE: NAME OF THE INLESS FIREWILL ROTED ROTE				
Steel Design (Track 0) Checks Cont           AL NYES XX - NN WHE (NALES STEMPLIE SPEED)           BORGEN TAKES (NALES)           Steel Design (Track 0) Checks Cont           AL NYES XX - NN WHE (NALES)           Steel Design (Track 0) Checks Cont           AL NYES XX - NN WYES           Steel Design (Track 0) Checks Cont           AL NYES XX - NN WYES XX - NN WYES           Steel Design (Track 0) Checks Cont           AL NYES XX - NN WYES XX - NN WYES           AL TY XX - Steel AL 21           AL TY XX - STEE AL 21           AL TY XXX - STEE AL 21 <td colspan<="" th=""><th>174 0326KSP-R45</th><th></th><th>Jul-2012 16:43</th></td>	<th>174 0326KSP-R45</th> <th></th> <th>Jul-2012 16:43</th>	174 0326KSP-R45		Jul-2012 16:43
Steel Design (Track 0) Checks Cont           All WITS M4 - NN         HET (MALES WIENDIE WITS)           WEIGE         HAND         K         K         K         Longity           42.3 T F1993.214.0 JSM         JSM         K         K         Longity         K           44.3 T F1993.214.0 JSM         JSM         K         Longity         K         Longity         K           44.3 T F1993.214.0 JSM         JSM         K         L <thl< th=""> <thl< th="">         L</thl<></thl<>				
31,71 7         -6.33         6.66         6.69           69 57 F719-5,26,5 Deg 10         6.64         5.63         6.66         5.64         5.66           10,51 7         6.05         7.65         6.66         5.66         5.66         5.66           10,51 7         7.65         7.65         5.66         5.66         5.66         5.66           10,57 7         7.63         5.64         5.66         5.66         5.66         5.66           10,57 7         7.63         5.64         5.66         5.66         5.66         5.66         5.66         5.66				
42 57 72793, IK.6 201 19-4, 12, 2 5, 15 27 -6, 2 1, 55				
694         57         97999.3X4.0         PASS         81-4.1.2.2         6.142         201				
285.34 C -2,18 0.00 0.00 (55 ST 12195.1X4.0 PASS 85-4.8.2.2 0.137 285 37.19 T -0.08 0.00 0.00				
697 57 FIM45.1X4.0 FASS 85-4.4.2.2 0.130 205 60.77 7 -0.69 0.00 1.70				
638 57 92993.124.0 PA35 85-4.8.2.2 8.147 285 34.35 7 -0.14 0.06 1.70 				
36.16 T         -0.17         0.00         1.10           766 ST F1P49.1X4.0 PASS         85-4.8.2.2         0.135         200           25.35 T         -0.41         0.00         0.00				
701 ST P1293.124.0 PASS B5-4.8.2.2 0.154 208 25.07 T -0.52 0.06 1.70				
702 ST P1995.124.0 PASS 85-4.8.2.2 0.152 208 24.82 T -0.54 0.00 0.00 703 ST P191355.0 PASS 85-4.7 (C) 0.351 209				
194.08 C -4.78 0.60 0.00				
24.65 T -0.33 0.00 0.00				

B

Print Run 35 of 104

TAN SIEW MOI

	2					Job No TPL40581	Sheel No.	a 134	Rev R4b-FAB2		Z	
-	Software license	d to Transerve F	Pie Lid			Partwind speed 32.	5 m/s		_		-	Software Ecenaed to
Job Yis	• Wisma Bella Swi					Ref Fabric R5					lob Title W	lisma Bella Swimm
						BY TSM	Dele17-D		TSM		Client N.	ajiis Perbandaran I
Chem	Majlis Perbandara	in Kuantan				File Q325-KSP-R4	-Deg.std	Deterime 10-Ju	1-2012 16:43	F	101	
	teel Design (T		hecks Cont								ALL I	al Design (Tra
	SHARE ADDRESS	ALSULT/	CRITICAL COND/	NATIO/	LOADING/						HIDIBI	
	771 ST 9191398.	PA55 29.49 T	85-4.8.2.2 -0.19	0.247	267 0.85						1	793 ST 9392196.0
0	772 57 \$1\$1394.		85-4.8.2.2 -7.91	0.239 0.00	209							794 ST PIP2196.0
	773 ST P191398.	PASS 34,24 T	85-4.4.2.2 -9.13	0.250 0.00	209							795 ST PIP2196.0
	774 ST P1P1394.	PASS 24.26 T	85-4.8.2.2 -8.43	0.254 0.00	207							794 ST 9392196.0
	775 ST PIPI398.	29.42 T	65-4.0.2.2 -0.01	0.242	207							197 ST 9192196.0
	776 ST PIP1398.0	29.36 T	85-4.8,2.2 -7.83	0.237 0.00	269							996 ST PIP2196.0
	777 ST PIPI398.0		#5-4.4.2.2 -7.63	0.232 0.00	207							99 ST PIP2196.0
	778 ST PIP1398.0	PASS 29.45 T	85-4.8.2.2 -7.55	0.230 0.00	209							000 ST PIP2196.0
	778 ST PIPI398.0	PASS 33.54 C	AMMEX I.1 -1.61	0.788 28.43	208							101 ST P1P2196.0
	760 ST PIP1398.0	15.07 T	N3-4.8.2.2 -21.12	0.549 0.00	208 0.00							02 ST PIP2196.0
	701 ST P2P1390.0	7N33 31.28 C	AMEX 1.1 -1.71	0.787 28.30	200							03 ST PIP2196.0
	742 ST P1P1398.0	PA15 15.25 T	85-4.1.2.2 -21.12	0.543 0.00	208							04 ST P1P2196.0
	743 57 9392196.0	PA35 111.46 T	85-4.8.2.2 -1.87	0.126 0.00	201 2.13							05 ST P1P2196.0
	784 ST P1P2196.0	46.06 C	ANNER 1.1 -4.68	0.333 20.62	205							06 ST 9392196.0
1	785 ST P1P2194.0	PASS 32.42 T	85-4.8.2.2 -20.55	0.303	205 8,00							07 ST PIP2196.0
	786 ST P1P2196.0		85-4.7 (C) -2.06	0.174	\$.00							68 ST PIP2196.0
	747 ST P1P2196.0		85-4.7 (C) -0.80	0.268	204 0.00							89 ST PIP2194.0
	788 ST P192156.0		85-4.7 (C) -2.41	0.363	204 0.00							30 ST PIP2196.0
	749 57 9192196.0	PASS 451.84 C	85-4.7 (C) -2.66	0.438	204							11 ST PIP2196.0
_	796 ST PIP2196.0		85-4.7 (C) -2.75	0.456	204							12 57 9192196.0
	791 ST 9192196.0		85-4.8.2.2 -7.13	0.544 0.00	205							13 ST PIP2194.0
	192 ST P1P2196.0	TASS	85-4.8.2.2 -4.92	0.653	205							14 ST PIP2196.0

Print Ten + Prais: 11/07/2012 17:2

STAAD Pro for Windows 20.07.02.15



Print Time/Dale: 11/07/2012 17:29

Print Run 36 of 104

2						Jeb No TPL40581	Sheat No	a 131	Rev R4b-FAB
◯.	tware licensed	o Transarva P	le Lid			Partwind speed 32	5 m/s		
Job Tille Wisma	Bella Swim	ming Pool				Ref Fabric R5			
						BY TSM	Date 17-D	ec-11	Chd TSM
Clani Mailis I	Perbandaran	Kuantan	1			F# Q326-KSP-R4	b-Deg.std	Date/Time 1	0-Jul-2012 16:43
	TABLE T PIPES.3X	25.80 T	CRITICAL CORD/ HT BS-4.9.2.2 -0.51	9.152 0.00	LOADTING/ LOCATION 208 1.70				
706 5	T PIP09.1X	.0 PASS 25.67 T	85-4.1.2.2 -0.40	0.130	1,70				
707 S	T PIP89.1X	.0 PASS 33.75 T	85-4.1.2.2 -0.16	0.135	204 1.70				
	T P1P89.1X	31.91 T	85-4.8.2.2 -0.12	0.124	264				

708 57	P1P89.1X4.0 PASS 31.82 T	85-4.8.2.2 -0.12	0.124 0.00	264
705 ST	PIP49.184.0 PASS 37.75 T	85-4.8.2.2	0.136	204
- 11 C	37.75 1	-0.68	0.00	1.7
718 ST	P1P09.1X4.0 PASS 37.78 7	83-4.8.2.2	0.136	204
	37.76 7	-0,04	0.00	1.2
711 ST	P191395.0 PASS	85-4.7 (C) -0.98	0.508	205
	283.63 C	-0.78	0.00	0.0
712 57	P1P09.1X4.0 PASS 20.89 T	83-4.8.2.2	0.151 0.00	1.7
			0.175	
713 ST	PIP45.114.0 PASS	85-4.8.2.2	0.175	207
	· 17.03 T	-0.45	*. **	
714 37	P3P45.3X4.0 PASS 27.25 T	85-4.0.2.2	0.170	207
	27.25 1			
715 ST	P1P2736.0 PASS	85-4.8.2.2	0.252	202
316 ST	P1249.1X4.0 PASS	-0.25	0.099	1.7
	17.01 T	-0.25		
717 ST	P1789.1X4.0 PASS 37.19 T	83-4.4.2.2	0.345	245
	27.13 1			
718 57	PIP49.3X4.0 PASS 63.02 T	13-1.1.2.2	0.219	0.0
	63.02 T			
715 ST	PIP45.1X4.0 PASS 31.93 T	15-4.0.2.2	0.157	0.0
720 ST	P1P49.1X4.0 PASS 25.84 T	83-4.8.2.2	0.150	207
721 57	PIP49.184.0 PASS 26.56 T	*0.57	0.00	0.0
722 ST	PIP2736.0 PASS 301.34 T	-15.16	0.00	0.0
***				
723 ST	PIPSS.1X4.0 PASS 18.50 T	a) #7	0.00	0.0
724 55	PIP49.1X4.0 PASS 40.57 T	-0.89	0.00	1.7
725 ST	P1P49.114.0 PASS 56.69 T	83-4.0.2.2	0.410	205
726 ST	P1P89.1X4.0 PASS 15.05 T	13-4.8.2.2		1.7
		-3.93		

 $\mathcal{B}$ 

STAAD.Pro for Windows 20.07.02.15

	Jab No TPL4058	1 Sheel No	a 135	Rev R4b-FA
lansone Pie Lid	Partwind speed	32.5 m/s		
ng Pool	Ref Fabric R5			
	By TSM	Dele17-D		TSM
uantan	File Q326-KSP-	R4b-Deg.std	Date/Time 10-J	ul-2012 16:43
k 0) Checks Cont				
PASS 85-4.8.2.2 0.546 06.93 T -4.49 0.00	205 0.00			
PASS 85-4.7 (C) 0.529 75.46 C -3.72 0.00	204 0.09			
PASS 85-4.7 (C) 0.525 71.55 C -3.35 0.00	204 0.60			
PASS 85-4.7 (C) 0.501 (5.40 C -3.93 0.00	204 0.00			
PASS 85-4.7 (C) 0.426 (3.40 C -3.80 0.80	204 0.00			
PASS 85-4.7 [C] 0.369 12.04 C -2.36 0.00	201 0.00			
FASS 85-4.7 (C) 0.372 15.10 C -2.72 0.00	281 0.00			
PASS 85-4.7 (C) 0.356 7.69 C -1.59 0.00	201			
PASS 85-4.7 (C) 0.375 2.20 C -2.65 8.00	201			
PAGS 85-4.7 (C) 0.383 6.37 C -2.28 0.60	201 1.84			
7A55 85-4.7 (C) 0.425 7.53 C -3.70 0.00	205			
PASS 85-4.7 (C) 0.512 7.48 C -3.57 0.00	205			
	205			
PASS 85-4.7 (C) 0.540 7.28 C -3.75 0.00	205			
	204			
	204			
	204			
	204			
	205			
	205 1.84			
	205			
PASS 85-4.7 (C) 0.175 0.30 C -1.58 0.60	2.00			

STAAD.Pro for Windows 20.07.02.15

that Run 37 of 15

Print Run 33 of 19



2		TPL40581	Sheel No	a 136	R4b-FAB
Software Reensed to Transerve Pie Ltd		Partwind speed 32.	5 m/s		
eb Tile Wisma Belia Swimming Pool		Ref Fabric R5			
		By TSM	Calt 17-D	ec-11 Chd T	SM
Mallis Perbandaran Kuantan		Fle Q325-KSP-R4			
Steel Design (Track 0) Checks Cont					
ALL UNITS ARE - IN HETE (UNLESS OTHERWISE NOTED)					
HIDHER TABLE RESULT/ CRITICAL COND/ BATIO/ IX HT HT HI	LOADING/				
415 ST F2F2156.0 FASS 85-4.4.2.2 8.308 29.36 T -21.15 0.00	204				
416 ST P1P2196.0 PASS NOMEX 1.1 0.335	204				
(9.34 C -4.11 20.45					
\$17 57 \$2\$2196.0 \$355 \$5-4.8.2.2 0.122 106.83 7 -1.89 0.00	201				
106.83 7 -1.89 0.00	0.00				
418 ST PIP2196.0 PASS 85-4.7 (C) 0.116 125.09 C -0.61 0.00					
819 ST F3F2156.0 FASS 85-4.7 (C) 0.186 203.14 C -0.13 0.00	s 0.00				
\$20 57 FIP2156.0 PASS \$1-4.8.2.2 0.205	207				
50.73 T -5.24 0.00	0.00				
421 ST PIP2196.0 PASS 85-4.7 (C) 0.185	204				
	0.00				
822 57 9292196.0 PASS 85-4.7 (C) 0.316 344.39 C -0.47 0.00	204				
423 ST 9292196.0 PASS 85-4.7 [C] 0.434 472.53 C -1.76 0.00	204 0.00				
824 57 P1P2196.0 PASS 85-4.7 (C) 0.535	204				
583.31 C -2.86 0.00	0.00				
825 37 9192196.0 9455 85-4.7 (C) 0.423 477.86 C -2.83 8.00	204				
	********				
424 ST P1P2136.0 PASS B5-4.7 (C) 0.674 733.23 C4.18 0.00	0.00				
127 ST PIP2186.0 PASS 85-4.7 IC1 0.702	204				
827 ST PIP2196.0 PASS 85-4.7 [C] 0.702 744.43 C -5.46 0.00	0.00				
828 ST P1P2196.6 PASS 85-4.7 (C) 0.478 737.01 C -4.22 0.00	204				
	0.05				
429 37 PIP2194.0 PASS 85-4.7 (C) 0.632 687.38 C -4.36 0.00	204 0.00				
623.00 C -3.94 0.00	204 0.00				
431 57 F1F2194.0 FASS 85-4.7 (C) 6.499 542.77 C -3.63 0.60	204				
542.77 C -3.43 0.00	0.00				
#32 ST P1P2196.0 PASS B5-4.7 (C) 8.432 447.92 C -3.18 8.60	204				
033 ST F1F2196.0 PASS 85-4.7 (C) 0.331 359.85 C -1.41 0.00	201 0.00				
#34 5T P2P2196.0 PASS #5-4.7 (C) 0.257	201				
388.61 C -1.64 0.00	0.00				
#35 ST PIP2196.0 PASS 85-4.7 (C) 0.372 405.10 C -2.15 0.00	201 0.00				
434 ST PIP1154.0 PRSS B5-4.7 [C] '0.372 404.50 C -1.85 0.00	201				

STAAD.Pro for Windows 20.07.02.15

0				Job No TPL40581	Sheet No	a 137	Rev R4b-FAB2
•				Partwind speed 32.5	m/s		
to Tale Wisma Belia Swimming Pool				Ral Fabric 85			
				By TSM	Dale 17-D		TSM
Test Matter B. A. A. Market							
Ilent Majils Perbandaran Kuantan				File Q325-KSP-R4b	Deg.sld	Landrome 10-	ul-2012 16:43
Steel Design (Track 0) C							
ALL UNITS ARE - IN HETE (UNL)							
TX I	CRITICAL COND/	RATIO/	LOCATION				
637 ST P1P2196.0 PASS 390.84 C	85-4.7 (C) -3.69	0.359	201				
			205				
#38 ST PIP2196.0 PA35 439.16 C	85-4.7 (C) -3.20	0.403	1.84				
	85-4.7 (C)	0.507	205				
435 57 9282194.0 PASS 551.44 C	-4.04	0.00	1.84				
840 ST P1P2196.0 PASS	85-4.7 (C)	0.595	205				
647.01 C	-4.43	0.00	1.84				
441 57 PIP2194.0 PASS 705.55 C	85-4.7 (C)	0.648	205				
	-4.35	0.00	1.84				
842 ST P1P2156.0 PASS 738.33 C	85-4.7 (C) -4.01	0.678	205				
	-4.01	0.00	1.84				
843 ST 9192196.8 9455 748.98 C	85-4.7 (C) -5.29	0.688	205				
844 ST PIP2196.0 PASS 697.34 C	85-4.7 (C) -3.47	0.641	205				
445 ST PIP2196.0 PASS 633.41 C	85-4.7 (C) -2.53	0.502	205				
	••••••						
446 ST P1P2196.0 PASS 459.01 T	85-4.8.2.2 -4.31	0.509	204				
#47 ST P2P2196.0 PASS	85-4.4.2.2	0.428	204				
410.39 T	-4.23	0.00	0.00				
148 ST P1P2196.0 PASS 297.07 T	85-4.4.2.2	0.310	204				
297.47 T	-3.65	0.00	0.00				-
445 ST P2P2196.0 PASS	85-4.7 (C)	0.195	,				
212.07 C	-1.85	0.00	0.00				
850 ST P1P2196.0 PASS	85-4.8.2.2	0.209	207				
<b>59.24</b> T	-1.95	0.00	1.80				
651 ST P1P2194.0 PASS 223.86 C	85-4.7 (C) -0.58	0.207	204				
		0.00	2.02				
#52 ST P1P2196.0 PASS 136.34 C	85-4.7 (C) -0.93	0.126	204				
453 ST FIF2136.0 FASS 123.32 T	BS-4.8.2.2 -2.01	0.130	201 2.13				
110.11 T	85-4.4.2.2 -7.05	0.193	207 2.02				
855 ST P1P2194.0 PASS	85-4.8.2.2	0.199	207				
/1.44 1	-9.28	0.00	0.00				
456 ST P1P2196.0 PASS 167.04 C		0.153					
167.04 C	85-4.7 (C) -1.62	0.00	204 0.00				
157 ST P1P2194.0 PASS 315.24 C	85-4.7 (C) -0.16	0.290	204				
315.24 C		8.00	0.00				
858 ST P172196.0 PASS	85-4.7 (C) -1.47	0.413	204				
449.67 C	-1.47	0.00	0.00				

	2					TPL40581	Sheel	a 138	Rev R4b-FAB
-	Software license					Perfwind speed 3	25 m/r		
Job Title	Wisma Bella Swi		14 118			Ral Fabric R5	2.3 1113		-
						BY TSM	Dale	-Dec-11 0	TSM
Client	Majlis Perbandari	an Kuantan				File Q326-KSP-F	4b-Deg.s	Id Delatime 10-	Jul-2012 16:43
**		HETE (UNLE	hecks Cont	13					
			кт	HZ.	LOCATION				
	419 ST PIP2196.		85-4.7 (C) -2.65	0.523 0.00	204				
			85-4.7 (C) -2.45	0.619	204 0.00				
	861 ST 9392196.	0 PASS 732.70 C	85-4.7 (C) -4.25	8.673 0.00	204				
	862 ST PIP2196.	0 PASS 760.91 C	85-4.7 (C) -5.08	0.499	204				
	863 ST P193196.	PASS 746.92 C	85-4.7 (C) -4.09	0.646	204				
	864 ST P3P2196.	PASS 710.66 C	BS-4.7 (C)	0.653	204				
	\$65 ST P1P2196.		85-4.7 (C) -3.38	5.608 5.00	204				
	#66 ST PIPI196.		85-4.7 (C) -3.73	0.549	204				
	867 ST P1P2196.0		85-4.7 (CI	0.478	204				
	868 ST 9192196.0		-3.39	0.00	203				
			-2.79	0.00	0.00				
	149 ST PIP2196.0		85-4.7 (C) -2.93	0.491 0.00					
	878 ST P1P2196.0	532.21 C	85-4.7 (C) -2.72	0.405	201 0.00				
	\$71 57 P1P2196.0	PASS 515.46 C	#1-4.7 (C) -2.25	0.474 0.00	201 3.84				
	872 ST P3P2196.0	PASS 487.49 C	85-4.7 (C) -2.00	0.448	201				
	873 ST P1P2196.0	PASS 475.76 C	85-4.7 (C) -3.30	0.437	205				
	874 ST P1P2196.0	PASS 585.99 C	83-4.7 (C) -4.30	0.538	205				
	475 ST PIP2196.0	PA55 680.29 C	85-4.7 (C) -4.68	0.625	205				
	876 ST P192196.0	PASS 723.10 C	85-4.7 (C) -4.28	0.664	205				
	\$77 ST \$1\$2196.0	PASS 235.43 C	85-4.7 (C) -3.75	0.674	205				
	078 ST P1P2196.0	PASS	85-4.4.2.2 -6.44	0.674	264				
	\$79 ST P1P2196.0		#5-4.7 (C) -2.35	0.631	245				
	440 ST 9192196.0		85-4.7 (0)	0.00	285				
		626.27 C	-2.39	0.00	1.84				

			TPL40581	Sheet No	140	Rev R4b-FAB
5			Panwind speed 32	5 m/r		
Tille Wisma Bella Swimming Pool			Ref Fabric R5	.5 m/s		
			BY TSM	Cale17-De	0.11 Chd	TSM
Mailis Perbandaran Kuantan			FI Q326-KSP-R4			
Steel Design (Track 0) Checks Co	ont					
ALL UNITS ARE - IN HETE UNLESS OTHERWISE						
HDHER TABLE RESULT/ CRITICAL C	COND/ NATIO/	LOADING/				
	(C) 0.353	201				
903 ST P1P2196.0 PASS 85-4.7 343.64 C -1.5	0.00	0.00				
	101 0.373	201				
***************************************		0.00				
905 ST PJP2196.0 PASS 85-4.7 414.54 C -2.2	(C) 0.301 2 0.00	201 0.00				
	(C) 0.375	201				
	4 0.00	1.84				
907 ST 9192196.0 9355 85-4.7 388.07 C -1.6	(C) 0.357 1 0.00	201				
		1.14				
427.89 C -3.1	(C) 0.393 0.00	205				
	IC) 0.496	205				
539.44 c -3.8	7 0.00	1.84				
910 3T P1P2196.0 PA35 85-4.7 635.93 C -4.3	(C) 0.584	205				
	¢ 0.60	1.84				
911 ST P1P2196.0 PASS 85-4.7 693.34 C -4.3	(C) 0.637 1 0.68	205				
	(C) 0.667	205				
726.27 C -3.9	0.00	1.84				
513 ST P1P2196.0 PASS 85-4.7 737.82 C -5.38	0.677	205				
-3.41	0.631	205				
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	(C) 0.573	205				
	8.00	1 44				
916 ST 9292196.0 PASS 85-4.8.2.2 494.28 T -4.27	0.504	204				
917 ST P1P2196.0 PASS 85-4.8.2.2 404.54 T -4.15		0.00				
918 ST P1P2196.0 PASS M5-4.4.2.2	0.315	204				
	0.00	0.00				
919 ST P1P2196.0 PASS 85-4.7 ( 211.87 C -1.85	C) 0.195 0.00	2.00				
920 ST P1P2156.0 PASS 85-4.8.2.2 103.34 T -8.79	0.211 0.00	207				
121 ST P1P2196.0 PAST 81-4.7	c) 0.203	204				
219.55 C -0.55		2.02				
922 ST 9192196.0 PASS 85-4.7 ( 133.25 C -0.93	C) 0.124	204				
125.09 C -0.61						
124 ST P1P2196.0 PASS 85-4.1	c) 0.186	,				
201.18 C -0.20		0.00				

K			Job No TPL40581	Sheel No	a 141	Rev R4b-FAB
Software Econsed to Transarve Pie Ltd			Panwind speed 33	2.5 m/s		
Jeb Title Wisma Belia Swimming Pool			Ref Fabric R5			
have a set of the set of the set of the			BY TSM	Date 17-De	to-11 Ch	TSM
Client Majils Perbandaran Kuantan			File Q326-KSP-R	b-Deg.sld	Deterime 10-J	ul-2012 16:43
Steel Design (Track 0) Checks ALL UNITS ARE - KN HETE (UNLESS OTHER HENRER TABLE RESULT/ CRITIC	WISE HOTEDI	LOADING/				
TX 925 ST P1P2196.0 PASS 85-4.		LOCATION				
90.72 T	-1.15 0.00	0.00				
201.48 C	-2.62 0.00	0.00				
927 ST 9192194.0 PASS 85-4. 344.40 C	7 (CI 0.316 -0.47 0.00	204				
520 ST PIF2196.0 FASS BI-4. 471.54 C	7 (C) 0.434 -1.76 0.00	204 0.00				
525 57 F1F2194.0 FASS 85-4. 543.33 C		204 0,00				
\$20 ST F1F2195.0 PASS 85-4.		204 0.00			15	
531 ST PIP2196.6 PASS 85-6.	7 (C) 8.674	204				
932 ST P1P2196.0 PASS 85-4.	7 (C) 0.702	204				
533 57 F1F2196.0 FASS 85-4.7 737.84 C		204				
936 ST P1P2195.0 PASS MS-4.7		204				
535 ST PIP2194.0 PASS 85-4.1 623.01 C		204 0.00				
936 ST PIP2196.0 PASS 85-4.1 542.77 C	1C1 0.499	204 0.00				
937 ST P1P2196.0 PASS 85-4.7	(C) 0.412	204				
338 ST PIP2196.0 P555 85-6.7		201				
939 57 9192196.0 PASS 85-4.7 388.78 C	ICI 0.357	201				
940 ST P1P2194.0 PASS 85-4.7 405.64 C -	(C) 0.372 2.15 0.00	201				
941 ST 9192196.0 PASS 85-4.7	(C) 0.372 1.65 0.00	201				
942 ST PIP2196.0 PASS 85-4.7 330.80 C	(C) 0.359	201				
943 ST P1P2196.0 P335 85-4.7 439.14 C -	(C) 0.403 3.20 0.00	205				
944 ST PIP2194.0 PASS 85-4.7 551.46 C -	(C) 0.307 4.04 0.00	205				
345 ST PIP2134.0 PASS 85-4.7	(C) 0.595	205				
946 ST P1P2196.0 PASS 85-4.7 705.53 C		205				

$\mathcal{D}$	TPL40581	Sheet No a 142	Rev R4b-FAB
Software licensed to Transerve Pie Ltd	Padwind speed 32.	5 m/e	
Jeb Tile Wisma Bella Swimming Pool	Ref Fabric R5		
	BY TSM	Cale17-Dec-11 CA	TSM
Clent Majlis Perbandaran Kuantan		-Deg.std Data/Time 10-	
Steel Design (Track 0) Checks Cont           NAL WITE WHEE WHEEM WHEEM WHEEM           MARK WHEEM WHEEM WHEEM WHEEM WHEEM           MARK WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM           MARK WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM           MARK WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM           MARK WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM WHEEM           MARK WHEEM WHEM WH			
954 57 P1P2196.0 PASS 85-4.7 (C) 0.195 9 212.07 C -1.85 0.06 0.00 355 57 P1P2196.0 PASS 85-4.8.2.2 0.204 207			
555 57 F172195.0 PASS 85-4.7 ICT 8.287 254 223.89 C -0.55 6.00 2.02			
957 3T FIF2196.5 FASS 85-4.7 (C) 6.124 284 136.37 C -0.53 5.00 2.13			
558 57 9292196.0 PA35 85-6,8,2,2 0.126 201 113.77 7 -1.88 0.00 2.13			
555 ST P1P2186.0 PASS JAMEX 1.1 0.237 208 46.44 C -4.09 20.36 -			
940 3T F172134.0         PASS         BF-1.8.2.2         0.265         256           22.7.7         -70.4.0         8.84         4.06           941 ST F172134.0         PASS         BF-4.7         (C1         0.174         4           951 ST F172134.0         FASS         BF-4.7         (C1         0.174         4			
192.10 C -2.65 0.00 0.00 962 ST F2F2196.6 FASS 85-6.7 (C) 0.246 266 249.23 C -5.75 0.00 0.00			
963 57 F1F2196.0 FASS 85-4.7 (C) 0.359 204 390.35 C -2.39 0.00 0.00			
364 ST PIP2196.0 PASS B5-6.7 (C) 0.415 204 451.39 C -2.64 0.00 0.00			
965 ST P1P2196.0 PAGS 85-4.7 (C) 0.453 204 453.25 C -2.73 0.60 0.60			
946 57 9292194.0 PASS 85-4.8.2.2 0.344 205 518.55 7 -7.21 0.00 1.84			
567 5T F172134.0 FASS 85-4.4.2.2 0.653 285 615.62 T -6.50 0.00 0.00			
968 57 9192396.0 PASS 85-4.6.2.2 0.546 205 534.92 7 -4.49 0.00 0.00			

Pdal TerelDala

2	TPL40581	Sheet No	a 139	Rav R4b-FAB	
Software licensed to Transerve Pie Ltd	Part wind speed 32.5 m/s				
Jee Tile Wisma Belia Swimming Pool	Ref Fabric R5				
	By TSM Dalk17-Dec-11 Chd TSM				
Client Majils Perbandaran Kuantan	File Q325-KSP-R4	-Deg.std	Date/Time 10-J	ul-2012 16:43	

### Steel Design (Track 0) Checks Cont...

	esign (Tr		hecks Cont		
KDIBER	TABLE	NESULT/	CRITICAL COND/	NAT10/ HZ	LOADING/
881	ST PIP2156.0	PASS 500.50 T	85-4.8.2.2 -4.27	0.510 0.00	204 0.00
102	57 P1P2196.0	PASS 419.97 T	85-4.8.2.2 -4.33	0.438	204
***	ST P1P2196.0	PASS 313.44 T	85-4.8.2.2 -3.83	0.335 0.00	204
	T 9192196.0	PASS 181.32 T	85-4.8.2.2 -3.11	0.205	204
115 2	67 PIP2196.0	7A35 121.73 T	85-4.8.2.2 -8.94	0.225 0.00	207
*** :	T PIP2156.0	7A55 206.20 C	85-4.7 (C) -0.74	0.191 0.00	204 2.02
<b>687</b> 2	T P1P2196.0	PA53 127.52 C	85-4.7 (C) -0.34	0.110	o
	T P1P2196.0	PA55 107.54 C	85-4,8,3,3,1 -0,67	0.121 0.67	202
	T P3P2196.0	PASS 175.37 C	85-4.8.3.3.1 -3.38	0.221 0.02	2
130 1	T P1P2196.0	PASS 61.06 T	85-4.9.2.2 -9.10	0.178 0.80	207
#91 S	T P1P2196.0	PASS 181.53 C	85-4.7 (C) -1.87	0.167 0.00	204
192 5	T P1P2196.0	PASS 330.16 C	85-4.7 (C) -8.34	0.303 0.00	204
***	T PIP2196.0	PASS 443.10 C	85-4.7 (C) -1.68	0.425	204 0.00
194 3	T PIP2196.0	PASS 579.43 C	85-4.7 (C) -2.83	0.503 0.00	204
195 5	T P172196.0	PASS 675.28 C	85-4.7 (C) -2.79	8.624 0.00	204
496 3	T P3P2196.0	PASS 739,23 C	85-4.7 (C) -4.16	0.675	204
897 5	7 9192136.0	PASS 176.61 C	85-4.7 (C) -5.61	0.714	204
••••	T PIP2196.0	PASS 750.27 C	85-4.7 (C) -4.26	0.609	204 0.00
459 5	T P1P2196.0	PASS 700.02 C	85-4.7 (C) -4.44	0.643	204 0.00
900 S	F \$1\$2196.0	FA35 635,73 C	85-4.7 (C) -4.02	0.504	204 0.00
301 S	P1P2196.0	PA55 555.53 C	85-4.7 (C) -3.70	0.510	204
902 5	F P1P2196.0	PASS 460.62 C	85-4.7 (C) -3.26	0.423	204

Refer Town Palace

2	TPL40581 a 143	Rev R4b-FAB			
Software Reenand to Transacro Pin Lid	Parl wind speed 32.5 m/s				
leb Tile Wisma Belia Swimming Pool	Ref Fabric R5				
	By TSM Dele17-Dec-11	Che TSM			
Clant Majils Perbandaran Kuantan	File Q326-KSP-R4b-Deg.std DeleTime	10-Jul-2012 16:43			

laa	Design	(Track	01	Checks	Cont	

MPP CHILIP	NRE - KN	HETE INNLE	S OTHERWISE NOTED		
HEHBER	TABLE	AESULT/	CRITICAL COND/	MATIO/	LOADING
969 57	P1P2196.0	FASS 573.29 C	85-4.7 (C) -3.71	0.527	204
\$70 57	P172196.0	PASS	85-4.7 (C)	0.524	204
		570.23 C	-3.34	0.00	0.01
	P172194.0	PASS	85-4.7 161	0.500	204
		544.21 C	-3.93	0.00	0,01
972 57	P1P2196.0	PASS 462.84 C	#5-4.7 (C) -3.80	0.425	204
			-2.10		
973 ST	P172196.0	PASS	85-4.7 (C)	0.369	201
		402.06 C	-2.17	0.00	0.00
974 ST	P1P2196.0	PASS 405.45 C	85-4.7 (C) -2.73	0.373	201
			*******		
975 ST	P1P2196.0	PASS	85-4.7 (C)	0.357	201
		368.16 C	-1.62	0.00	0.00
	P1P2195.0	PASS	85-4.7 (C)	0.375	201
310 31	F1F2138.V	412.75 C	-2.70	0,00	1.84
\$77 ST	P1P2196.0	PASS 416.65 C	85-4.7 (C) -2.28	0.363	201
		414.45 0		0,00	
178 17	P1P2196.0	PASS	85-4.7 (C)	0.438	205
		476.22 C	-2.69	0.00	1.84
979 57	FIP2196.0	7A55 555.89 C	#5-4.7 (C) -3.97	0.511	205
980 ST	P172196.0	PASS	85-4.7 ICI	0.540	205
		587.65 C	-3.72	. 0.00	1.84
	P792196.0	PASS	85-4.7 (C)	0.510	205
		385.43 C	-2.74	0.00	1.64
	******				
582 57	P1P2196.0	PASS 525.82 T	85-4,8.2.2	0.535	204
			-1.12		
383 57	PIP2196.0	PASS	85-4.8.2.2	0.644	204
		613.23 T	-6.73	0.00	1.14
584 ST	P1P2196.0	7A55 525.10 T	15-4.8.2.2	0.567	204
985 ST	F1F2196.0	PASS	15-4.8.2.2	0.465	204
		462.48 T	-3.48	8.00	0.00
		PASS	85-4.7 (C)	0.397	205
		431.69 C	-2.55	0.00	1.00
987 ST	P1P2196.0	7455 375.63 C	85-4.7 (C) -2.32	0.345	205
188 57	P1P2196.0	PASS	N-4.7 (C)	0.256	205
		279.07 C	-0.68	0.00	1.84
989 ST	P1P2196.0	PASS 189.42 C	85-4.7 (C) -1.58	0,174	0.00
110 ST	P1P2196.0	73.55	\$5-4.8.2.2	0.312	204
		30.04 7	-21.35	0.00	1.90



Ð	TPL40581	Sheel No	a 144	R4b-FAE
Solivare Icansed in Transacre Pie Lid	Partwind speed 32.5	5 m/s		_
a Tile Wisma Belia Swimming Pool	Ref Fabric R5			
	BY TSM	Calt 17-D	ec-11 Chd	SM
Mailis Perbandaran Kuantan	File Q326-KSP-R45		Date/Time 10-Jul	
Steel Design (Track 0) Checks Cont				
HDSRR TABLE REVELT/ CRITICAL CORD/ NATIO/ LOADING/ RY HI LOCATION				·
591 ST P1P2194.0 PASS ANNEX 1.1 0.335 208 50.34 C -4.15 20.57 -				
992 ST P3P2194.0 PX35 B5-4.0.2.2 0.322 201 107.13 T -1.89 0.00 0.00				
993 57 FIP#9.124.0 FASS 85-4.7 (C) 0.278 265 69.05 C -0.36 0.05 0.00				
394 ST PIPHS.1X4.0 PASS 85-4.8.2.2 0.295 205 71.22 T -0.42 0.80 1.55				
555 57 F1795.124.0 F355 85-4.7 (C) 9.224 265 59.17 C -9.46 8.60 0.00				
934 ST PIP49.3X4.0 PASS 85-4.8.2.2 0.287 205 66.42 T -8.58 0.00 1.35				
337 ST PIPHS.1X4.0 PASS 85-4.8.2.2 0.225 204 45.22 T -0.46 0.00 1.35				
398 ST P2P89.1X4.0 PASS 85-4.8.2.2 0.21 205 54.82 T -0.43 0.00 1.35				
335 ST PIPES.1X4.0 PASS 35-4.8.2.2 0.255 204 54.78 7 -8.50 8.60 8.60				
1000 ST P3P#5.1X4.0 TASS 85-4.7 (C) 0.232 204 57.73 C -0.46 8.60 1.85				
1001 3T P2F89.1X4.0 PASS 85-4.4.2.2 0.292 209 71.75 T -0.38 0.00 1.55				
1007 ST P1989.1X4.0 PASS 85-4.7 (C) 0.260 209 64.53 C -0.63 0.00 1.95				
1003 ST P1949.3X4.0 PASS 85-4.8.2.2 0.342 209 84.39 T -0.60 8.00 1.95				
1004 ST P1P09.3X4.0 PASS 85-4.7 [C] 0.322 209 75,59 C -0.73 0.00 1.95				
1805 ST P1P49.1X4.0 PASS 85-4.8.2.2 0.383 209 54.89 T -0.56 0.40 1.55				
1004 ST P1P89-1X4.0 PASS B5-4.7 (C) 0.271 269 52.20 C -0.58 0.00 1.55				
1007 ST PIPES,1X4.0 PASS 85-4.8.2.2 0.447 205 98.147 -0.91 0.08 0.00				
1084 ST P1P49.1X4.0 PASS B5-4.8.1.3.3 0.616 209 184.58 C -0.72 0.55 -				
1009 57 P1P114.3X4.5 PASS ANNEX 1.1 0.342 205 42.17 C -1.74 2.55				
1010 ST PIPES.IX4.0 PASS 85-4.8.7.2 0.274 205 35.55 T -1.22 0.00 1.55				
1011 5T PIPHS,1X4.0 PASS 85-4.7 (C) 0.199 204 49.50 C -0.29 0.00 0.00				
1812 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.247 204 50.13 T -8.61 0.60 1.95				

2	TPL40581	Shael No a 145	Rev R4b-FAI
Software licensed to Transance Pie Lid	Partwind speed 32.	5 m/s	
Tile Wisma Bella Swimming Pool	Ref Fabric R5		
	BY TSM	Date 17-Dec-11 Ch	TSM
N Majils Perbandaran Kuanlan	File Q326-KSP-R4		Jul-2012 16:43
Steel Design (Track 0) Checks Cont			
HOWER TABLE RESULT/ CRITICAL COND/ RATIO/ LOADING/ FX HT HE LOCATION			
***************************************			
1013 3T \$1989.1X4.0 \$ASS 85-4.7 [C] 0.220 206 54.66 C -0.23 0.00 0.06			
1014 5T F2P114.3X4.5 P355 B5-4.8.2.2 0.259 254			
1014 ST F1F114.384.5 FASS B5-4.8.2.2 0.259 204 48.55 T -2.16 0.00 3.55			
1015 ST PIP49.1X4.0 PASS 85-4.7 (C) 0.224 204			
55.57 C -0.25 0.00 0.00			
1016 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.245 204 48.85 T -0.66 0.00 1.95			
1017 ST F1P89.1X4.0 FASS 85-4.7 (C) 0.185 206			
1017 57 PIPES.1X4.0 PAIS 85-4.7 (C) 0.185 206 45.82 C -0.17 0.00 0.00			
1018 ST PIPEP.1X4.0 PASS 85-4.8.2.2 0.262 206			
46.55 7 -0.61 0.00 1.55			
1019 ST P3P89.1X4.0 PASS 85-4.8.2.2 0.222 207 23.22 T -0.07 0.00 0.00			
1020 ST P1P89.1X4.0 PASS 85-4.0.2.2 0.254 206 43.15 T -0.85 0.00 0.00			
1021 ST PIPH9,1X4.0 PAGS ANNEX 1.1 0.243 206 31.49 C =0.46 1.19 -			
1022 ST P1P89.3X4.0 PASS 85-4.8.2.2 0.362 205 47.66 T -1.61 0.00 0.00			
***************************************			
1023 ST P1P49.1X4.0 PAES MMCX 1.1 0.273 206 25.68 C -0.43 1.53 -			
1024 ST P1/14.384.5 PASS 85-4.7 (C) 0.199 202			
77.32 C0.28 0.00 1.36			
1025 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.242 202 64.66 T -0.33 0.00 2.02			
***************************************			
1026 ST P1P89.1X4.0 PASS 85-4.7 (C) 0.387 202 75.16 C -0.42 0.00 2.02			
1027 ST P1P49.1X4.0 PASS 85-4.8.2.2 0.348 202			
84.35 T -0.48 0.00 2.02			
1028 ST PIPED.1X4.0 PASS JUNEX 1.1 0.125 202 25.18 C -0.39 0.50 -			
1029 ST PIP14.3X4.5 PASS 85-4.7 (C) 0.375 202 101.75 C -0.55 0.00 3.59			
1030 ST PIPIL4.384.5 PASS 85-4.7 (C) 0.178 204			
69.41 C -0.67 0.00 0.00			
1031 ST F1P#9.1X4.0 FASS B5-4.8.2.2 0.292 204 59.51 T -0.43 0.00 1.55			
1832 ST P1P89.1X4.0 PASS 85-4.7 IC] 0.247 204 61.46 C -0.45 8.00 8.00			
1033 57 F1F45.3X4.0 FASS 85-4.4.2.2 0.336 204			
70,78 T -0.76 0.00 1.55			
1034 ST PIP89.1X4.0 PASS 85-4.8.2.2 0.249 205 49.42 T -0.44 0.00 0.00			

2					Jet
	ensed to Transarve P	te Ltd			P
ob Title Wisma Bella					-
					1
Ieni Majlis Perban	daran Kuantan				
ALL UNITS AND - HEMBER TABL	KN HETE IUHLE E RESULT/ FX 19.114.0 PASS 64.55 T	\$\$-4.8.2.2 -0.62	0.231 0.00	204 1.95	
		85-4.8.2.2 -0.56			
	19.1X4.0 PAIS 51.86 T	-0.53	0.243	204 6.00	
1038 57 919	19.114.0 PASS 74.75 T				
	9.1X4.0 PA35 67.27 C	-0.72	0.271 0.00	205	
1040 ST FIF	\$5.91 T	85-4.8.2.2 -0.75	0.386 0.00	209	
1041 ST PIP	9.1X4.0 PAIS 81.01 C	85-4.7 (C) -0.91	4.326 0.00	205	
1042 ST PIP	5.1X4.0 FASS 54.36 T		0.410 0.00	205	
3043 ST PIPI	9.124.0 PASS 91.94 C	85-4.7 [C] -0.63	0.370	205	
1044 ST PIP	97.90 T	85-4.8.2.2 -0.91	0.447 0.00	205	
	9.1X4.0 PASS	85-4.4.3.3.3 -0.62	0.420	12	
1046 ST 7171		NINEX 1.1	0.348 2.55	204	
1047 ST PIPE	9.1X4.0 PASS	85-4.8.2.2 -1.32	0.254	204	
1048 ST PIPS			0.217 0.00	205 0.00	
1049 ST PIPE		85-4.8.2.2 -0.62	0.232	205	
1050 ST PIPO		#1-4.7 ICI -0.25	0.231 0.00	205	
1051 ST PIPI	14.384.5 PASS 50.39 T	85-4.8.2.2 -1.75	0.235	205	
1052 ST PIPE	5.1X4.0 PASS 57.69 C	85-4.7 (C) -0.18	0.232	205	
1053 ST PIPE	9.1X4.0 PASS 30.60 T	85-4.8.2.2 -0.60	0.246 0.00	205 1.95	
1854 ST PJP4		85-4.7 (C) -0.17	0.185 0.00	204 0.00	
3055 ST P1P4		85-4.8.2.2 -0.81		206	
1056 ST P1P8	5.1X4.0 PASS 32.58 T	85-4.8.2.2 -0.91	0.226	207	

2				TPL40581	Sheel No	a 148	Rev R4b-FAB
Software licensed to Transprve	Pield			Partwind speed 32.	5 m/s		
eb Tille Wisma Bella Swimming Poo				Ref Fabric R5			
				BY TSM	Date 17-D	ec-11 Cha	TSM
Majis Perbandaran Kuantan		_		Fla Q326-KSP-R4b		Dele/Time 10-J	
Steel Design (Track 0)	Checks Cont						
ALL UNITS MAE - KH HETE (UNI							
HENDER TABLE RESULT	CATTICAL COND/	AATIO/	LOADING/				
1075 ST P1P#5.1X4.0 PASS	83-4.4.2.2	0.325	201				
*******							
1080 ST PIP89.1X4.0 PASS 80.60 C	85-4.7 (C) -0.44	0.324	201				
1081 57 91989.1X4.0 9A55 85.45 7	85-4.8.2.2 -0.75	0.384	201 0.00				
1092 ST #1949.1X4.0 PASS	85-4.4.3.3.1	0.401	209				
13.76 c	-0.36	0.10					
1083 57 PIP114.3X4.5 PASS 77.34 7	85-4.0.2.2	0.328	203				
77.34 7	-2.20	0.00	1.95				
1004 ST PIP09.1X4.0 PASS 22.16 T	85-4.8.2.2	0.214	207				
	-1.11	0.00	1.95				
1045 ST FIP#9.1X4.0 PASS	85-4.8.2.2	0.270	205				
1086 ST P1P89.1X4.0 PASS 50.62 C	85-4,7 (C) -0,65	0.204	206				
		0.333	205				
1087 57 PIP89.1X4.0 PASS 67.32 T	85-4.8.2.2 -0.83	0.333	0.00				
1088 ST PIP114.3X4.5 PASS	85-4.8.2.2	0.205	204				
	-2.25	0.00	1.95				
1045 ST PIPES.1X4.0 PASS	85-4.8.2.2	0.377	205				
64.16 T	-0.72	0.00	0.00				
1090 ST PIPES.1X4.0 PASS 74.44 C	85-4.7 (C) -0.52	0.308	205				
	-9.52		1.55				
1091 ST P1P89.1X4.0 PASS	85-4.8.2.2	0.366	205				
1092 ST P1P69.1X4.0 PASS 83.42 C	83-4.7 (C) -0.65	0.335	205				
	\$5-4.8.2.2	0.449	203				
1093 57 PIPES.1X4.0 PASS 95.41 T	-0.89	0.00	0.00				
1094 ST P1P49.1X4.0 PASS	85-4.7 ICI	4.397	205				
98.71 C	-0.19	0.00	1.95				
1095 ST PIPS9.1X4.0 PASS	85-4.8.2.2	0.466	205				
109.74 7	-0.74	0.00	0.00				
1696 ST PIP89.1X4.0 PASS 99.55 C	85-4.7 (C) -0.53	0.400	205				
	-4.53	0.00					
1097 ST PIPES.1X4.0 PASS 96.25 T	85-4.8.2.2 -0.20	0.352	205				
1094 ST P1P114.3X4.5 PASS 44.52 C	ANNEX 1.1 -0.95	0.172	205				
1099 ST PIP89.1X4.0 PASS 36.14 C	-0.23	0.195	205				
	No. 1.1.1.1	0.176	204				
1100 ST PIPES.1X4.0 PASS 2.54 C	85-4.8.3.3.3 -0.77						
		50 C 21	2018-04-04-0 <del>77</del> 5				

R					Jeb No TPL40581	Sheel No	a 149	Rev R4b-FAB
Solware	Ecensed to Transerve P	in Lid			Partwind speed 32	.5 m/s		
Job 716 Wisma Bel					Ref Fabric R5			
					BY TSM	Dele17-D		
clieni Majils Perb	andaran Kuantan		and the		Fla Q326-KSP-R4	b-Deg.sid	Data/Time 10-Jul	-2012 16:43
ALL UNITS AND	ALE MESULT/	SE OTHERWISE HOTED CRITICAL COND/	MATIO/	LOADING/				
	<u>n</u>	HY M-4.7 [C]	H2 0.220	LOCATION				
	53.75 C	-0.10	0.00	0.00				
	1989.1X4.0 PASS 3.23 C		0.076	200				
	19114.3X4.5 PASS #2.93 7	85-4.8.2.2 -0.63	0.235	245				
	19114.384.5 PASS 69.91 T	85-4.8.2.2 -1.27	0.249	205				
	70.64 T	85-4.8.2.2 -0.37	0.207 0.00	204				
	1949.184.0 PASS 59.84 T	85-4.8.2.2 -0.43	0.265	205				
	1989.1X4.0 PASS	#1-4.8.2.2 -0.75	0.325	204 1.95				
	1989.1X4.0 PASS 52.97 7	85-4.8.2.2 -0.71	0.269	205				
1109 ST P	789.1X4.0 PASS 57.05 T	85-4.8.2.2 -0.58	0.266	204				
1110 ST #	P45.1X4.0 PASS 47.02 T	#5-4.8.2.2 -1.00	0.285	205				
1313 ST P	P49.1X4.0 PASS	85-4.8.2.2	0.238	204				
1112 ST P	P89.1X4.0 PASS 45.37 T	85-4.8.2.2 -0.91	0.268	205 0.00				
	P89.1X4.0 PASS 54.57 C	MS-4.7 (C) -0.88	0.228	205 1.95				
	P85.1X4.0 PASS 40.76 T	85-4.8.2.2 -0.55	0.258	205				
	P89.1X4.0 PASS 54.45 C	83-4.7 (C) -0.58	0.215	205				
1116 ST PI	P89.1X4.0 PASS 54.48 T	85-4.8.2.2 -0.58	0.272	201				
	519.124.0 PASS	85-4.7 (C) -0.51	0.239	201				
	PED.1X4.0 PASS 65.70 T	85-4.8.2.2 -0.70	0.312 0.00	201 0.00				
	P49.1X4.0 PASS 44.09 C	85-4.8.3.3.1 -1.05	0.382	203				
1120 57 92	F114.3X4.5 FASS 12.28 C	ANNEX 1.1 -7.16	0.354	204				
3123 57 91	P89.1X4.0 PASS 30.70 T	85-4.8.2.2 -1.16	0.250	207				
	P#9.1X4.0 PASS 45.20 7	#5-4.8.2.2 -0.93	0.270	204				

TAN SIEW MOI

Subus Isauel u Tanzara Pa Lid un Tite Wilsma Bala Swimming Pool Zeel Majils Parbandaran Kuantan Steel Design (Track 8) Checks Cont ALL WILT JAL - MI HETE GINLESS enternist writen	Parlwind speed 32. Ref Fabric R5 By TSM Pile Q326-KSP-R41		
va Tra-Wisma Bella Swimning Pool Zmi Majlis Parbandaran Kuantan <u>Steel Design (Track 8) Checks Cont</u> Auk Witt Jak - on mitte lioktat entemiste wortan	Ref Fabric R5		
Zeel Majlis Perbandaran Kuanlan Steel Design (Track 0) Checks Cont ALA WITH AM - NH INTE (DALES PREMITE WITH	BY TSM	Dale17-Dec-11 Ch	
Steel Design (Track 0) Checks Cont	Ple Q326-KSP-R4		TSM
Steel Design (Track 0) Checks Cont		Deg.std DeterTime 10-	Jul-2012 16:43
ALL UNITS ARE - 101 HETE (UNLESS OTHERHISE HOTED)			
HEMBER TABLE RESULT/ CRITICAL COND/ NATIO/ LONDING/			
HDHBER TABLE RESULT/ CRITICAL COUD/ NATIO/ LOADING/ FX HY HI LOCATION			
1123 ST PIP#9.1X4.0 PASS 85-4.7 (C) 0.180 205 44.70 C -0.44 0.00 1.95			
1124 ST P3P89,1X4.0 PA35 B5-4.8.2.2 0.320 204 10.45 7 -0.64 0.00 0.00			
70.45 T -0.64 0.00 0.00			
1125 57 FIP114.2K4.5 FA55 B5-4.8.2.2 0.181 9 27.94 7 -1.73 0.00 1.95			
1126 ST PIP83.1X4.0 PASS 83-4.8.2.2 8.385 204 86.30 T -0.72 0.00 0.00			
1127 ST PIP89.1X4.0 PASS B5-4.7 (C) 0.318 204 79.08 C -0.54 0.00 1.55			
1126 ST FIFES.1X4.0 FASS 85-4.8.2.2 0.381 204 50.70 7 -0.58 0.00 0.00			
1125 ST F1F99.1X4.0 FASS 85-4.7 (C) 0.345 204 85.72 C -0.66 0.00 1.95			
1130 ST P1989.1X4.0 PASS B5-4.8.2.2 0.467 204 101.64 T -0.96 0.00 0.00			
1131 57 P1789.1X4.0 PASS 85-4.7 (C) 0.487 204 101.15 C -0.52 0.00 1.55			
1132 ST FIP45.1X4.0 PASS 85-4.8.2.2 0.485 204			
1122 ST P1P45.1X4.0 PASS 85-4.7 (C) 0.408 204			
101.30 C -0.57 0.00 1.55			
1134 ST P1P89.1X4.0 PA3S 85-4.8.2.2 0.358 204 98.86 T +0.17 0.00 1.93.			
1135 ST P1P114.3X4.5 PASS ADMEX 1.1 0.171 206 43.46 C -0.94 1.40 -			
1136 ST FIF99.1X4.0 FASS 85-4.8.3.3.3 8.202 204 28.28 C -0.23 8.05 -			
1137 ST P1P89.1X4.0 PAGS 85-4.8.3.3.3 0.174 206 1.36 C -0.77 0.26 -			
1139 ST PIP49.1X4.0 PASS 85-4.7 (C) 0.226 204			
1139 ST PIPE9.124.0 PASS AMMEX 1.1 0.077 208 3.12 C -0.44 0.17 -			
1140 ST P1P114.3X4.5 PASS 85-4.8.2.2 0,240 284 84.34 7 -0.42 0.00 3.59			
1141 57 F1F89.1X4.0 FASS 85-4.8.3.3.3 0.316 5 53.07 -0-25 0.12 -			
1142 57 P1993.1X4.0 PASS 85-4.8.2.2 0.304 205			
75.66 7 -0.37 0.00 1.93			
1143 ST PJP89.114.0 PASS M5-4.7 (C) 0.291 205 72.30 C -0.43 0.00 0.00			
1144 ST P1P49.1X4.0 PA35 E5-4.8.2.2 0.307 205 77.53 T -0.33 0.00 0.00			

a 146

Oble17-Dec-11 Child TSM 4b-Deg.std Oble75me 10-Jul-2012 16:43



Sobres Scased Is Timesve Pie Lis Wisma Bella Swimming Pool	100 No TPL40581	Sheel No a 147	Rev R4b-FAB			
	Parlwind speed 32.5 m/s					
	Ral Fabric R5					
	BY TSM	Dale17-Dec-11	TSM			
Majlis Perbandaran Kuantan	File Q326-KSP-R4	b-Deg.std Date/Time 10-	Jul-2012 16:43			

eel Design (Ti		hecks Cont		
HIGER TABLE	NESULT/	CRITICAL COND/	NATIO/ M2	LGADING/ LOCATION
1057 ST PIP49.13	4.0 PASS 43.84 T	85-4.8.2.2 -0.81	0.251 0.00	206
1058 ST PIP89.1X	4.0 PASS 38.41 C	AUGER 1.1 -0.43	0.234 1.14	206
1059 ST PIPES.1X	4.0 PASS 47.75 T	85-4.8.2.2 -1.57	0.359	206
1060 ST 91989.1x	4.0 PASS 26.74 C	AURICX 1.1 -0.41	0.269 1.51	206
1061 ST P3P114.3	X4.5 PASS 75.27 C	85-4.7 (C) -0.28	0.194 0.00	202
1062 ST P1289.13	4.0 PASS 64.71 T	85-4.8.2.2 -0.33	0.262 0.00	202
1063 ST PIP89.18	4.0 PASS 75.15 C	85-4.7 (C) -0.42	0.307	202
1064 ST 91989.1X	4.0 PASS 84,77 T	83-4.8.2.2 -0.49	0.349	202
1065 ST PIP89.1X	4.0 PASS 25.43 C	AXMEX 1.1 -0.38	0.125 0.51	202
1066 ST P1P114.3	X4.5 PASS 102.09 C	85-4.7 (C) -0.56	0.376 0.00	202 3.59
1067 ST P3P89.1X	4.0 PASS 68,96 T	85-4.8.2.2 -0.66	0.317 0.00	204
1048 ST P1785.18	4.0 PASS 68.25 T	85-4.8.2.2 -0.35	0.201	205
1069 ST P1989.1X	(.0 PASS 59.15 T	85-4.8.2.2 -0.79	6.301 8.00	204
1070 ST P3P89.18	4.0 PASS	83-4.8.2.2 -0.50	0.295 0.00	205
1071 ST PEPSS.1X	.0 PASS 55.15 C	85-4.7 (C) -0.43	0.322	205
1072 ST PIP69.13	4.0 PASS 64.16 T	85-4.8.2.2 -0.41	0.270 0.00	205
1073 ST P1P09.1X	40.05 T	85-4.8.2.2 -0.93	0.253 0.00	204
1074 ST P1P85.3X	.0 PASS 56.50 T	85-4.8.2.2 -0.55	0.265 0.00	205
1075 ST P1P89.1X	1.0 PASS 40.91 T	65-4.8.2.2 -0.91	0.253	204
1076 ST P3P85.3X	.0 PASS 54.02 T	85-4.9.2.2 -0.37	0.231 0.00	1.95
1077 ST P1P89.1X4	.0 PASS 46.31 T	85-4.8.2.2 -0.83	0.262	294
1076 ST PIPOD.1X	PASS	85-4.7 ICI	0.235	203

Client

Int Run 45 of 10

20.07.02.1

2	TPL40581	sheel No a 151	Rev R4b-FAB
Solware licensed to Transerve Pie Ltd	Panwind speed 32	.5 m/s	
Job Tille Wisma Bella Swimming Pool	Ref Fabric R5		
	BY TSM	Dale17-Dec-11	Chd TSM
Citati	Ela conse unos es	Deleteration of the second sec	

(Track 0) Checks Cont
(Track 0) Checks Cont

HDIGES	TABLE	BESULT/	CRITICAL COND/	BATID/	LEADING
ADABLA	INDIA	FX	HY	HI	LOCATIO
1145 57	PIP69.13	4.0 PASS 48.01 C	85-4.7 (C) -0.43	0.274	205
1146 57	PIP89.13	4.0 PASS 76.16 T	61-4.8.2.2 -0.31	0.258	205
1147 57	\$1969.13	4.0 PAIS	85-4.7 (C) -0.43	0.243	205
1148 57	P1P89.13	4.0 PASS 71.20 T	85-4.8.2.2 -0.28	0.278	205
	P1P89.13	4.0 PASS	85-4.7 (C)	0.203	205
1345 57	F1749.10	50.34 C	-0.42	0.00	0.0
1150 57	P1249.10	4.0 PASS	85-4.1.2.2	0.244	285
IIN IT	A1111.10	63.78 T	-0.22	0.00	0.0
1151 57	P1P89.13	4.0 PASS 55.05 T	85-4.8.2.2	0.207	201
1152 ST	P1209.13	4.0 PASS	85-4.8.3.3.3	0.212	104
		42.71 C	-0.54	0.21	
1153 57	PIP89.13	4.0 PASS	85-4.0.2.2	0.275	201
		68.91 T	-0.35	6.00	0.0
1134 57	P1P89.13	4.0 PASS	85-4.7 (C)	0.269	201
1154 ST	ALLAN. 13	66.56 C	#5-4.7 (C) -0.38	0.265	1.9
1155 ST	P1P89.13	4.0 PASS 70.15 T	85-4.8.2.2	0.283	201
1156 ST	P1785.1X	4.0 PASS	85-4.7 (C)	0.282	201
		70.21 C	-0.28	0.00	1.5
1157 57		14.5 PASS	85-4.8.2.2	0.228	201
1141 51		78.41 T	-0.62	0.00	0.0
1158 ST	P1785.1X	4.0 PASS	85-4.7 ICI -0.28	0.074	205
1159 ST	P1789.13		85-4.1.2.2	0.178	205
		45.96 7	-0.18	6.00	1.9
1160 57	P1P85.1x	4.0 PASS	85-4.7 (C)	0.128	205
		31.70 C	-0.36	8.00	1.9
					205
1161 57	P1799.1x	4.0 PASS 55.34 T	85-4.8.2.2 -0.15	0.207	1.9
1162 57	P1P114.3	10.52 T	85-4.6.2.2	0.118	204
1143 ST	P1P85.1X	4.0 7855	85-4.8.3.3.3	0.271	284
		54.95 C	-0.20	0.16	
1164 57	P1247.12	4.0 73.55	\$5-4.1.3.3.1	0.250	205
		52.32 C	-0.05	5.42	
1165 ST	P1P49.13	4.0 PASS 57.63 C	83-4.4.3.3.3	0.286	:

Print Time/Dele: 11/07/2012 17:

STAAD.Pro for Windows 20.07.02.15



-					TPL40581	sheel No a 152	Rev R4b-FAB
Softwar	licensed to Transerve	Pie Lut			Panwind speed 32.	5 m/s	
	ia Swimming Poo				Raf Fabric R5		
					BY TSM	Date17-Dec-11 Chd	TSM
tent Majlis Perb	andaran Kuantan				File Q326-KSP-R4		
(20) 700 M		al and a					
		Checks Cont					
HIDHAEA TA		CRITICAL COND/	10.110/ HI	LOADING/ LOCATION			
1167 ST P	77.24 C	M-4.7 (C) -0.27	0.311 0.00	204 0.00			
1168 ST P	1989.114.0 PASS 72.29 T	85-4.8.2.2 -0.43	0.300	204			
	199.124.0 PASS #6.76 C	85-4.7 (C) -0.44	0.345	204			
1170 57 8		*****	0.320	0.00			
			0.00	0.00			
1171 ST F1	19.114.0 7355 19.99 C	85-4.7 (C) -0.12	0.363	204			
	P114.3X4.5 PASS 48.01 C	85-4.7 (C) -0.45	0.124 0.00	204			
1173 ST PI	F83.1X4.0 PASS	85-4.8.2.2	0.189	204			
1174 ST PI	P49.1X4.0 PASS 41.23 C	85-4.7 (C) -0.34	0.169	204			
1175 ST P1	P89.1X4.0 PASS 39.50 T	83-4.4.2.2 -0.22	0.163	204			
1176 57 11	19.1X4.0 PASS	85-4.7 (C)	0.00	204			
	10.53 C		0.00	2.02			
	48.75 C	85-4.7 (C) -0.10	6.00	3.59			
	114.3x4.5 PA35 63.41 C	85-4.8.3.3.3 -0.65	0.244 0.31	!			
1175 ST PI	49.1X4.0 PASS 75.88 C	85-4.7 (C) -0.32	0.305	205			
	49.3X4.0 PASS 67.66 T	#5-4.8.2.2 -0.37	0.277	205			
1141 ST P10	19.1X4.0 PASS 72.40 C	85-4.7 (C) -0.31	0.291	205			
	19.3X4.0 PASS 59.59 T	85-4.0.2.2	0.253	205			
	19.1X4.0 PASS	85-6.7 (5)	0.00	0.00			
	66.66 C	-0.23	0.00	1.95			
1184 57 919	40.60 T	85-4.8.2.2 -0.38	0.214 0.00	205			
1145 ST PIP	19.1X4.0 PASS 61.99 T	85-4.8.2.2 -0.23	0.240 0.60	204			
	19.1X4.0 PASS 37.64 T	85-4.8.2.2	0.173	205			
1187 ST PIP	9.1X4.0 PASS	85-4.4.3.3.1	0.243	205			
	49.30 C	-0.03	0.23				
	19.1X4.0 PASS 38.55 C	83-4.8.3.3.3 -0.10	0.198	205			

2					Job No TPL40581	Shint No a 153	Rev R4b-FAB
2	licensed to Transerv	Ball			Panwind speed 32.5	i m/s	
	la Swimming Poo				Ref Fabric R5		
					By TSM	Dale17-Dec-11 Ch	TSM
Mailis Perb	andaran Kuantar					-Deg.std Dalemme 10-	
					4020101101	-Deg.ata 100	10-2012 10,43
ALL UNITS ARE	- XX HETE IVN	Checks Cont					
	rχ	/ CUITICUL COND/ HT	HATIO/	LOADING/			
	1985.124.0 PASS 46.74	-0.16	0.179 0.00	204 0.00			
1190 ST P	1989.1X4.0 PASS 46.64	85-4.0.3.3.3 -0.17	0.232	202			
1191 ST P	1949.114.0 PASS (6.14	85-4.8.2.2 -0.26	0.190	202			
3192 ST P	1989.1X4.0 PASS 40.77 (	83-4.8.3.3.3 -0.18	0.208	:			
1193 ST P1	P#9.124.0 PASS	85-4.8.2.2	0.199	202			
1154 57 91	P114.3X4.5 PASS	#5-4.8.2.2 -0.74	0.165	207			
	P89.124.0 PASS 19.21 T	85-4.4.2.2	0.031	205			
	789.114.0 PASS 42.21 T	85-4.8.2.2	6.161	204			
	P89.124.0 PASS	85-4. 8. 7. 7	0.00	1.95			
	23.74 T	-6.26	0.00	204			
	42.91 T		0.00	1.95			
	49.71 C	-0.55	0.00	204			
		85-4.8.2.2 -0.24	0.275 0.00	204			
	49.85 C	85-4.8.3.3.1 -0.64	0.273 6.38	104			
	49.1X4.0 PASS 79.36 T	85-4.8.2.2 -0.32	0.310	204			
	49.124.0 PASS 70.34 C	85-4.7 (C) -0,48	0.203	204			
	89.1X4.0 PASS 85.48 T	85-4.8.2.2	0.332	204			
1205 ST P1P	19.124.0 PASS 81.28 C	85-4.7 (C) -0.45	0.327	204			
1206 ST PIP	99.1X4.0 FASS 51.50 T	85-4.6.2.2 -0.45	0.373 0.00	204			
	19.114.0 PASS	85-4.7 (C) -0,45	0.327	204			
	19.114.0 PASS 84.17 C	85-4.7 (C) -0.12	0.337	205			
1209 ST PIP	114.384.5 PASS 39.70 C	85-4.8.3.3.3	0.143	3			
1210 ST PIP		85-4.4.2.2	0.172	205			
	40.38 T	-0.28	0.00	0.00			

STAAD.Pro for Windows 20.07.02.15

al Dam EE al 1

1-1-1					TPL40581	Sheet No	a 154	Rev R4b-FA
$\bigcirc$	ire licensed to Transerve I				Partwind speed 32	Emis		
	elia Swimming Pool	ria Lid			Ref Fabric R5	.o mvs		
					BY TSM	Dale17-D	Inc.11 Chd	TSM
Client Mailis Pe	bandaran Kuantan				File Q326-KSP-R4			
india i a	Pariot an recentari					0-0 89.510	10-30	A-2012 16:4.
	ign (Track 0) C							
	ABLE MESULT/			LOADING/				
		нт	81	LOCATION				
1211 57	PIP89.114.0 PASS 38.23 C	83-4.7 (C) -0.30		205 2.02				
1212 57	P1P19.114.0 PASS 35.42 T	85-4.8.2.2 -0.19	0.146	205				
1213 57	P1P49.1X4.0 PASS 1.73 C	85-4.8.3.3.3 -0.02		:				
	PIP114.384.5 PASS 46.16 C	85-4.1.3.3.3	0.105	·····.,				
	P1P49.1X4.0 PASS	15-4.1.3.3.3	0.278	······				
	\$6.93 C	-0.11	0.23					
1214 57	67.32 C	85-4.7 (C) -0.34	0.271 0.00	204				
1217 57	64.45 T	85-4.8.2.2 -0.37	0.266	204 0.00				
1218 57	PIP49.124.0 PASS 47.97 C	85-4.7 (C) -0.30	0.273	204				
	11949.114.0 PASS 57.60 T	85-4.8.2.2	0.241	204				
1220 ST	11949.114.0 PASS	85-4.4.2.2 -0.25	0.256	205				
	11989.124.0 PASS		0.207	204-				
1222 57	1949.1X4.0 PA35 55.58 C	85-4.8.3.3.3 -0.17	0.273 0.20	204				
	1949.1X4.0 PASS 38.41 T	85-4.8.2.2 -0.32	0.171 0.00	204				
1224 ST 1	1949.124.0 PASS 52.68 T	85-4.8.2.2	0.203	205				
	1949.1X4.0 PASS 55.46 T	\$5-4.4.2.2	0.209	201				
			0.00	1.95				
1226 57 9	1989.1X4.0 PASS 42.40 C	85-4.8.3.3.3 -0.11	0.209 0.17	104				
1227 57 9	1989.124.0 PASS 69.45 T	85-4.8.2.2 -0.35	0.280	201 0.00				
1228 57 .		85-4.7 (C) -9.33	0.271 0.00	201				
1229 ST P	1989.184.0 PASS 70.47 T	85-4.4.2.2 -0.36	0.285	201				
		85-4.7 (C)	0.283	201				
	P114.384.5 PASS	85-4.8.2.2	0.228	703				
	75.06 7	-0.64 AMHER 1.1 -0.22	0.00	0.00				
1232 57 8	12.64 C		0.20					

			Job No TPL40581	Sheel No	a 156	Rev R4b-FAB
5			Partwind speed 32.			
ab Tile Wisma Bella Swimming Pool			Ref Fabric R5	5 mvs		
			BY TSM	Delt17-D	en-11 Chd	TSM
Majlis Perbandaran Kuantan		31	Fle Q326-KSP-R4			
						1 2012 10,40
Steel Design (Track 0) Checks Cont						
ALL UNITS ARE - IN HETE (UNLESS OTHERWISE NOTED)						
HDIBER TABLE RESULT/ CRITICAL COND/ FX HY	RATIO/ HI	LOCATION				
1255 ST PIPES.1X4.0 PASS 85-4.7 (C) 71.78 C -0.31	0.288	205				
	0.252	205				
1257 ST PIPER.1X4.0 PASS 85-4.7 (C)	0.267	205				
66.48 C -0.23	0.00	1.95				
1258 ST P1P89.1X4.0 PASS 85-4.8.2.2 49.29 T -0.37		205				
1259 ST PIPES.1X4.0 PASS 85-4.8.3.3.3 48.91 C -0.15	0.38	105				
1240 ST PIPHD.1X4.0 PASS 85-4.4.2.2 34.25 T -0.35	0.174	205 0.60				
1261 ST P1P99.1X4.0 PASS 85-4.8.3.3.3 49.66 C -0.13	0.241 0.18	205				
1262 ST P1P49.1X4.0 PASS 85-4.8.2.2 38.26 T -0.18	0.152 0.00	209				
1243 37 P1P89.1X4.0 PASS 85-4.7 (C) 39.50 C -0.03	0.161	205				
1264 ST PIPPS.1X4.0 PASS 85-4.8.3.3.3 37.29 C -0.11	0.17	<u>:</u>				
44.32 T -0.25	0.182	202				
1246 ST PIPES.1X4.0 PASS B5-4.7 (C) 47.95 C -0.26		202				
1267 57 P1P89-1X4.0 PASS 85-4.8.2.2 48.65 7 -0.24	0.196	202				
1268 ST P1P114.314.5 PASS 85-4.8.2.2 (9.78 7 -0.12	0.149	209				
1269 ST PIP49.1X4.0 PASS 85-4.8.2.2	0.084	205				
	0.00					
	0.137	205				
21.71 T -0.25	0.105 0.00	205				
1272 57 F1949.3X4.0 FASS 85-4.4.2.2 52.44 T -0.11	0.193	204 1.95				
1273 57 P1P114.3X4.5 PASS 85-4.8.2.2 28.65 7 -0.41	0.110 0.00	9				
1274 57 P1P89.1X4.0 PA55 85-4.6.2.2 60.81 T -0.18	0.230	204				
1275 ST P1P49.1X4.0 PASS 85-4.7 (C) 49.54 C -0.41	0.199	204				
1276 ST PIPHP.1X4.0 PAIS 85-4.8.3.3.3 56.22 C -0.22	0.279 0.15	?				

TAAD D. /..

Pdel Time/Dale: 11/07/2012 17:2

2			Job No TPL40581	Sheel No a 157	Rev R4b-
Software licensed to Transervo Pie Lid			Partwind speed 32.5	i m/s	
sh Title Wisma Bella Swimming Pool			Rel Fabric R5	i iivs	
			By TSM	Dale17-Dec-11 C	TSM
Nent Majils Perbandaran Kuantan					
				10	00-2012 10
Steel Design (Track 0) Checks           ML 0917 AD - BI WET OWERS DWE           HOMEN TABLE NEWS COMESS DWE           1201 ST PURS, NAME           1205 ST PURS, NAME	What avertup: We have been been been been been been been be	LEADEDNEY 1002 41100 1.33 244 1.33 244 1.35 244 1.35 244 1.35 245 3.54 245 3.54 245 3.54 245 3.54 245 3.54 245 3.55 3.55 3.5	Pa 0228-KSP-R45	Deg.atd (Deta/Tore 10-	Jul-2012 16
1284 ST PIP114.3X4.5 PASS \$5-4.3		3.00			
1289 ST FIF89.1X4.6 FASS 85-4.8 61.43 C -	4.72 0.15	2			
1230 ST PIPES.1X4.0 PASS 85-4.7 70.99 C	(C) 0.286 0.37 0.60	204			
1291 57 71P49.1X4.0 PASS #5-4.#		204			
(4.67 T -		0.00			
1292 ST P1P89.1X4.0 PASS #5-4.7		284			
1293 57 FIF49.1X4.0 FASS 85-4.8 60.45 7	0.36 0.00	204 0.00			
1234 ST P1P45.1X4.0 PASS 85-4.8	.2.2 0.275 0.27 0.00	205			
1285 ST PIPER.124.0 PASS 85-4.8	.3.3.3 0.307	205			
55.06 C -	0.30 0.23				
1296 ST PIPES.1X4.0 PASS 85-4.8		205			
1297 ST PIP49.1X4.0 PASS 85-4.4. 43.74 C -4	0.25 0.21	?			
1258 ST P1P45.1X4.0 PASS 85-4.8		205			

TAAD, Pro for Wi

dows 20 07 02

~			TPL40581	sheet No a 158	Rev R4b-FAB
Software Econsed to Transerve Pie Lid			Parlwind speed 32.5	ī m/s	-
We Wisma Bella Swimming Pool			Ref Fabric R5		
			BY TSM	Dale17-Dec-11 Chd	TSM
Majils Perbandaran Kuantan			File Q326-KSP-R45	-Deg.std Date/Time 10-Ju	-2012 16:43
Steel Design (Track 0) Checks					
ALL UNITS ARE - NY HETE HUNLESS OTHER HENRER TABLE RESULT/ CRITIC TX		LOADING/			
1255 ST P1965.124.0 PASS 85-4.	.*.2.2 6.279	201			
	-0.21 0.00	1.95			
1300 ST PIP49.1X4.0 PASS 85-4. 67.75 C	-0.55 0.273	201			
93.12 T	0.2.2 0.379 -0.50 0.00	203			
1302 ST PIPSP.1X4.0 PASS 85-4.		202			
1303 ST PIP89.1X4.0 PASS 85-4.	.4.2.2 0.368	201			
90.94 T	-0.47 0.00				
1304 ST P1P49.1X4.0 PASS 85-4. 91.31 C	7 (C) 0.367 -0.35 0.60	201			
1305 ST P1P114.384.5 PASS 85-4. 98.74 T	1.2.2 0.263 -0.76 0.00	201 0.00			
15.23 C	8.3.3.3 0.074 -0.08 0.25	208			
1307 ST P1P#9.1X4.0 PASS 85-4.	8.2.2 0.155 -0.12 0.00	205			
1308 ST P1P89.124.0 PASS 85-4.	******	205			
1309 ST PIP49.1X4.0 PASS 85-4.1	0.2.2 0.205	205			
1310 ST P1P114.314.5 PASS 85-4.	7 (5) 0.112	1.95			
43.43 C	-0.00 0.00	1.95			
(2.19 7 -	-0.19 0.00	1.95			
1312 57 PIP45.1X4.0 PASS 85-4.7 52.13 C		205			
1313 ST PIPES.1X4.0 PASS 85-4.4 42.25 C	0.317 -0.21 0.11	204			
1214 ST PIPES.184.0 PASS 85-4.7		205			
1315 ST #1949.1X4.0 PASS 85-4.7 73.98 C		204			
1314 ST P1P89.1X4.0 PASS 85-4.8		204			
1217 5T PIPEP.1X4.0 PASS 85-4.7	(C) 0.341	204			
		0.00			
76.10 T -	0.41 0.00	0.00			
1319 ST PIP49.1X4.0 PASS 85-4.7 89.44 C -		204 0.00			
1326 ST P3P314.3x4.5 PASS 85-4.8					

Print Time/Date: 11/07/2012

Print Run 54 of 104



Point Blues Ed. ed. 154

2	TPL40581	a 155	Rev R4b-FAB		
Software Reased to Transerve Pie Lid	Patwind speed 32.5 m/s				
Job Tille Wisma Belia Swimming Pool	Rel Fabric R5				
	By TSM Datr17-Dec-11 Chd TSM				
Cleni Majlis Perbandaran Kuantan	File Q326-KSP-R4b-D	eg.std Dete/Time 10-	Jul-2012 16:43		

### Steel De an (Track 0) Checks Cont

	sign (T		hecks Cont		
1013128	TABLE	NESULT/	CRITICAL CONS/ HT	RATIO/ HZ	LOADING/
1233 51	P1749.13	4.0 PASS 38.20 T	85-4.8.2.2 -0.10	0.143 0.00	205 1.95
1224 51	P1P49.13	4.0 PASS 23.51 C	85-4.7 (C) -0.32	0.095	205
1235 51	P1P19.1X	4.0 PASS 45.62 T	85-4.4.2.2 -0.10	0.168	205
1236 51	PIP114.3	X4.5 PASS 27.61 T	35-4.1.2.2 -0.65	0.105 0.00	204
1237 57	P1919.1X	4.0 PASS 51.81 C	85-4.8.3.3.3 -0.20	0.256 0.13	204
1238 57	P1989.1X	4.0 PASS 40.55 T	85-4.8.2.2 -0.34	0.180 0.00	204
1239 57	P1969.1X	4.0 PASS 34.95 C	85-4.8.3.3.3 -0.22	0.273 0.14	:
1240 ST	P1989.1X		85-4.8.2.2 -0.37	0.232	204
1241 57	P1209.1X	4.0 PASS 74.11 C	85-4.7 (C) +0.25	0.258 0.00	204
1242 57	PIP69.1X	1.0 PASS 61.39 T	85-4.4.2.2 -0.42	0.267	204
1243 ST	PEP49.12	1.0 PASS 83.45 C	85-4.7 IC  -0.42	0.336 0.00	204 0.00
1244 ST	P1209.1X	1.0 PASS 75.92 T	85-4.8.2.2 -0.41	0.305 0.00	204
1245 57	PIP49.1X	0 PASS 87.65 C	85-4.7 (C) -0.13	0.351 0.00	204
1246 ST	PIP114.20	4.5 PASS 47.70 C	85-4.7 (C) -0.44	0.123	204
1247 ST	P2909.1X4		B5+4.0.2.2 -0.32	0.191 0.00	204 0.00
1248 ST	PIP89.1X4	.0 PASS 41.97 C	85-4.7 (C) -0.35	0.172 8.00	204 2.02
1249 57	P1249.1X4	.0 PASS 40.33 T	85-4.8.2.2	0.165	204
1250 57	P1P89.1X4	.0 PASS 10.56 C	85-4.7 (C) -0.17	0.643 0.00	204 2.02
1251 ST	PIP114.3X	4.5 PASS 49.40 C	85-4.7 (C) -0.11	0.142	264 3.59
1252 ST	P1P114.3X	4.5 PASS 73.68 T	85-4.8.2.2 -0.77	0.223 8.00	205
1253 57	P1P89.1X4	0 PASS 61.39 C	85-4.8.3.3.3 -0.33	0.303 0.25	105
1254 ST	P3P09.3X4	4 PASS	85-4.4.2.2	0.273	205

2	TPL40581 Sheet No a 159					
Software licensed to Transerve Pie Ltd	Panwind speed 32.5 m/s					
Jeb Tite Wisma Bella Swimming Pool	Raf Fabric R5					
	By TSM Dele17-Dec-11 Chd TSM					
Clisht Majils Perbandaran Kuantan	File Q326-KSP-R4b-Deg.std DeterTime 10-Jul-20	12 16:43				

L UNITS	NR - 101	-	IS OTHERWISE NOTED	1	
ISER .	TABLE	ACSULT/	CRITICAL COND/	NATIO/	LOCATION
1321 5	17 91999.13	4.0 PASS 42.19 T	85-4.4.2.2 -0.32	0.184	204 0.00
		4.0 PASS 40.33 C	85-4.7 (C) -9.34		204
1323 5	T PIPOD.1X	4.0 PASS	85-4.8.2.2		204
1324 5	T 91949.1X	4.0 PASS		0,047 0,00	204
	T P1P114.3		85-4.7 (C) -0.12	0.173 0.00	
		4.5 PASS 60.47 C	85-4.8.3.3.3 -0.57	0.227	:
	T #1#49.1X	4.0 PASS 70.58 C	85-4.7 (C) -0.25	0.284	205
	T PIPES.1X	PASS	85-4.7 (C)	0.258	204
	T PIPUS.1X		85-4.4.2.2 -0.30	0.285	204
	F P3P89.1X		85-4.8.2.2 +0.33		
1331 51	F PIPPS.1X		85-4.7 (C) -0.30		205
1332 57	F PIPES.1X4		85-4.8.2.2 -0.43	0.253	205
1333 57	PIPES.1X4	.0 FASS 67.04 C	85-4.7 (C) -0.21	0.270	205
1334 51		.0 PASS 27,72 C	85-4.8.3.3.3 -9.24	0.212	
			85-4.7 (C) -0.14		
			85-4.4.2.2 -0.16		*******
			85-4.8.3.3.3 -0.05		
	P1P89.1X4	**********	-0,03 85-4.4.2.2 -0.19		********
339 ST	PIP49.1X4	.0 PASS	-0.19 85-4.7 (C) -0.32	0.191	
	P1789.124	47.42 C	-0.32 85-4.8.2.2 -0.25	0.211	
					201
*****	*******	0 PAES 50.71 C			1.95
342 57	P3P114.3X	51.48 T	85-4.8.2.2 -0.75	0.171	207

Print Time/Date: 11/07/2



K	TPL40581 Sheet No a 160 Rev R4b-FAB
Software licensed to Transerve Pie Ltd	Partwind speed 32.5 m/s
Isb Tile Wisma Bella Swimming Pool	Rel Fabric R5
Cleni Mallis Perbandaran Kuantan	
Majis Perbandaran Kuantan           Steel Design (Track 0) Checks Cont           All WIS AN ON STEE WISSIE STEELED S	133       24       25       33       34
1361 ST F1F49-1X4.0 PASS 85-4.7 (C) 0.048 11.77 C -0.06 0.00	205 2.02
1342 ST P1P114.3X4.5 PA55 85-4.7 [C] 0.145 44.47 C -0.13 5.00	242 3.59
1363 ST PIP49.1X4.0 PASS B5-4.0.3.3.3 0.289 60.12 C -0.17 0.20	2
1264 ST PIPES.1X4.0 PASS 85-4.7 (C) 0.283 70.36 C -0.37 0.00	204

STAAD Pro for Windows 20.07.02.1

2			Job No TPL40581	Sheet No	a 161	R4b-FAB
Software Ecenard to Transerve Pie Ltd			Parlwind speed 32	5 m/s		
The Wisma Bella Swimming Pool			Ref Fabric R5			
			By TSM	Dale17-D	er.11 DA	TSM
Majlis Perbandaran Kuantan			Fa Q325-KSP-R4		Data/Time 10-J	
			and the second	0.009.010	10-0	UP2012 10.45
Steel Design (Track 0) Checks Cont.	100					
ALL UNITS ARE - IN HETE (UMLESS OTHERWISE NOT						
HENDER THELE RESULT/ CRITICAL COND.	/ RATIO/	LEADING/				
EX HY	11	LOCATION				
1345 57 PIP49.1X4.0 PASS 85-4.8.2.2	0.279	204				
<b>68.45 T</b> -0.37	0.00	0.00				
1346 ST PIP65.124.0 PASS D5-4.8.3.3.3 70.16 C -0.21		204				
***************************************						
1347 ST FIFE9.1X4.0 PASS 85-4.8.2.2 60.52 T -0.36	0.251 0.00	204 0.00				
	0.266	205				
1368 ST PIPE9.124.0 7A53 85-4.0.2.2 60.49 T -0.26	0.00	0.00				
1369 ST PIPP9.1X4.0 PASS 85-4.8.2.2	0.214	204				
50.13 T -0.35	0.00	0.00				
1370 ST P2P49.1X4.0 PASS 85-4.4.3.3.3	0.281	204				
55.54 C -0.13	6.23					
1371 ST P1989.1X4.0 PASS 85-4.8.2.2 40.50 T -0.31	0.177	204				
***************************************						
1372 ST PIPOS.124.0 PASS 85-4.8.3.3.3 45.04 C -0.13	0.247	204				
	0.278					
1373 ST FIF49.1X4.0 FASS 85-4.0.2.2 74.20 T -0.21	0.278	201 1.95				
1374 ST PIPES 184.0 PLAS 85-4.7 (2)	0.272	261				
67,60 C -0.59	0.00	1.95				
1375 ST P3789.184.0 PASS 85-4.8.2.2	0.378	201				
52.54 7 -0.49	0.00	0.00				
1376 ST P1P19.1X4.0 PASS 85-4.7 [C] 90.40 C -0.50	0.365	201				
	•••••					
1377 ST FIF49.1X4.0 PASS 85-4.8.2.2 30.67 7 -0.47	0.367	201 0.00				
1376 ST P1789.1X4.0 PASS 85-4.7 (C)	0.366					
1376 ST P1789.1X4.0 PASS 85-4.7 (C) 91.04 C -0.25	0.366	201				
1379 ST PIPI14.3X4.5 PASS 85-4.4.2.2	0.282	201				
98.36 T -0.77	0.00	8.00				
1380 ST P1P89.1X4.0 PASS 85-4.8.3.3.3	0.074	205				
13.89 C -0.13	0.23					
1301 3T P1P09.1X4.0 PASS 85-4.4.2.2 39.33 T -0.10	0.146	205				
1382 ST P1P99.1X4.0 PASS 85-4.7 IC) 24.75 C +0.34	0.100	205 .				
	0.196	285				
1383 ST P3P89.124.0 PASS 85-4.8.2.2 53.21 T -0.12	0.154	1.95				
1384 ST F18114.384.5 PAGS 85-4.8.2.2	0.106					
24.32 7 -0.55	0.00	1.95				
1385 ST PIPEP.1X4.0 PASS 85-4.0.3.3.3	0.242	204				
48.89 C -0.19	0.13					
1386 ST PIP89.3X4.0 PASS 05-4.7 [C] 49.68 C -0.40	0.201	205				

1					TPL40581	Sheel No	a 162	
$\bigcirc$					Partwind speed 3	25 m/s		
	e licensed to Transerve P ella Swimming Pool	te Ltd			Ref Fabric R5	2.0 1125		
					By TSM	Dale17-D	Inc.11	Chd TS
Clent Majlis Per	handaran Kuantan				File Q325-KSP-R			
					different in	10-0-03.010	1	10-00-2
Steel Desi	ign (Track 0) C	hecks Cont	2					
ALL UNITS AN	E - KN HETE IUNLE	SS OTHERMISE NOTE	01					
HDGER T	ABLE RESULT/	CRITICAL COND/	AATIO/	LOADING/				
				*******				
1387 37	PIPES.1X4.0 PASS 54.55 C	-0.21	0.273 0.15	<u> </u>				
	PIP49.1X4.0 PASS	85-4,7 (C)	0.237	205				
	59.00 C	-0.41	0.00	1.95				
1385 ST 1	73.54 C	85-4.7 (C) -0.24	0.296	204				
				*******				
1390 ST 1	44.11 T	85-4.8.2.2	0.284	204				
	PIP45.184.0 PASS	85-4.7 (C)		204				
	64.21 C			0.00				
		\$5-4.8.2.2	0.308	204				
	75.51 7		0.00	0.00				
1353 ST #	1149.1X4.0 PASS	#5-4.7 (C) -0.11	0.356	204				
	19114.3X4.5 PASS 38.90 C	85-4.4.3.3.3 -0.34	0.145	:				
	1749.1X4.0 PASS	85-4.8.2.2	0.184	204				
	42.52 T	-0.33	0.60	0.00				
	1949.1X4.0 PASS	85-4.7 (C) -0.34	0.165	204				
			*******					
	1943.114.0 PASS 25.75 C		0.156 0.17	205				
1194 67 1	1989.1X4.0 PASS		0.047	204				
	11.43 C	-0.14	0.00	2.02				
1399 ST P	17114.384.5 PASS 47.16 C	85-4.7 (C) -9.12	8.174	:				
		-9.12						
1400 ST P	19114.384.5 PASS 71.41 T	-0.71	0.215	205				
		85-4.7 (C)	0.285	205				
	1969.114.0 PASS 78.86 C	-0.30	0.00	1.95				
	1985.114.0 PASS 53.34 C	85-4.4.3.3.3	0.272					
	53.34 C	-0.17	0.25	· · · ·				
1403 ST P	1769.124.0 PASS 69.40 T	85-4.8.2.2	0.274	204				
				*******				
1404 37 8	1989.3X4.0 PASS 47.37 T	85-4.0.2.2 -0.33	0.270	205				
	1989.1X4.0 PASS 72.86 C	85-4.7 (0)	0.293	285				
	72.86 C	-0.31	¢.00	1.95				
1406 ST PI	1985.1X4.0 PASS 59.19 T	85-4.8.2.2	0.255	205				
•								
1407 ST PI	67.78 C	85-4.8.3.3.3 -0.16	0.27	205				
	1789.184.0 PASS 46.72 T	85-4.4.2.2	0.205	205				
		-0.38		0.00				

4			TPL40581	Sheel No	a 164	R4b-FAB
Selfware licensed to Transervo Pie Lid			Patwind speed 32	5 m/r		
No Tile Wisma Bella Swimming Pool			Ref Fabric R5			
			By TSM	Dale 17-D	ec-11 Chi T	SM
Sient Majils Perbandaran Kuanlan			Fle Q326-KSP-R4			2012 16:43
Steel Design (Track 0) Checks Cont ALL WITE ARE - 104 HETE INVLESS OTHERWISE NOTED	100000					
ун хt	NAT10/ HZ					
37.67 C -0.28	0.132 0.19	:				
36.05 T -0.19	0.146	205				
34.92 C -0.25	0.143	205 2.02				
	0.125	262				
	0.649	205				
1436 ST PIP114.3X4.5 PASS 85-4.8.3.3.3	0.180 0.10	12				
1437 ST PIPEB.1X4.0 PASS S5-4.8.3.3.3 60.82 C -0.17	0.285	?				
1438 ST PIPES.1X4.6 PASS 85-4.8.2.2	0.278	205				
	0.271	204				
	0.344	204				
•••••••••••••••••••••••••••••••••••••••	0.248	205				
1442 ST PIP09.1X4.0 PASS 85-4.4.2.2	0.278	205				
49.24 T -0.27	0.00	0.00				
56.83 C -0.34	0.22					
(4,65 C -0.39						
36.90 T -0.38	0.00	205				
59.04 T -0.17	0.218 0.00	201 1.55				
\$3, 30 C -0.44	0.214 0.00	201				
1445 ST PIPES.1X4.0 PASS 85-4.8.2.2 0 71.62 T -0.37	0.290	201				
	0.282	201				
	0.293	201				
1452 ST PIPEP.1X4.0 PASS 85-4.7 (C) 0 73.62 C -0.29	0.254	201				

K		TPL40581	sheet No a 165	R45-FAB
Sofeware Transed in Transerve Pie Lid		Parlwind speed 32.5	m/s	
es Tille Wisma Bella Swimming Pool		Ref Fabric R5		
		By TSM	Dale17-Dec-11 C	TSM
<sup>zient</sup> Majils Perbandaran Kuantan		File Q326-KSP-R4b-	Deg.std Data/Time 10-	Jul-2012 16:43
Amerika Muljik Perkandaram Kujentan           Steel Dasian (Track 0) Checks Cont All 9972 MC - 99 KET BOKES 6700054 97000 4870           Nones, Yank KE, Mark J, Status KETAJ, S	LECOTION LECOTI			Jul-2012 16:43
1471 ST PIP89.1X4.0 PASS 85-4.8.2.2 0.161 39.20 T -0.22 0.00				
1472 ST P1P89.124.0 PASS 85-4.7 (C) 0.047	204			
10.50 C -0.16 0.00	204			
47.47 C -0.10 0.00	205			
1474 ST PIPI14.244.5 PAIS 834.8.2.2 0.225 74.02 T -0.78 0.00	205			

$\mathcal{D}$						TPL40581	Sheel No	a 166		Rev R4b-FAB
$\bigcirc$	Itware licensed to	Transacon P	te Lid			Partwind speed 32	.5 m/s			
	a Bella Swimm					Ref Fabric R5				
						By TSM	Date 17-D	ec-11	Che TS	м
Hent Majils	Perbandaran I	Kuanlan				File Q326-KSP-R4	b-Deg.sld	DeterTime	10-Jul-2	012 15:43
202 202			2 2 2 2 2							
			hecks Cont							
HEHBER			CRITICAL COND/		LOADING/					
				HZ	LOCATION					
1475 1	FT P1989.184.	0 PASS	85-4.8.3.3.3	0.363	205	2				
	FT PIPS9.1X4.	46.93 T	85-4.8.2.2	0.274 0.00	205 0.00					
	IT P1P49.1X4.		85-4.7 (C)	0.290	205					
		72.05 C	-0.30	0.00	1.35					
1478 5	T F1P89.3X4.	0 FA35	85-4.8.2.2	0.252	205					
14/9 3	T PIPes.1x4.	66.59 C	85-4.7 (C) -0.23	0.250	205					
	T FIF89.184.	0 7355	85-4.4.2.2	0.213	205					
			-0.37	0.00	0.00					
1481 5	T #1#89.1X4.	0 PASS 54.64 C	85-4.0.3.3.3	0.248	205					
				********						
1462 5	T P1P89.1X4.	0 FASS 37.83 T		0.172	205					
1483 5	T PIP45.184.	. PASS	81-4.4.3.3.3		205					
		49.49 C	-0.10	0.19						
	T P1P89.1X4.	34.71 C	85-4.8.3.3.3 -0.05	0.176	10					
1405 5	T P1P89.1X4.0	39.56 C	MS-4.7 (C) -0.65	0.153	205					
1486 5	T PIPES.1X4.0	PASS	NS-4.7 (C)	0.169	202					
		42.68 C	-0.16	0.00	0.00					
1487 5	T P1P89.1X4.0	10.65 T	85-4.4.2.2	0.168	202					
*******				*******						
	T P1P89.1X4.0	45.34 C	85-4.7 (C) -0.24	0.102	202					
	F PIPS9.1X4.0	PASS	85-4.8.3.3.3	0.201	203					
		37.70 C	-0.20	0.16						
1450 5	F PIP114.3X4.	5 PASS	85-4.8.2.2	0.161	207					
	T P1P89.1X4.0		#5-4.1.2.2 -0.23	0.095	205					
	PIPES.134.0	PASS	85-1.7 101	0.149	205					
		36.91 C	-0.68	0.60	0.00					
1493 55	FIP89.1X4.0	7355 24.83 T	NS-4.8.2.2 -0.25	0.117	205					
1494 51	F \$1989.1x4.0	59.24 T	-0.14	0.225	204					
1495 51	F PIP114.3X4.	S PASS	85-4.4.2.2	0.121	,					
		33.67 T		0.00	1.95					
1496 51	P1F89.1X4.0	1935	85+4.8.2.2	0.258	204					
		*/.84 7	-0.22		1.55					
			2 10 10 10						_	
ni Tima/Dale: 11/0	Priz012 17:29		S	TAAD, Pro fe	r Windows 20.0	07.02.15			Pris	Run 55 of 15

142 ST P199.1K4.0 PAS 34.37 S 142 ST P199.1K4.0 PAS 34.37 S 143 ST P199.1K4.0 PAS 143 ST P199.1K4.0 PAS 143 ST P199.1K4.0 PAS 143 ST P199.1K4.0 PAS	-0.47 B5-4.8.2.2 -0.46 B5-4.7 (C) -0.42 B5-4.7 (C) -0.13	0.347 0.00 0.315 0.00	294 0.00 204 1.95 205 0.00				
1428 ST P1P49.124.0 PA35 85.26 T 1429 ST P1P49.124.0 PA55 79.18 C 1428 ST P1P49.124.0 PA55 79.18 C	85-4.8.2.2 -0.46 85-4.7 (C) -0.42 85-4.7 (C) -0.13	0.347 0.00 0.313 0.00 0.351 0.00	204 0.00 204 1.95 205 0.00				
83.26 T 1425 ST PIP45.134.0 PASS 79.18 C 1438 ST PIP45.334.0 PASS 47.49 C	-0.46 B5-4.7 (C) -0.42 B5-4.7 (C) -0.13	0.315 0.00 0.351 0.00	204 1.95 205 0.00				
1429 ST PIP49.1X4.0 PASS 19.18 C	85-4.7 (C) -0.42 85-4.7 (C) -0.13	0.319 8,00 0.351 0.00	204 1.95 205 0.00				
1438 ST PIPES.3X4.0 PASS 47.45 C	85-4.7 (C) -0.13	0.351	205				
47.49 C	-0.13	0.00	0.00				
	-0.13	0.00					
Ima/Date: 11/07/2012 17:29	5	TAAD.Pro for	Windows 20.	07.02.15		P	fint Run 65 c
-				Job No	Sheet No		Rev
<				1PL40581	a	107	R4b-FA
Software licensed to Transerve A	'ie Lid			Partwind speed 32.	5 m/s		
We Wisma Bella Swimming Pool				Ref Fabric R5			
				By TSM	Dale 17-Dec-1	1 Che TS	-
	8	Cohung Second To Second To Life	Cohung Tarasad ta Toracone Pa Lut	Cohuen licensed to Transme Pa Lid	Justini TPL400581     Privation Pa Ltd     Privatio Pa Ltd     Privation Pa Ltd     Privation Pa Ltd	Justinia The Addition of	Jub No.         Jub No.           TPL40581         Exet Mo.           Softwart Texase Pa Lid         Period speed 32.5 m/s           We Wana Bela Swimming Peck         Mr. Fabric R.S.



R		Rev R4b-FAB
Software Deensed to Transerve Pile Lid	Patwind speed 32.5 m/s	
Jeb Title Wisma Bella Swimming Pool	Ref Fabric R5	
	By TSM Date 17-Dec-11 Chd TSM	
Clent Majis Perbandaran Kuantan	File Q326-KSP-R4b-Deg.std Date/Time 10-Jul-201	2 16:43

### Stee

Rev RAD.EAD

			hecks Cont	4	
Diada	THELE	NESULT/	CASTICAL COND/	AATIO/ HZ	LOADING/
1409 51	P1989.1X	.0 PASS 57.71 C	85-4.7 (C) -0.15	0.232 0.00	205
1410 57	P1989.1X	1.0 PASS 49.39 T	85-4.1.2.2 -0.17	0.185 0.05	201 0.00
1411 57	P1989.1X4	47.35 C	85-4.7 (C) -0.08	0.190 0.05	205
1412 57	P1P69.1X	.0 PASS 50.84 T	85-4.4.2.2 -0.19	0.197	201
1413 57	P1989.1X	0 PASS 47.64 C	83-4.7 (C) -0.32	0.192 0.00	201 1.95
1414 37	PIP45.1X4	.0 PASS 52.48 T	85-4.8.2.2 -0.25	0.212 0.00	201
1415 ST	P1209.1X4	.0 PASS 50.63 C	85-4.7 (C) -0.24	0.204 0.00	201 1.95
1416 57	P1P114.33	4.5 PASS 50.85 T	85-4.1.2.2 -0.78	0.173 0.00	209
1417 ST	PIP89.1X4	.0 PASS 23.22 T	85-4.8.2.2 -0.24	0.103 0.00	205 1.95
1418 ST	PIP89.1X4	.0 PASS 37.75 C	85-4,7 (C) -0,09	0.152 0.00	205
1419 ST	P1785.134	0 PASS 25.74 T	85-4.1.2.2 -0.25	0.120 0.00	205
1420 ST	P1P83.1X4	0 PASS 61.35 T	85-4.8.2.2 -0.14 -	0.227	204
1421 57	PIP114.3X	4.5 PASS 48.56 C	85-4.7 (C) -0.94	0.125 0.00	204
1422 57	P1765.1X4	0 PASS 69.33 T	85-4.8.2.2 -0.22	0.263 0.00	204
1423 ST	P1705.1X4	0 PASS 50.20 C	85-4.7 (C) -0.45	0.234 0.00	204
1424 ST	P1263.1X4	0 PASS 60.04 C	85-4,1,3,3,3 -6,23	0.299 0.16	:
1425 ST	P1769.1X4	0 PASS 67.42 C	85-4.7 (C) -0.46	0.271 0.00	204 1.95
1426 57	PIP49.1X4	0 PASS 80.83 T	85-4.4.2.2 -0.32	0.315 0.00	204
1427 57	P1789.1X4.	0 PASS 76.97 C	85-4.7 (C) -0.47	0.310 0.00	204
1428 ST	P1209.124.	0 PASS 85.26 T	85-4.8.2.2 -0.46	0.347 0.00	204
1429 ST	P1P45.124.	0 PASS 79.18 C	85-4.7 (C) -0.42	0.319 0.00	204
1438 ST	P1989.1X4.	0 PASS	85-4.7 (C)	0.351	205

L UNITS	ARE - KH	-	SS OTHERWISE NOTED		
HADR	TABLE	RESULT/	CRITICAL COND/	NATIO/	LOADING/
1497 5	F 91909.1	14.0 PASS 56.48 C	85-4.7 (C) -0.44	0.227	264 1.95
1498 5	F \$1989.1	X4.0 PASS 39.40 C	85-4.8.3.3.3 -0.23	0.238 0.35	:
1499 5	* *1***.1	44.0 PASS 66.74 C	85-4.7 (C) -0.46	0.269	284
1500 51	P1989.1	4.0 PASS 81.48 7	85-4.8.2.2 -9.32	0.317	204 0.00
1501 51	F P3P49.33	4.0 PASS 77.40 C	85-4.7 (C) -0.47	0.311	204
1502 51	P1919.11	4.0 PASS 87.14 T	85-4.8.2.2 -0.46	0.355	204
1503 51	P1709.11	4.0 PASS 40.16 C	85-4.7 (C) -0.43	0.322 0.00	204
1504 51	P100.11	4.0 PASS 85.24 C	85-4.7 (C) -0.13	0.342	203
1505 51	PIP114.3	37.68 C	85-4.8.3.3.3 -0.28	0.132 0.18	!
1306 57	P1P49.13	4.0 PASS 36.49 T	85-4.8.2.2 -0.20	0.149 0.00	205
1507 57	PIP89.13	4.0 PASS 35.29 C	85-4.7 (C) -0.26	9.144 0.00	205
1504 57	P1749.13	4.0 PASS 33.60 T	N5-4.8.2.2 -0.14	0.133	202
1509 57	P1P09.13	10.88 C	85-4.7 (C) -0.63	0.045	205 2.02
1510 ST		14.5 PASS 49.86 C	85-4.7 (C) -0.15	0.184 0.00	202
1511 57	\$1989.1X	61.52 C	es-4.4.3.3.3 -0.22	0.303	
1512 57	P1249.1X	72.13 T	85-4.8.2.2 -0.23	0.267	205
1513 57	P1999.1X	69.91 C	85-4.7 (C) -0.41	0.277	205
1514 57		4.0 PASS 74.03 T	85-4.8.2.2 -0.31	0.251	205
1515 57	P1P49.1x	64.45 C	85-4.7 (C) -0.41	0.259	0.00
1516 57	PIP#9.1X	72.17 7	85-4.9.2.2 -0.29	0.281	205 0.00
1517 57	P1949.1X	56.85 C	85-4.7 (C) -0.41	0.225	0.00
1518 ST	P1789.1X	4.0 PASS 36.28 C	85-4.4.3.3.3 -0.10	0.278	204

Print Tene Data: 11/07/2012 1

.... ....

C



2	Job No TPL40581	Sheel No.	a 168	Rav R4b-FAB
Software Domand to Transerve Pie Lid	Partwind speed 32	5 m/s		-
twe Wisma Bela Swimming Pool	Ref Fabric R5			
	BY TSM	Dele17-D	lec-11 Chd T	SM
Majlis Perbandaran Kuantan	File Q326-KSP-R4			
			1	
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - NY METE (UNLESS OTHERWISE HOTED)				
HENGER TABLE RESULT/ CASTICAL COND/ RATIO/ LOADING/				
1519 57 F1P89.1X4.0 PASS 85-4.8.3.3.3 0.242 5 43.58 C -0.25 0.23 -				
*****				
1520 ST P1P85.3X4.0 PASS 85-4.8.2.2 0.228 205 35.34 T -0.33 0.00 0.00	8°			
1521 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.214 201				
1521 ST P1P49.1X4.0 PASS B5-4.8.2.2 0.216 201 57.34 T -0.15 0.00 1.55				
1522 57 P1P89.1X4.0 PASS 85-4.7 (C) 0.212 201				
52.67 C -0.43 0.00 1.85				
1523 ST P2P85.3X4.0 PASS 85-4.8.2.2 0.267 201 70.56 7 -0.37 0.00 0.00				
70.56 7 -0.37 0.00 0.00				
1524 ST PIP89.3X4.0 PASS 85-4.7 (C) 0.280 201 (9.42 C -0.39 0.00 1.95				
1525 ST PIPES.1X4.6 PASS 85-4.8.2.2 0.251 201 71.80 T -0.37 0.00 0.00				
1526 ST PIPEP.1X4.0 PA35 85-4.7 ICI 0.252 201				
1526 ST P1P89-1X4.0 PA25 85-4.7 [C] 0.252 201 72.47 C -0.28 0.05 1.55				
1527 ST PIP114.3X4.5 PASS 85-4.8.2.2 0.232 201				
80.67 T -0.66 0.00 0.00		9		
1528 ST P1P89.1X4.0 PASS 85-4.7 (C) 0.063 205 15.68 C -0.26 0.00 1.95				
15.48 C -0.26 0.00 1.95				
1529 ST PIPEP.1X4.0 PASS 85-4.8.2.2 0.159 205 42.05 T -0.12 0.00 1.55				
1530 ST PIPE9.1X4.0 PASS 85-4.7 (C) 0.112 205 27.93 C -0.34 0.00 1.95				
1531 ST PIPS9.1X4.0 PASS 85-4.8.2.2 0.189 205				
50.67 T -0.13 0.00 1.95				
1532 ST #19114.3X4.5 PASS 85-4.8.7.2 0.114 204				
29.16 7 -0.49 0.40 1.95				
1533 ST PIPE9.1X4.0 PASS B5-4.6.3.3.3 0.263 204 53.38 C -0.19 0.15 -				
1534 57 F1FF9.1X4.0 FASS 85-4.7 (C) 0.153 205 47.94 C -0.39 0.00 1.95				
1535 ST P1P89.1X4.0 PASS 85-4.8.3.2.3 0.276 1				
1535 ST PIPE9.1X4.0 PASS 85-4.8.3.3.3 0.276 8 55.56 C -0.21 0.16 -				
1536 ST PIPER.124.0 PASS 85-4.8.2.2 0.239 204				
54.08 T -0.38 0.00 1.05				
1537 ST PIP99.1X4.0 PASS 85-4.7 (C) 0.304 204 75.44 C -0.26 0.00 0.00				
1538 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.293 204 70,70 T -0.42 0.00 1.95				
1539 57 P1P89.1X4.0 PASS 85-4.7 (C) 0.342 204 95.08 C -0.43 0.08 0.00				
1540 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.314 204 76.84 T -0.42 0.00 0.00				

STAAD Pro for V

Dwn 20.07.02.15

Run 70 of 10

Met Time/Dale: 11/02/2012 17:2

$\overline{\mathcal{O}}$						Job No TPL40581	Sheel No a 169	Rev R4b-FAB
>						Parlwind speed 32.	E	
		tio Transerve P nming Pool	le Lid			Ref Fabric R5	5 HVS	
		aning room				By TSM	Date 17-Dec-11 Ch	TSM
Malle D	whendau	n Kuantan					-Deg.sid Detertime 10-	
magaa r	CI Dariuara	n Kuran				Gazo-Kar Hite	Porgusta 1 104	JUP2012 10.43
			hecks Cont					
	7,312	TX .	CRITICAL COND/	NATIO/ HI	LOADINS/			
1541 57		4.0 PASS 11.45 C	85-4.7 (C) -0,12	0.355	204			
	PIP114.3	14.5 PASS 39.54 C		0.146 0.24	:			
		4.0 PASS	85-4.8.2.2 -0.31	0.188 0.00	204			
		4.0 PASS 41.11 C	85-4.7 (C) -0,34	0.160	204			
1545 57		4.0 PASS 39.40 T	15-4.8.2.2 -0.22	0.163	204			
		4.0 PASS 10.55 C		0.043	204			
	P1P114.3	X4.5 PASS		0.177	204			
1540 ST	P1P114.3	X4.5 PASS	85-4.8.3.3.3	0.228				
1549 57	P1P45.1X	60.56 C	-0.33 85-4.7 (C)	0.244	205			
				0.00	1.95			
			-0.37	0.00	0.00			
				0.287 0.00	205			
1552 57	P1989.1X		85-4.8.2.2 -0.39	0.248	205			
1553 57		4.0 PASS 65,59 C	85-4.7 (C) -0.22	0.264 0.60	205			
1554 57		45.22 C	85-4.8.3.3.3 -8.24	0.219	104			
	P1989.1X	\$7.59 C	85-4.7 (C) -0.16	0.232 0.00	205 1.95			
	P1P89.1X		85-4.8.3.3.3 -0.24	0.234 0.22	:			
		40.33 C	85-4.8.3.3.3 -0.06	0.236 0.23	205			
		1.0 PASS 30.34 C	85-4.8.3.3.3 -0.23	0.175	:			
1559 57	PIP69.1X	1.0 PASS 43.71 T	85-4.8.2.2 -0.14	0.166	204			
********	P1P89.1X	43.52 C	#5-4.8.3.3.3 -0.15	0.216	202			
1541 ST		42.03 T	85-4.8.2.2 -0.25	0.175	202			
	P1P03.1X	.0 PASS	85-4.8.3.3.3	0.191	•			
		37.84 C	-0.15	0.14				

WS 20 07.02.1

P				TPL40581	shael No a 170	Rev R4b-FA
Software licensed to Transerve Pie La	1			Parlwind speed 32.	5 m/s	
ab Title Wisma Bella Swimming Pool				Raf Fabric R5		
-					Dale17-Dec-11 Ch	TSM
Clent Majlis Perbandaran Kuantan				Fie Q326-KSP-R4	-Deg.sid Date/Time 10-	
Steel Design (Track 0) Che	eke Cent					
ALL UNITS ARE - IN HETE UNLESS	OTHERWISE NOTED					
HDISER TABLE RESULT/ C	HT COMP/					
1563 57 PIP89.124.0 PAIS 37.00 C		0.193 0.17	201			
1564 ST P1P114.384.5 PASS 46.19 T	-0.73	0.157	209			
1545 ST PIPES.1X4.0 PASS 1 19.37 T		0.035	205			
1544 ST FIP89.124.0 PASS 41.41 T		0.155	204			
			205			
24.78 T	-0.26	0.00	3.95			
1568 ST P1P89.1X4.0 PASS 1 61.54 T		0.225	204			
1549 ST P1P114.3X4.5 PASS 1 48.43 C	-0.57	0.124	204			
1570 ST PIPES.1X4.0 PASS 1 70.40 T	4.4.2.2 -0.23	0.268	204			
1571 ST PIPES.1X4.0 PASS 8		0.235	204			
	-0.31	0.354	204			
	15-4.7 (C)	0.278	204			
	15-4.8.2.2 -0.33	0.327	204			
	15-4.7 (5)	0.322	784			
	-0.48	0.00	204			
	******	0.60	1.55			
1577 ST P1P89.1X4.0 PASS 8 82.19 C	5-4.7 [C] -0.43	0.331 0.00	204			
1576 ST P1P85,124.0 PAES 8 65.37 C	-0.13	0.342	205			
		0.109	205			
1500 ST PIP69.1X4.0 PASS 8		0.147	205			
1581 57 PIP49.1X4.0 PASS 8	5-4.7 ICI	0.142	205			
1542 ST PIP49.1X4.0 PASS 8	5-4.8.2.2	0.130	202			
	5-4.7 (C) -0.09	0.044	205			
1584 ST P19114.3X4.5 PASS 8	5-4.7 (5)	0.178	202			
	-0.15	6.00	3.59			

2			TPL40581	Sheel No a 172	Rev R4b-FAB
Software licensed to Transerve Pie Lid			Panwind speed 32.1	5 m/s	
Tile Wisma Belia Swimming Pool			Ref Fabric R5		
			By TSM	Daw17-Dec-11	Chil TSM
Majils Perbandaran Kuantan			Fie Q326-KSP-R4b		10-Jul-2012 16:43
Steel Design (Track 0) Checks C	ont				
ALL UNITS ARE - IN HETE INHLESS OTHERWIS	-				
HEMBER TABLE RESULT/ CRITICAL PX HT	COND/ NAT30/ HZ	LOADING/			
1607 ST P1P89.1X4.0 PASS 83-4.8.3 51.53 C -8.	.3.3 0.254 20 0.13	204			
1608 ST P1P05.1X4.0 PASS 85-4.8.2 40.26 T -0.	.2 0.175 54 0.00	204			
1409 ST PIP49.1X4.0 PASS 85-4.8.3	.3.3 0.271 21 0.14	:			
1410 ST P1P89.1X4.0 PASS 85-4.8.2 54.18 T -0.	.2 0.231	204			
3411 ST PIPOD.1X4.8 PASS 85-4.7 73.84 C -0.		204			
1612 ST PIP05.1X4.0 PASS 83-4.8.2 68.64 T -0.	.2 0.285 43 0.00	204			
1613 ST FIFES.1X4.0 FASS 85-4.7 83.13 C -0.	(C) 0.334 43 0.00	204			
1414 57 91999.124.0 PASS 85-4.8.2. 78.86 7 -9.1	.2 0.309 40 0.00	204 0.00			
1615 ST PIPES.1X4.0 PASS 85-4.7 87.55 C -0.1	(C) 0.351 13 0.00	204			
1416 ST P3P114.3X4.5 PASS 85-4.8.3 39.20 C -0.3	.3.3 0.130 30 0.21	104			
1417 ST FIP49.1X4.0 FASS 85-4.8.2 43.89 T -0.	.2 0.190 33 0.00	204			
0.4(5 -4.3	IC) 0.171 06 0.00	204 2.02			
1619 ST PIPES.1X4.0 PASS 85-4.8.2. 40.20 T -0.1		204 0.00			
1420 ST PJP83.1X4.0 PASS 85-4.7 10.54 C -0.1		204 2.02			
1421 ST F1F114.3X4.5 PAGS 85-4.7 49.26 C -0.1		204			
1622 ST PIP114.3X4.5 PASS 85-4.8.2. 73.13 T -0.7	2 0.223 17 0.00	205			
1623 ST PJPP9.1X4.0 PASS 85-4.8.3. 61.63 C -0.1		105			
1424 57 PIPP9.1X4.0 PASS 85-4.8.2 66.80 T -0.3	.2 0.274	205 0.00			
1425 5T P1P49.1X4.0 PASS 85-4.7 73.83 C -0.3	(C) 0.285 03 0.00	205 1.95			
1426 ST P1P89.3X4.0 PASS 85-4.8.2. 59.70 T -0.3	2 0.252	205			
1427 ST P1789.1X4.0 PASS 85-4.7 66.61 C -0.2		205			
1428 57 P1P85.124.0 PASS 85-4.8.2. 45.45 7 -0.3	2 0.215	205			
		20202002020			

2				Jab No TPL40581	Sheel No	a 173	Rav R4b-FAB
Software Ricensed to Transerve Pie Li				Partwind speed 32.	5 m/s		
Jeb Tile Wisma Bella Swimming Pool				Ref Fabric R5			
				By TSM	Dele17-D	ec-11 Chd T	SM
Client Majis Perbandaran Kuantan				Fite Q326-KSP-R4	-Deg.std	Dele/Time 10-Jul-	2012 16:43
Steel Design (Track 0) Che ALL WRITS AAC - NY HETE (WHIESS O MEMBER TABLE RESULT/ CT	THERWISE HOTES	RATIO/	LOADING/	4			
1429 ST P1P45.3X4.0 PASS 1 34.83 C	HY 15-4.8.3.3.3 -0.18	HZ 0,288 0,21	LOCATION 205		2		
***************************************	-0.18	0.21	205				
1431 ST P1P89.1X4.0 PASS 4	15-4.8.3.3.3 -0.14	0.241	205				
1432 ST P2P09.3X4.0 PASS 0	15-4.8.2.2 -0.18	0.155	207				
	15-4.8.3.3.3 -0.09	0.192	205				
	15-4.8.3.3.3 -0.12	0.100 0.12	:				
1635 ST P1P89.1X4.0 PASS 43.38 T	5-4.8.2.2 -0.24	0.380 8.00	202				
1636 ST PIPES,1X4.0 PASS 8 47,35 C	15-4.7 (C) -0.26	0.151 0.00	262 0.60				
1437 ST P1P89.1X4.0 PASS 8 (8.35 T	-0.25	0.196 0.00	202				
49.14 7		0.171 0.00					
16.34 T	5-4.8.2.2 -0.22	0.003	205				
33.79 C			205				
21.54 7	-0.24	0.304 0.60	205				
52.67 T	-4.8.2.2	0.194 0.00	204				
29.55 7	5-4.8.2.2 -0.61 5-4.8.2.2	0.231	3.95				
61.63 7	-0.18	0.00	3.95				
45.78 C	-0.41	0.00	1.95				
58.18 C	-0.27	0.748	204				
	-0.43 5-4.8.2.2 -0.28	0.00	1.95 204 0.00				
1649 57 PIP49.1X4.0 PASS 8	-0.28 5-4.7 (C) -0.45	0.281 0.00	204				
	5-4.8.2.2 -0.42	0.325	204				

ows 20.07.02.1

-	2						Job No TPL40581	Sheel No	a 174	Rev R4b-FAB
7	>						Partwind speed 3	25 m/s		
Job Ti	We Wisma f		to Transarve P uming Pool	He Lid			Ref Fabric R5			
							BY TSM	Date 17-0	ec-11 Chd	TSM
Clant	Mails Pr	rbandara	n Kuantan				File Q325-KSP-R			
-										
				hecks Cont						
				SS OTHERWISE NOTES						
		TABLE	EX.	CNITICAL COND/	HAT10/	LOCATION				
		P1P69.13	4.0 PASS 74.73 C	85-4.7 (C) -0.40	0.301	204				
	1452 ST	PEP49.13	4.0 PASS 82.22 C	85-4.7 ICI -0.13	0.330	205				
		P1P134.3	14.5 PASS	85-4.8.3.3.3	0.129	105				
			36.91 C	-4.33	0.22					
	1654 57		4.0 PASS 40.57 T	85-4.8.2.2	0,174 0,00	205				
			4.0 PASS 38.86 C	85-4.7 (C) -0.32	0.159 0.20	205				
	1454 ST	PIP49.33	4.0 PASS 35.99 T	85-4.8.2.2 -0.20	0.148	205 0.00				
	1457 57	PIP05.18	4.0 PASS 10.27 C	85-4.7 (C) -0.15	0.042	205 2.02				
		P1P114.3	44.5 PASS 46.10 C	85-4.7 (C) -0.12	0,178	3 0.00				
		P1P89.1X	4.0 PASS	#5-4.8.3.3.3 -0.28	0.337	2				
	1440 ST		4.0 PASS	#5-4.8.2.2 -0.37	0.304	205				
	1441 57	P1989.1X	4.0 PASS 72.54 C	85-4.7 (E) -9.43	0.292	205				
	1462 57	P1P89.1X	4.0 PASS 78.16 T	85-4.8.2.2 0.33	0.308	205				
			4.0 PASS 69.20 C	85-4.7 (C) -0.43	0.275	205				
			4.0 PASS 76.40 T	#5-4.8,2.2 -0,31	0.298	205				
				85-4.7 (C)	0.244					
			4.0 PAIS 71.46 T	15-4.8.2.2 -0.28	0.279	205				
			4.0 PASS 50.61 C	-6.28 85-4.7 (C) -0.42	0.204	205				
		P1P89.1X	50.61 C		0.245	205				
				-0.22	0.00	0.00				
		P1P85.1X	41.33 C	25-4.8.3.3.3 -0.08	0.205	12				
		P1989.1X	4.0 PASS 42.42 C	85-4.8.3.3.3 -0.04	0.211 0.21	104				
	1671 ST	P1989.1X	4.0 PASS 68.51 T	85-4.8.2.2 -0.25	0.277	201				
	1672 57	P1989.1X	4.0 FASS 66.58 C	85-4.7 (C) -0.30	0.268	201				

Subvare Teassed to Transerve Pile Ltd	TPL40581 Sheet No a 171 Rev Ab-FJ				
	Parlwind speed 32.	5 m/s			
Wisma Belia Swimming Pool	Raf Fabric R5				
	BY TSM	Dale17-Dec-11	Nd TSM		
Majlis Perbandaran Kuanlan	File Q326-KSP-R4	b-Deg.std Date/Time 10	Jul-2012 16:43		

ALL UNITS ARE - IN		S OTHERWISE NOTED		
HDIER TABLE	ALSVLT/	CRITICAL COND/ HY	NAT10/ H1	LOCATIO
1585 ST P1P19.13	56.83 C	85-4.8.3.3.3 -0.11	0.278	2
1586 ST P3P88.11	4.0 PASS 67.50 C	85-4.7 (C) -0.35	0.272	204
1587 ST P1989.11	4.0 PASS	85-4.8.2.2	0.267	204
	44.30 T	-0.37	0.00	0.0
1588 ST P1P89.11	PASS	85-4.7 (C) -0.30	0.275	204
	69.24 C	-0.30	6.00	1.9
1549 ST P1889.13	4.0 PASS \$7.90 T	45-4.8.2.2	0.242	204
1590 ST 91949.13	4.0 PASS 65.80 T	85-4.8.2.2	0.255	205
1591 ST P1789.13	48.40 T	85-4.8.2.2	0.219	204
1592 ST P1P89.13	4.0 PASS 54.29 C	85-4.8.3.3.3 -0.17	0.276	204
1593 ST P1P49.33	4.0 FASS 38.77 T	85-4.0.2.2	0.173	204
1594 ST P1P89.13	4.0 PASS 53.42 T	85-4.8.2.2	0.202	205
1595 ST #1989.13	4.0 PASS 34.06 T	85-4.8.2.2	0.210	201
1596 ST PIPES.13	4.0 PASS 51.29 C	85-4.7 ICI -0.15	0.204	204
1597 ST P1P09.13	4.0 PASS 49.84 T	85-4.8.2.2	0.282	201
1598 ST P1989.13	4.0 PASS 67.01 C	85-4.7 (C) -0.39	0.273	201
1599 ST #1989.13	4.0 PASS 70.85 T	85-4.8.2.2	0.286	201
1400 ST P1P89.13	4.0 PASS 70.79 C	85-4.7 (C) -0.25	0.215	201
1401 ST P3P114.3	14.5 PASS 79.30 T	85-4.4.2.2	0.229	201
1402 ST P3P89.13	4.0 PASS	85-4.8.3.3.3 -0.19	0.015	105
1603 ST PIPES.18	4.0 PASS 38.33 T	85-4.8.2.2	0.144	205
	34.35 1	-9.15		
1604 ST P2P89.13	4.0 PASS 23.70 C	85-4.7 (C) -0.32	0.055	205
	23.70 C	-0.32	0.00	1.9
1605 ST PIPES.1X	4.0 PASS	85-4.8.2.2	0.169	205
	45.73 T	-0.11	0.00	1.4
1404 ST PIP134.3	84.5 PA35	85-4.8.2.2	0.108	204
	21.30 T	-0.66	0.00	1.9

8 Solvere Franked to Transante Pie Lid	TPL40581 Shest No a 175 Rate
	Parl wind speed 32.5 m/s
Job 78e Wisma Bella Swimming Pool	Ref Fabric R5
	By TSM Dale 17-Dec-11 Chd TSM
Cleni Majis Perbandaran Kuantan	Fie Q326-KSP-R4b-Deg.std Dete/Time 10-Jul-2012 1

LL UNITS	NAE - INI		S OTHERWISE HOTED		
CHIER	TABLE	NESULT/	CAITICAL COND/	MATIO/	LOADING/
1673 57	P1999.1X	4.0 PASS 69.75 T	85-4.0.2.2 -0.35	0.282	201 0.00
1674 57	P1P49.18	4.0 PASS 69.83 C	85-4.7 (C) -0.28	0.203	201 1.95
1675 57	PIP114.3	X4.5 PASS 79.00 T	85-4.8.2.2 -0.61	0.226 0.00	201
1676 37	P1789.1X	4.0 PASS 15.13 C	85-4.8.3.3.3 -0.03	0.692 0.23	201
1677 57	P1949.1X	4.0 PASS 45.84 7	85-4.8.2.2 -0.18	0.178 0.00	205
1678 57	P1P49.1X	1.0 PASS 31.58 C	85-4.7 (C) -0.36	0.137 6.60	205
1479 57	P2P49.1X	1.0 PASS 55.24 7	85-4.8.2.2 -0.15	0.207 0.00	205
1440 37	P1P114.2	4.5 PASS 30.83 T	85-4.8.2.2 -0.79	0.119	204
1681 57	P1989.1X	PASS 35.28 C	85~4.8.3.3.3 -0.20	0.273	204
1442 57	P1P89.1X	4.0 PASS 52.21 C	85-4.0.3.3.1 -0.06	0.230	205
1443 57	PIP85.1X	PASS 57.85 C	AS-4.8.3.3.3 -0.22	0.207	:
1684 57	PIP89.1X	1.0 PASS 62.57 C	85-4.7 (C) -0.44	0.253	205
1605 57	P1P89.1X	1.0 PASS 77.56 C	85-4.7 (C) -0.27	0.312	204
1686 57	PIP19.12	72.45 T	85-4.8.2.2 -0.43	0.301	204
1687 57	P1P89.1X	1.0 PASS 87.68 C	85-4.7 (C) -0.44	0.350 0.60	204
1600 57	P1249.1X	1.0 PASS 78.20 T	85-4.8.2.2 -0.43	0.320	204
1619 57	P1P83.1X	90.03 C	85-4,7 (C) -0,11	0.363	204
1630 57	P1P114.33	4.5 PASS	85-4.7 (C) -0.45	0.125	204
1491 57	P1P65.1X	1.0 PASS 44.30 T	85-4.8.2.2 -0.31	0.190	204 0.00
1692 57	P1P09.1X	1.0 PASS 41.36 C	85-4.7 (C) -0.24	0.149	264 2.02
1693 57	P1989.184	40.04 T	85-4.8.2.2 -0.22	0.164	204



2	TPL40581	sheel No a 176	Rev R4b-FAE
Software licensed to Transerve Pie Lid	Panwind speed 32.5	5 m/s	
to Tide Wisma Bella Swimming Pool	Ref Fabric R5		
	BY TSM	Date 17-Dec-11 C	TSM
Majlis Perbandaran Kuantan	Fit Q326-KSP-R4b	-Deg.std DataTime 10-	Jul-2012 15:43
Steel Design (Track 0) Checks Cont           Number of the state (State (State))           Number of the state (State)           Number of the sta			
1765 ST F2R45.1X4.0 FASS B5-4.4.2.2 0.241 244 42.33 T -6.32 0.68 0.69 1764 ST F2R45.1X4.0 FASS B5-4.4.5.2 4.172 265 1764 ST F2R45.1X4.0 FASS B5-4.4.5.2 4.172 265 17.4 ST -0.0.3 6.68 0.00			
1765 3T PIPH9,1X4-0 PAIS B5-4,8,2,1,1, 8,242 265 49,13 C -0.03 0.22 -			
1766 ST PIPH9,124.0 PASS 85-4.8.3.3.3 0.201 208 39.65 C -0.10 8.21 -			
1707 ST P2P49-124-0 PASS B5-4.8.2.2 0.181 254 47.12 T -0.16 0.60 0.00			
1708 ST P2F89.1X4.0 PASS 85-4.8.3.3.3 0.223 282 47.85 C -0.16 0.17 -			
1709 ST P1P49.1X4.0 PASS B5-4.0.2.2 0.192 202 46.50 T -0.27 0.00 1.55			
1718 ST P1P49.1X4.0 PASS 85-4.8.3.3.3 0.210 6 41.04 C -0.17 0.15 -			
1711 ST P1P49-1X4.0 PASS B5-4.8.2.2 0.199 262 50.36 T -0.22 0.00 0.00 0.00			
1712 ST P1P114.3X4.5 FRS5 85-4.4.2.2 0.163 265 49.20 T -0.72 0.00 1.55			
1713 ST FIF49.184.0 FASS 85-4.8.2.2 0.092 265 18.36 T -0.23 0.00 1.55			
1714 ST P1P49.1X4.0 PASS 85-4.8.2.2 0.141 264 42.03 T -0.14 0.00 1.95			
1715 57 FIPES.1X4.0 PASS 85-4.6.2.2 0.114 265 23.68 7 -0.26 0.00 1.55			
1716 ST P1P49.1X4.0 PASS 85-4.8.2.2 0.234 204 62.68 T -0.16 0.00 1.85			

0			TPL40581	Shaet No	a 177	Rev R4b-FAB
			Parlwind speed 32.	S m/s		
Software licensed to Transerve Pie Ltd Ne Wisma Bella Swimming Pool			Ref Fabric R5			
1000 Contraction - 1000			By TSM	Date 17-De	c-11 Du	TSM
Majlis Perbandaran Kuantan			Fie Q325-KSP-R4b			Jul-2012 16:43
1713 ST FEP114.384.5 PAGE 85-4.7 [6] 31.45 ST FEP3.184.5 PAGE 85-4.7 1718 ST FEP3.184.6 PAGE 85-4.1.2.2 1719 ST FEP3.184.6 PAGE 85-4.5.2.1 1719 ST FEP3.184.6 PAGE 85-4.5.2.2 1728 ST FEP3.184.6 PAGE 85-4.5.2.2	RATIO/ ME 0.127 0.00 0.274 0.00 0.327 0.46	204 1.95 204 1.95 204 204 204 204				
1721 ST F1P49.3X4.0 FASS E5-4.7 [C] 70.11 C -0.48 1722 ST F1P49.3X4.0 FASS E5-4.8.2.2 1722 ST F1P49.3X4.0 FASS E5-4.8.2.2	0.242 0.00 0.331	204 1.95				
1723 57 FIP65.1X4.0 FASS 85-4.7 (C) 81.00 C -0.45	0.326 0.00	204 1.95				
1724 ST PIP49.1X4.0 PASS 85-4.4.2.2 51.22 T -0.45	0.372 0.00	204 1.95				
	0.327					
H.25 C -0.11	0.338	205				
45.00 C -0.40	0.00	205				
40.36 T -0.27	0.00	285				
38.04 C -0.30	0.146	205				
35.70 T -0.13 1731 ST PIP99.1X4.0 PASS 85-4.8.3.3.3 7.72 C -0.02	0.00	0.00				
	0.184	:				
1733 ST P1P49.1X4.0 PASS 65-4.7 (C) 61.44 C -0.36	0.275	205				
1734 ST PIP89.1X4.0 PASS 85-4.8.2.2 70.64 T -0.42	0.294 0.00	205				
1735 ST PIPOD.1X4.0 PASS 85-4.7 (C) 57.52 C -0.45	0.231	205				
1736 ST P1P89.1X4.0 PASS 85-4.0.2.2 45.57 T -0.50	0.286	205				
1737 ST P3P89.1X4.0 PASS 85-4.4.2.2 49.34 T -0.46	0.228 0.00	204				
1738 57 P1P49.1X4.0 PASS 85-4.8.2.2 54.19 T -0.43	0.239	205				

					Jeb No TPL40581	Sheet No a 178
5						
	are licensed to Transerve I	he Lid			Panwind speed 32.	5 m/s
and more evisional	Bella Swimming Pool				By TSM	Cale17-Dec-11
Cleni Malte D	erbandaran Kuantan		-			-Deg.std Data/Time 10.
	sign (Track 0) C					
	UNE - XN HETE (UNLI TABLE RESULT/	CRITICAL COND/	NATIO/	LOAD ING/		
	R R		HI	LOCATION		
1739 57	PIP49.124.0 PASS	85-4.8.2.2	0.302	204		
1740 57	P1P49.1X4.0 PASS 58.39 C	85-4.7 (C) -0.47	0.235	1.95		
1741 57	PIPOS.1X4.0 PASS 72.80 T	85-4.8.2.2	0.295	207		
		85-4.7 (01	0.264	207		
			0.00	1.55		
1743 57	PIPES.1X4.0 PASS 85.36 T	-0.61	0.366	207		
1744 57	P1P13.1X4.0 PASS	85-4.7 (C)	0.326			
		-0.74	0.00	1.95		
1745 57	PIP89.184.0 PASS 95.82 T	85-4.8.2.2 -0.56	0.397	207		
	P1719.184.0 PASS	85-4.7 (C)	0.375	207		
	53.15 C		0.00			
1747 ST	P1969.1X4.0 PASS 59.01 T	85-4.8.2.2 -0.91	0.451 0.00	207 6.00		
	P1P09.124.0 PASS 105.50 C		0.620	207		
	P1P114.3X4.5 PASS		0.342	205		
1/49 11	47.33 C	ANNEX 1.1 -1.73	2.55			
1750 57	PIP49.124.0 PASS 35.26 T	85-4.8.2.2	0.273	205		
	P1P13.1X4.0 PASS 49.18 C		0.138	208		
	43.38 C	-0.29	0.00	0.00		
	P1P89.1X4.0 PASS 49.74 T	85-4.8.2.2 -0.61	0.245	208		
1753 57	P1249.1X4.0 2855	85-4.8.3.3.3	0.310	104		
	45.10 C	-0.54	0.45			
1754 ST	P1P114.3x4.5 PASS (8.31 7	85-4.0.2.2 -2.16	0.254 0.00	204		
1755 ST	PIP49.184.0 PASS 55.44 C	85-4.7 (C) -0.24	0.223	204		
	PIPED.1X4.0 PASS 48.69 T	85-4.8.2.2 -0.66	0.248	204		
1757 57	P1P89.1X4.0 PASS 46.17 C	85-4.7 (C) -0.17	0.186	208		
1754 57	PIP49.124.0 PASS	85-4.1.2.2	0.262	208		
		-0,01	0.00	1.95		
	P1P09.1X4.0 PASS 32.80 T	85-4.0.2.2 -0.87	6.220 0.00	209		
	P1P49.1X4.0 PASS 43.50 T	05-4.0.2.2	0.256	208		
		-0.85	0.00	0.00		

			TPL40581	Sheet No a 180	Rev R4b-FAB
5					
eb Title Wisma Bella Swimming Pool			Perl wind speed 32.1	m/s	
The Trisma Dola Swittining Pool				Delle17-Dec-11 Chi	TSM
Majlis Perbandaran Kuanlan				Deg.std Dete/Time 10-J	
Steel Design (Track 0) Checks Cont					
ALL UNITS ARE - WH HETE UNLESS OTHERWISE NOTE HUMER TABLE RESULT/ CALTICAL COND/	NATIO/	LOADING/			
PX HY	нı	LOCATION			
\$2.88 C -0.63	0.374	207			
1784 ST PIPS9,1X4.0 PASS 85-4.8.2.2	0.450	267			
58.80 T -0.93					
1785 ST P1P89.1X4.0 PASS 85-4.7 (C) 105.25 C -0.61	0.423	207			
1786 ST PIP114.3X4.5 PASS ANNEX 1.1 87.15 C -1.72	0.344 2.53	204			
	0.292				
1707 ST PIPOD.1X4.0 PASS 85-4.8.2.2 37.54 T -1.31	0.00	204			
53.69 C -0.17	0.216	205 0.00			
1789 ST P1P89.1X4.0 PASS B5-4.8.2.2 45.18 7 -0.42	0.231	205			
1790 ST PJP09.1X4.0 PASS 85-4.7 (C) 57.23 C -0.28	0.230 8.00	205			
1791 ST PIP114.384.5 PAdS 85-4.4.2.2 50.21 T -1.74	0.234	205			
1792 ST F1F89.1X4.0 FASS 85-4.7 (C) 57.52 C -0.18	0.231	265			
•••••••••••••••••••••••••••••••••••••••	0.00	0.00			
1793 ST FIP49.1X4.0 PASS 85-4.8.2.2 50.40 T -0.60	0.247	205			
1794 ST #1989.1X4.0 PASS 85-4.7 (C) 46.47 C -0.17	0.187	208			
1795 ST PIP89.1X4.0 PASS 85-4.8.2.2 47.66 T -0.80	0.263	208			
1796 ST PIPES.1X4.0 PASS 85-4.8.2.2 32.52 T -0.50	0.223	205			
1797 ST P1999.124.0 PASS 85-4.4.2.2	0.253	208			
44.27 7 -0.82	0.00	0.00			
1798 ST FIRES.1X4.0 PASS ANNEX 1.1 38.89 C -0.43	0.225	208			
1781 ST FIPES.1X4.0 PMS5 MS-4.8.2.2	0.362	7.08			
1800 ST PIPE3.1X4.0 PASS ANMEX 1.1 27.51 C -0.40	0.273	200			
1801 57 PIP114.3X4.5 PASS 85-4.7 (C) 76.07 C -0.27	0.156	202			
	0.261	202			
64.23 T -0.24	0.00	2.02			
1003 57 92999.1X4.0 PASS 85-4.7 (C) 74.97 C -0.42		202 2.02			
1804 ST P3P89.1X4.0 PASS 85-4.8.2.2 84.43 T -0.49	0.348	202			
11.13 T =0.17					

STAAD.Pro for W

ows 20.07.02.15

2						TPL40581	a 181	Rev R4b-FAE
2	vare licented	to Transerve Pr	e Lid			Perf wind speed 32.5	m/s	
Tile Wisma						Rel Fabric R5		
						BY TSM	Dele17-Dec-11 Ch	TSM
ent Mallis P	erbandarar	Kuanlan				File Q328-KSP-R4b		Jul-2012 18:43
ALL UNITS HD-BEA 1805 ST 1806 ST 1807 ST 1809 ST	ARE - IN TABLE PIPH9.12/ PIPH9.12/ PIPH9.12/ PIPH9.12/ PIPH9.12/	HETE (UNLE: RESULT/ FX 4.0 FASS 25.48 C (4.5 FASS 101.36 C 1.0 FASS 48.77 T 4.0 FASS 48.77 T 4.0 FASS 58.86 T 58.86 T	85-4.8.2.2 -0.65 85-4.8.2.2	RATIO/ HE 0.325 0.50 0.374 0.316 0.316 0.316 0.280 0.280 0.00 0.299 0.09	282 202 3.59 204 1.95 205 206 1.95			
1010 57	P1989.1X4	.0 PASS 68.25 T	85-4.8.2.2 -0.53	0.294 0.00	205	8		
1012 ST	PIP89.184	.0 PASS 44.32 T	85-4.7 [C] -0.43 85-4.8.2.2 -0.42	0.271	205			
1833 57	PIP49.124	.0 PASS 39.61 T	85-4.8.2.2	0.253 0.00	204			
	PIPES.124	56.75 T	85-4.8.2.2 -0.60 85-4.8.2.2	0.268 0.00 0.251	205			
	PIP89.1X4	40.32 7	-0.91 85-4.8.2.2 -0.38	0.00	a.do 9 1.95			
1817 57	P3P89.334	.0 PASS 45.48 T	85-4.8.2.2 -0.83	0.260 8.00	294			
1010 57	P1P89.1X4	.0 PASS 58,70 C	85-4.7 (C) -0.51	0.236 0.00	201			
		80.44 T	85-4. P.2.2 -0.42 85-4.7 (C)	0.324 0.00	201 0.00			
	P1P85.1X4	.0 7355	-0.43	0.00	201			
	\$1545.1X4	0 PASS	-0.75 85-4.8.3.3.1 -0.95	0.399	207			
1823 57	P3P114.3K	4.5 PASS	AMMEX J.1 -2.07	0.344	205			
		22.46 1	85-4.8.2.2 -1.30					
		50.25 7	85-4.9.2.2 -0.75 85-4.7 (C)					
1824 57	P1209.1X4	50.37 C	85-4.7 (C) -0.64	0.203	200			

	JOB NO TPL40581	Sheel No a	182	Rev R4b-FAB
5	Parlwind speed 32.	Com/r		
Tale Wisma Bella Swimming Pool	Ref Fabric R5	o mvs		
	By TSM	Dele17-Des	-11 Chd	TSM
ani Majiis Perbandaran Kuantan	File Q326-KSP-R4		Date/Time 10-J	J-2012 16:43
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - KH HETE (UNLESS OTHERWISE HOTED)				
HEMBER TABLE RESULT/ CRITICAL COND/ NATIO/ LOADING/ PX HY HI LOCATION			*3	
1427 ST P1049.1X4.0 PASS 85-4.8.2.2 0.332 205				
1027 ST P1089-134.6 PASS 85-4.8.2.2 0.332 205 67.21 T -0.82 0.00 0.08				
1424 ST 939114.3X4.5 PA55 85-4.4.2.2 0.206 204 23.49 T -2.25 0.00 1.95				
1829 57 F1F85.1X4.0 FASS 85-4.8.2.2 8.376 205 84.00 T -0.72 8.00 0.00				
1830 ST P2P49.1X4.0 PASS 85-4.7 (C) 0.308 205				
1830 57 9299.1X4.0 9A25 85-4.7 (C) 0.308 205 76.53 C -0.51 0.09 1.95				
1031 ST PIF45.1X4.0 PASS B3-4.8.2.2 0.365 205 87.94 T -0.53 0.00 0.00				
1832 ST PIP49.1X4.0 PASS B5-4.7 (C) 0.335 285 83.25 C -0.65 0.00 1.95				
1833 ST P1P49.3X4.0 PASS 85-4.4.2.2 0.449 205				
39.22 T -0.85 0.00 0.00				
1824 ST P2289.124.0 PASS 85-4.7 (C) 0.396 205 98.52 C -0.49 0.00 1.95				
***************************************				
1835 ST P1P49.3X4.0 PASS B5-4.8.2.2 0.445 205 109.34 T -0.74 0.00 0.00				
1436 ST FIP45.1X4.0 PASS 85-4.7 (C) 8.408 285				
59.52 C -0.53 0.00 1.55				
1037 ST PIP49.1X4.0 PASS B5-4.4.2.2 0.352 205 94.25 T -0.20 0.00 1.33				
1928 ST PIP114-2K4.5 PASS ANNEX 1.1 0.175 208				
45.24 C -0.55 1.43 -				
1839 ST P1P89.1X4.0 PASS 85-4.4.3.3.3 0.195 205 36.59 C -0.24 0.06 -				
1840 ST PIP49.1X4.0 PASS 85-4.8.2.2 0.151 205 33.85 T -0.25 0.00 2.02				
1841 ST F2P89.1X4.0 PASS 85-4.7 (C) 8.220 205				
53.71 C -0.10 0.00 0.00				
1842 ST FIF89.1X4.0 FASS ANNEX 1.1 0.075 206 3.36 C -0.43 0.15 -				
1843 57 F1P114.3X4.5 FA55 85-4.0.2.2 0.234 205 42.46 7 -0.45 0.06 3.59				
1844 ST PTP114.324.5 PASS 85-4.8.7.7 0.748 185				
69.69 T -1.26 0.00 1.95				
1845 57 P1P89.1X4.0 PASS 85-4.8.2.2 0.287 204 70.59 T -0.37 0.00 1.95				
1846 57 P1993.1X4.0 PASS 85-4.8.2.2 0.264 205 59.58 7 -0.49 8.00 1.95				
1847 ST P2P89.1X4.0 PASS 85-4.8.2.2 0.314 204				
64.48 T -0.76 0.00 1.95				
1848 ST P1P89.1X4.0 PASS 85-4.8.2.2 0.268 205 52.64 T -0.71 0.00 8.00				

Print Run 78 of 10

2	Job No TPL40581 a 179 R4b-F					
Software Reensed to Transerve Pie Ltd	Parlwind speed 32.	5 m/s	1.1.1			
* Wisma Bella Swimming Pool	Ref Fabric R5					
	BY TSM	TSM				
Majlis Perbandaran Kuantan	Fle Q325-KSP-R4	Deg.sld	Date/Time 10-J	ul-2012 16:43		

# Steel Design (Track 0) Checks Cont...

LL UNITS	NR - 154	HETE (UNLE	SS OTHERMISE NOTED	,	
DGDA	TABLE	RESULT/	CRITICAL COND/	NATIO/	LOADING/
1761 57	P1989.1	14.0 PASS	ANNEX 1.1 -0.46	0.244	208
1762 57	P1989.1	41.8 PASS	85-4.4.2.2 -1.62	0.00	205
1763 51	PIP69.1		AMMEN I.1	0.277	200
		26.71 C	-0.42	1.55	
1764 ST	F1P114.	X4.5 PASS	85-4.7 (C)	0.198	202
		77.09 C	-0.27	0.80	1.96
1765 51		4.0 PASS	35-4.8.2.2	0.261	202
1765 57	\$1969.1	64.47 T	-0.34	0.00	2.02
*******			*******		
1766 ST	PIP45.1	4.0 PASS 75.24 C	85-4.7 (C) -0.62	0.305	202
					*********
1767 57	P1749.11	4.0 7355	85-4.4.2.2	0.346	202
1		84.06 T	-0.48	0.00	2.02
1768 ST	P1789.11	4.0 PASS	ANNEX 1.1 -0.37	0.123	202
1769 57	P12114.3	X4.5 PASS	85-4.7 (0)	0.372	202
		100.83 C	-0.54	0.00	3.55
				0.176	204
1770 ST	PIP114.:	124.5 PASS 68.45 C	85-4.7 (C) -0.67	0.00	0.00
1771 ST	#1789.13	4.0 PASS 69.23 T	85-4.1.2.2	0.290	204
		19.23 T	-0.43	0.00	1.95
1772 57	PIP49.13	4.0 PASS	35-4.7 (C)	0.244	204
		60.63 C	-0.45	0.00	0.00
					204
1773 57	PIP83.13	69.96 T	85-4.8.2.2	0.333	1.95
			**************		
1774 57	P1P89.13	4.0 PASS	83-4.8.2.2	0.252	205
		50.12 T	-0.65	0.00	0.00
1775 57	P1789.13	4.0 PASS	85-4.8.2.2	0.295	204
		63.67 T	-0.63	0.00	1.95
					205
1776 57	P1P49.13	4.0 PASS 54.02 T	85-4.8.2.2	0.304	0,00
1777 ST	P1209.13	4.0 PASS	85-4.4.2.2	0.240	204
		50,98 T	-0.53	0.00	0.00
1778 57	P1P85.13	4.0 PASS	85-4.8.2.2	8.110	207
	*****	75.72 T	-0.42	0.00	1.95
		*******	***************		
1779 ST	PIP49.13		85-4.7 (C)	0.275	207
		68.24 C	-0.73	0.00	1.95
		4.0 PASS	85-4.8.2.2	0.391	207
1780 ST	P1709.13	4.0 PASS 86,86 T	-0.76	0.00	1.95
1781 ST	P1789.13	4.0 PASS	85-4.7 (C)	0.330	207
		81.59 C	-0.92	0.00	1.95
1782 ST	P1709.1X	4.0 PASS 95.09 T	85-4.8.2.2	0.414	207

dows 20.07.02.1 TAAD Pro for W

2	Job No TPL40581 Sheet No a 183 Rev R4b-F				
Software licensed to Transarve Pto Lid	Patiwind speed 32.5	5 m/s	100		
se Tile Wisma Bella Swimming Pool	Ref Fabric R5				
	By TSM	Dale17-Dec-11	Chd T	SM	
Client Majils Perbandaran Kuantan	File Q326-KSP-R4b	Deg.std Dele	The 10-Jul-	2012 16:43	

### Steel Design (Track 0) Checks Cont...

ALL UNITS	ARE - IN	HETE INNLES	S OTHERALISE HOTEON		
DIBER	TABLE	ALSULT/	CRITICAL COND/ HT	NAT10/ H2	LOADING/
1849 57	P1P45.1X4	.0 PASS 57.16 T	85-4.8.2.2 -0.38	0.268 0.00	204
1850 ST	P1789.1X4	.0 PAIS 46.43 T	85-4.8.2.2 -1.00	0.204	205
1851 57	PIP05.1X4	.0 PASS 49.27 T	85-4.8.2.2 -0.50	0.239	204
1052 57	P1989.1X4	0 PASS 44.90 T	85-4.8.2.2 -0.91	0.266 0.00	205
1053 57	P3P83.1X4	.0 PASS 36.11 C	85-4.7 (C) -0.88	0.224 0.00	205
1854 ST	P1P89.1X4	.0 PAIS 40.23 T	85-4.1.2.2 -0.54	0.255	205
1855 ST	P1P85.1X4	.0 PASS 53.92 C	85-4.7 (C) -0.98	0.217	205
1856 ST	P3P89.3X4	.0 PASS 37.45 T	85-4.8.2.2 -0.58	0.269	201
1857 57	PIPES.1X4	.0 PASS 58.55 C	85-4.7 (C) -0.51	0.236	201
1859 57	P1785.1X4	0 PASS 64.83 T	85-4.4.2.2 -0.70	0.309	201 0.00
1859 57	P1P89.1X4	0 PASS 63.29 C	85-4.8.3.3.1 -1.05	0.379 0.02	203
1060 57	P1P114.3X	.5 PASS 12.77 C	ANNEX 1.1 2.16	0.353	204
1861 57	P1209.1X4	0 PASS	BS-4.4.2.2 -1.15	0.250	209
1862 57	PIP49.1X4	0 PASS 44.94 T	85-4.8.2.2 -0.93	0.265	204
1863 57	PIP85.1X4	0 PASS 44.47 C	85-4.7 (C) -0.43	0.175	208
1864 57	P1P49.1X4	0 PASS 70.34 T	85-4.8.2.2 -0.63	0.318	204 0.00
1845 57	P1P114.3X4	.5 PASS 17.93 T	85-4.8.2.2 -1.72	0.181 0.00	9 1.95
1866 57	P1P89.1X4	0 PASS	85-4.8.2.2 -0.71	0.384	204 0.00
1867 57	PIP89.1X4.	0 PASS 78.70 C	85-4.7 (C) -0.54	8.317 0.00	204
1468 57	PIP49.124	0 PASS 50.44 T	85-4.8.2.2 -0.58	0.380	204
1869 57	P1P49.1X4.	0 FASS 85.50 C	85-4.7 (C) -0.45	0.344	204
1870 ST	P1P89.1X4.	0 PASS 101.30 T	85-4.8.2.2 -0.96	0.445 0.00	204
	**********	*********		*********	*******

Print Time/Date: 11/07/2012 1

TAAD.Pro for Windows 20.07.02.15



	TPL40581	Sheet No a 18	4	Rev R4b-FAB
Software licensed to Transerve Pie Ltd	Patwind speed 32	5 m/s		
Tile Wisma Belia Swimming Pool	Ref Fabric R5		C	
	BY TSM	Date17-Dec-11	CM TS	м
Majlis Perbandaran Kuantan	Fe Q326-KSP-R4			
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - KN HETE (UNLESS OTHERMISE NOTED)				
HDISER TABLE RESULT/ CRITICAL CONE/ SATIO/ LOADING/				
•••••••••••••••••••••••••••••••••••••••				
1473 ST PIFES.3X4.0 PASS 85-4.7 (C) 0.406 204 100.46 C -0.91 0.00 1.95				
1672 ST P1789.1X4.0 FASS 85-4.8.2.2 0.443 204				
111.83 T -0.82 0.00 0.00				
1073 57 FIFE9.134.0 FA35 85-4.7 [C] 0.407 204 101.20 C -0.57 0.00 1.95				
101.20 C -0.57 0.00 1.95				
1874 ST FIF49.1X4.0 PASS 85-4.8.2.2 0.358 204 58.84 7 -0.17 0.00 1.53				
1075 ST PIP114.3X4.5 FASS ANTX J.1 0.173 200				
44.05 C -0.94 1.43 -				
1876 ST PIPES.1X4.0 PASS 85-6.8.3.3.3 0.201 204				
38.63 C -0.23 0.05 -				
1677 3T PIP69.1X4.0 PA3S BI-4.6.2.2 0.155 264 35.28 T -0.28 0.00 2.02				
1478 ST P1999.1X4.0 PASS 85-4.7 (C) 0.225 204 55.12 C -0.10 0.00 0.00				
1879 ST PIPES.184.0 PASS NONEX 1.1 0.076 206				
1879 ST P1989.1X4.0 PAIS ANNEX I.1 0.076 226 3.24 C -0.44 0.16 -				
1880 ST P1P114.3X4.5 PATS 85-4.8.2.2 0.240 204 84.77 T -0.52 8.00 3.59				
1481 ST PIP1395.0 PASS ANNEX 1.1 0.471 204 154.25 C -1.59 7.19 -				
1462 ST P1P1395.0 PASS ANMEX 1.1 0.323 206				
42.05 C -1.28 6.36 -				
1483 ST 9291395.0 PASS ANNEX I.1 0.396 286 109.67 C -2.07 6.40 -				
109.67 C \$2,67 8.40 -				
1674 ST PIP1355.0 PASS 85-4.0.2.2 0.366 206 9.67 T -7.22 0.00 1.57				
1445 ST FIF1395.0 FASS ANMEX 1.1 0.324 204				
42.73 C -1.32 6.35 -				
1986 ST PJP1395.0 PASS ANNEX 1.1 0.396 206 108.50 C -2.07 5.40 -				
1887 ST F1F1395.0 FASS ANNEX T.1 0.478 206 154.77 C -1.68 8.03 -				
1486 57 F1F1395.0 FASS ANNEX 1.1 0.311 204				
6.76 C -2.69 5.63 -				
1489 ST PIP1395.0 PASS 85-4.7 (C) 0.167 201				
91.40 C -1.11 0.00 1.57				
1890 ST PIP1395.0 PASS ANNEX 1.1 0.119 204 38.41 C -1.76 1.07 -				
1491 ST F1F1395.0 PASS ANNEX 1.1 0.109 205 5.85 C -2.24 8.45 -				

STAAD Pro fe

ws 20.07.02.15

2						TPL40581	Shest No	a 185	Rev R4b-FAB
>	Software licensed					Panwind speed 32.	m/s		
	ma Belia Swim		19 [44			Ref Fabric RS			7.5
						By TSM	Dale 17-Di	IC-11 Chd	TSM
ient Mall	s Perbandara	Kuanlan				File Q326-KSP-R4b		Date/Time 10-J	
		HETE (UNLE	hecks Cont	1 BATIO/	LOADING/				
	TALE		CAUTICAL COND/	HZ HZ	LOCATION				
	ST P1P1395.0	45.17 C	\$5-4.8.3.3.3 -1.93	0.223	205				
3894	ST PIP1395.0	PASS 13.70 T	83-4.8.2.2	0.113 0.00	2.24				
1895	ST P1P1395.0		85-4.7 (C) -1.17	0.175	201				
1090	ST PIP1395.0	\$5.54 C	85-4.7 (C) -1.15	0.174 0.00	201				
	ST P1P1395.0	1225	MOTEX 1.1	9.142	207				
		64.03 C	-0.55	2.76					
	ST PIP1395.0	PASS 98.37 C	85-4.7 (C) -0.54	0.183	201 0.00				
1899	ST P1P1395.0	PA55 98.49 C	85-4.7 (C) -0.44	0.183	201 0.00				
	ST P1P1395.0	PASS 76.23 C	85-4.7 (C) -0.69	0.139	201				
	ST P1P1395.0	PASS 44.37 C	85-4.8.3.3.3 -1.54	0.130 0.65	201				
	ST PIP1395.0	7355 4.50 C	ANNEX 1.1 -2.56	0.130 0.46	204				
1903	ST P1P1395.0	PASS 124.64 C	85-4.7 (C) -1.44	0.227 0.00	201 1.97				
	ST PIP1395.0	PASS -123.91 C	85-4.7 (C) -1.39	0.226	203	r			
	ST PJP1395.0	PASS 31.32 C	ANNEX 1.1 -0.51	0.137 2.40	207				
	ST PIP1395.0	78.66 C	85-4.7 (C) -0.45	0.146	201 0.00				
1907	ST PIP1355.0	74.55 14.15 C	85-4.7 (C) -0.35	0.146 0.00	201 0.00				
	ST PIP1395.0	PASS 58.00 C	AMMEX 1.1 -0.54	0.134 2.40	209				
	ST P1P1395.0	PASS 38.01 C	ANNEX 1.1 -0.48	0.110 2.13	207				
	ST P1P1395.0	2355 46.70 C	ANNEX J.1 -1.69	0.113 0.74	205				
	ST PIP1395.0	PA33 19.63 C	85-4,7 (C) -1.22	0.182	201				
	ST PIP1395.0	PASS 99.07 C	85-4.7 (C) -1.15	0.181 0.00	201				
	ST P1P1395.0	PASS 91.30 C	85-4.7 (C) -3.12	0.166	201				
	ST P191395.0	PASS ().57 C	ANNEX 1.1 -0.40	0.111 2.21	207				

2					TPL40581	Sheel No	a 186	Rev R4b-FAB	
Software licensed to	Transerve P	la Lid			Partwind speed 32.	5 m/s			
Jeb Title Wisma Belia Swimm				1	Ref Fabric RS				
					By TSM	Cate 17-D		TSM	
Clent Majlis Perbandaran I	Kuanlan				FIN Q326-KSP-R4	-Deg.std	Ostertime 10-J	ul-2012 16;43	
Steel Design (Tra ALL UNITS ARE - KN K MOREK TABLE 1915 ST F1F1395.0	PASS 90,54 C	SS OTHERWISE WOTED CRITICAL COMD/ HT ANNEX I.1 -1.77 85-4.7 [C] -1.06	8ATIO/ HZ 0.117 1.01	203					
1917 ST 9391395.0	FASS 13.72 T	85-4.8.2.2	0.113	1.24					
1910 ST PIP1395.0				105					
1919 57 9391395.0	96.26 C	85-4.7 (C) -1.28	0.175	201 1.57					
1920 ST PIP1395.0		85-4.7 (C) -1.12	0.174 0.00	201					
1921 ST P191395.0		ANNEX 1.1 -1.54	0.476 0.11	208					
1922 ST PIP1395.0	47.56 C	AUMEX 1.1 -1.25							
	PASS 009.23 C	-2.05	0.400 6.50 0.311	204					
1924 ST P191395.4				1.97					
1926 ST #1#1395.0			0.401						
1927 ST P1P1395.0		-2.06 ANNEX 1.1 -1.67	6.51 0.483 6.15	208					
1928 ST P1P1395.0	PASS 12.05 T		0.316	209					
1929 ST 9191686.0	PASS	85-4.7 (C) 0.00	0.533	207					
1930 ST P3P1686.0	7855 75.44 T		0.090 0.00	204					
1931 ST 9191686.0	PASS 45.31 C	85-4.7 (C) 0.00		284 7.35					
1932 ST P3P1606.0		85-4.6 (T) 0.00	0.065 0.00	204					
1933 ST P1P1696.0		0.00	0.240	205					
	PA33 29.28 C	85-4.7 (C) 0.00		200 8.51					
1935 ST PIP1486.0		85-4.7 (C) 0.00		205 7.35					
1936 ST P1P1696.0	PASS 56.65 T	85-4.6 (T) 0.00	0.067 0.00	205					

	Jeb No TPL40581	Sheet No	a 188	Rev R4b-FAB
5	Parlwind speed 32.			
Set Tile Wisma Bella Swimming Pool	Ref Fabric R5	5 m/s		
	By TSM	Dale17-D	ec.11 Chd	TSM
Majils Perbandaran Kuantan	File Q326-KSP-R4		Date/Time 10-J	
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - IN HETE (UNLESS OTHERWISE NOTED)				
HDMER TABLE RESULT/ CRITICAL COND/ RATIO/ LOADING/ FX HY HE LOCATION				
1555 57 P1P14110.0 PATE 85-4.7 (C) 0.458 209 105.34 C 0.08 0.89 13.24				
1940 ST PIP1448.0 PA3S 85-4.7 (C) 0.843 205 148.73 C 0.68 0.00 0.00				
1941 57 7171448.0 FASS B3-4.7 (C) 0.422 289 152.24 C 8.00 0.00 5.55				
1942 ST PIP16810.0 PASS 85-4.7 (C) 0.574 208				
417.15 C 0.66 0.00 0.01 1943 ST P1P2738.0 P3655 85-4.7 (C) 0.472 287 228.39 C 0.69 0.49 0.09				
1964 ST P3P2738.8 PASS 85-4.7 (C) 0.650 205 235.45 C 0.68 0.00 0.00				
1945 ST P1F2734.0 PASS 85-4.7 (C) 0.443 204 321.59 C 0.00 0.00 0.00 0.00				
1966 ST P1P2738.0 PASS B5-4.7 (C) 0.446 207 216.48 C 0.00 0.00 0.00				
1967 5T P1P2738.0 PN55 B5-6.7 [C] 0.631 205 306.44 C 0.00 8.40 0.00				
1944 ST F1F2734.0 FXSS B5-4.7 (C) 0.643 204 312.14 C 0.00 8.00 8.00				
1949 37 F1F2738.0 FASS 85-4.7 (C) 0.419 209 203.73 C 0.09 0.419 20.00 0.00				
1970 ST P1P2738.0 PASS 85-4-7 ICI 0.626 205				
344,20 C 0.88 0.68 0.68 1971 57 FIF2738.0 PASS 85-4.7 (Cl 0.637 204 309.47 C 0.60 0.60 0.60				
1972 ST PTP2738.0 PASS 85-4.7 ICI 6.445 209 216-13 C 6.00 6.00 8.00				
1973 ST P1P2738.0 PASS 85-4.7 (C) 0.431 205 364.55 C 0.00 0.00 0.00				
1974 ST P192738.0 PASS 85-4.7 (C1 0.443 204 312.28 C 0.60 0.00 0.00				
1975 57 9392738.0 PASS 85-4.7 (C) 0.469 209 227,94 C 0.00 0.00 0.0				
1976 ST P1P2738.0 PASS 85-4.7 IC1 0.651 205				
322.34 C 0.08 0.00 6.00				
1976 ST CH5669X16 PASS ANNEX T.1 0.264 204 120.55 C -213,60 196.56 -				
1979 57 CH569X16 PASS JUMEX 1.1 0,475 204 422.27 c -215.33 496.23 -				
1980 ST CH1609X16 PASS ANMEX I.1 0.271 205 143.29 C -220.79 197.98 -				

2					Job No TPL40581	Sheel No	a 189	R4b-FAB
Software Roensed	la Transerve P	ia Lid			Perf wind speed 32.	5 m/s		_
Job Tile Wisma Bella Swim					Ref Fabric R5			3
					BY TSM	Dale 17-D	ec-11 Chd	TSM
Client Majils Perbandaran	Kuantan				File Q326-KSP-R4	-Deg.std	Date/Time 10-Ju	-2012 15:43
Steel Design (Tr ALL UNITS ARE - IN HENRER TABLE	HETE IUNLE		93 PAT10/ H2	LOADING/				
1961 ST CH5609K16		AMONEX 1.3 +222.30	0.482	205				
1942 ST CH5409X16	PASS 550.13 C	AMMEX 1.1 -159.95	0.204	209				
1983 ST CH3695K16	PASS 547.07 C	AMMEX 1.1 -163.02	0.206 153.79	209				
1944 ST CH5609X16	PASS 493.94 T	85-4.0.2.2 -131.07	0.145 0.08	202 3. 66				
1983 ST CH2609X14	PASS 57.54 C	NORX 1.1 -34.51	0.364 526.01	204				
1986 ST CH5689X16	PASS 472.51 T	85-4.4.2.2 -99.85	0.122 0.00	30 3.66				
1987 ST CH3609X16	133.86 C	AMMEX 1.1 -223.44	0.486 527,49	205				
1948 ST CH5603X16	424.56 T	85-4.8.2.2 -101.03	0.117	202				
1965 ST CH5609X16	436.65 7	85-4.6.2.2 -130.50	0.138	202 0.00				
1990 ST CH5405X14	PASS 500.12 T	85-4.4.2.2 -133.32	0.147 0.00	10 3.66				
1991 ST CH1409X14	147.84 C	AMEX 1.1 -7.73	0.353 529.38	204				
1992 ST CH5609X16	PASS 467.80 C	ANNEX 1.1 -4.09	0.128 192.55	201				
1993 ST CH5609X16	507.05 C	AMMEX 1.1 -39.19	0.532 773.54	201				
1994 ST CH5609X16	FASS 676.49 C	85-4.7 (C) -48.08	0.003	203				
1995 ST CH1609X16	PASS (45.52 T	85-4.4.2.2 -132.16	0.140 0.00	10 0.00				
1996 ST CK5605X16	503.93 T	15-4.1.2.2 -138.35	0.151 0.00	202				
1997 ST CH5403X16	FASS 61.34 C	AMIEX 1.1 -1.75	0.336 500.05	204				
1998 ST CH5603X16	PASS 418.07 T	45-4.4.2.2 -117.64	0.127	10 0.00				
1999 ST CH2609X16	FASS 9.51 C	AUGHER 1.1 -70.14	0.428 531.07	205				
2000 ST CH5605X16	7A33 421.25 T	N-4.4.2.2 -33.19	0.073	10 0.00				
2001 ST CH3609X16	PASS 444.18 T	85-4.8.2.2 -137.58	0.143	202				
2002 37 CH5609X16	FASS 494,14 T	85-4.4.2.2 -131.16	0.145 0.00	202				

ws 20.07.02.

TAN SIEW MOI

12					Job No TPL40581	Sheel No	a 190	Rev R4b-FAB
5					Partwind speed 32.			_
ob Tile Wisma Bella Swim		la Lid			Rel Fabric R5	b m/s		
					By TSM	Dale 17-D	ec.11 Chd	TSM
Majlis Perbandaran	Kuantan				File Q326-KSP-R4t			
inger i den der an	(constant				date har her	-Deg.stu	100	01-2012 10.43
Steel Design (Tra	ack 0) C	hecks Cont						
ALL UNITS ANE - IN	-	SS OTHERWISE NOTED	•					
	FX	CAITICAL COMP/	NATIO/	LOADING/				
2003 ST CH3609X16	PASS 57.93 C	ANNEX 1.1 -35.51	0.364 525.99	264				
2004 ST CH5409X16	FA53	85-4.8.2.2	0.122	12				
		-100.22	8.00	3.66				
2005 ST CH5405K16	PASS	ANNEX 3.1 -224.15	0.486	205				
		-44.15	327.73					
2006 ST CH5409X16	PASS 424.74 T	85-4.8.2.2 -101.03	0.117	202				
2007 ST CH5409X16		85-4.9.2.2	0.134	202				
2007 37 CR3403414	436.87 T	-130.97	0.00	0.00				
2006 ST CHE409X14	PASS	ANNEX 1.1	0.264	204				
	130.49 C	-213.94	194.46					
2009 57 CH1609X16	PASS 421.50 C	AINEX 1.1 -215.50	0.475	204				
		***************						
2010 ST CH5403X14	142.33 C	ANNEX 1.1 -220.51	0.270	205				
2011 ST CH5405X16	PARE	ANNEX 1.1		205				
	443.13 C	-221.96	497.33					
2012 ST CH5609X16	PASS	AMMEX 1.1 -162.76	0.106	207				
	550.32 C		153.89					
2013 ST CH5405X16	PASS 547,45 C	AMMEX 1.1 -145.02	0.207	207				
		ANNEX 1.1	0.390	206				
2014 ST PIP40612.5	260.58 C	-132.70	19.26					
2015 ST P1P40612.5		ANNEX 1.1	0.299	206				
		-131.29	20.03	·····				
2016 ST PIP40612.5	PASS 533.56 C	85-4.7 (C) -31.71	0.138	201				
				*******				
2017 ST PIP40412.5	547.75 C	85-4.7 (C) -35.38	0.147 0.00	201 0.00				
2018 ST P1P40412.5		NS-4.7 (C)	0.157	201				
	405.13 C	-31.15	0.00	0.00				
2019 ST P1P40612.5	PASS	85-4.7 (C)	0.190	201				
			0.00	0.00				
2020 ST 91940412.5	PASS 486.53 C	85-4.7 (C) -22.94	0.126	201 0.00				
			••••••					
2023 ST P1P40412.5	589.98 C	85-4.7 (C) -41.85	0.153 0.00	201 0.00				
2022 ST PIP40612.5	PASS	85-4.7 (5)	0.128	201				
	533.41 C	-31.72	0.00	0.00				
2023 57 91940612.5	PASS	85-4.7 (C) -39.39	0.147	201				
	*********							
2024 ST P1P40612.5	PASS 241.69 C	AUDIEX 1.1 -133.69	0.303	200				



8	TPL40581 Sheet No a 187 R4b-				
Software licensed to Transerve Pie Ltd	Padwind speed 32.5	5 m/s			
Jeb Title Wisma Belia Swimming Poel	Ref Fabric R5				
	By TSM	Dale17-Dec-	11 Che	TSM	
Clent Mallis Perbandaran Kuantan	File Q325-KSP-R4b	-Deg.std D	alama 10-J	ul-2012 15:43	

### on (Track 0) Checks Cont.. Steel D

CORCA.	S ARE - IN TABLE	RESULT/	CRITICAL COND/	BATIO/	LOADING/
CHICK.	TABLE	FX	KT KT	H1	LOCATION
1937	ST PIP1686.0	7A55 204.92 T	85-4.6 (T) 0.00	0.244 0.00	206
1938	ST P3P1686.0	PASS 122.91 C	85-4.7 (C) 0.00	0.533	209
1929	ST PIP1686.0	PASS 75,71 7	85-4.6 (7) 0.00	0.050	204
1940	ST PIP1686.0	PASS 145.79 C	83-4.7 (C) 6.00	0.00	284
1943	ST PIP1686.0	PA55 54.10 T	85-4.6 (7) 8.00	0.064	204 0.00
1942	ST P1P1686.0	PASS 205.43 T	35-4.6 (T) 0.00	0.246	205
1943	ST P391686.0	PASS 21.11 C	85-4.7 (C) 0.00	0.135	206
1944 :	ST PIPLEES.0	PASS	35-4.7 (C)	0.437	205
1945 :	ST 9191686.0	PAES 56.77 T	85-4.6 (7)	0.067	205
1946 1	ST PIP1686.0	PASS 204.71 T	85-4.6 (7)	0.243	208
1947 :	ST P1P16810.0		85-4.7 (C) 0.00	0.477	207
1948 1	T P1P1688.0	PASS 191.75 C	85-4.7 (C) 0.00	1.894	204
1949 1	T PIPIGOR.0	PASS	85-4.7 (C) 0.00	0.626	207
1950 :	T PIP16810.0	163.39 C	85-4.7 (C)	0.962	206
1951 2	T P1P16818.0	411.85 C	0.00 85-4.7 (C)	0.00	207
1952 1	T PIPI 688.6	187.35 C	0.00 85-4.7 (C)	0.00	205
1953 0		187.53 C	8.00 83-4.7 (C)	0.45	0.00
	T PIPIERIO.0	164.30 C	0.00	0.00	9.55
	T P1P16810.0	417.21 C	0.00 85-4.7 (C)	0.60	0.00 209
		108.91 C	0.00	0.00	11.26
	T PIP1668.0	153.43 C	6.00	0.00	0.00
	T PIP1608.0	PASS 161,35 C	85-4.7 (C) 0.00	0.618	209
1958 3	T P3P14810.0	PASS (11.91 C	85-4.7 (C) 0.00	0.962	204

TAAD, Pro for Windows 20.07.02.1

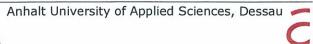
2	TPL40581 Sheet No Rev R4b-F/					
Software Reensed to Transerve Pie Lid	Partwind speed 32.5 m/s					
<ul> <li>Wisma Bella Swimming Pool</li> </ul>	Ral Fabric R5					
	By TSM Dall 17-Dec-11 Chd TSM					
Matter Ontaria Karalan						

eel	Design	(Track	0)	Checks	Cont

HARA TABLE	RESULT/	CRITICAL COND/	RATIO/	LOADING/
	R	HT HT	HZ	LOCATION
2025 57 91940612.	5 PASS 263.95 C	ANNEX 1.1 -132.31	0.302 20.17	201
2026 ST CH3409816	PASS 684.97 C	AMMEX 1.1 -21.41	0.252 356.24	203
2027 57 CH5403814	PASS 582.25 C	ANNEX 1.1 -23.46	0.207	201
2028 ST CH5409X14	PASS 271.74 C	ANNEX 1.1 -206.25	0.153 29.94	206
2029 ST CH5409X16	7A55 273.91 C	AMMEX 1.1 -204.06	0.152 31.16	204
2030 57 045609816	PASS 380.67 T	85-4.8.2.2 -33.43	0.058 0.00	10 0.00
2031 ST CH5409814	PASS 354.73 T	85-4.8.2.2 -37.87	0.073 0.00	10 0.00
2032 ST CH5609X16	PASS 617.92 C	85-4.7 (C) -48.41	0.67E 0.00	201
2033 ST CH5609X16	PASS 747.13 C	85-4.7 (C) -81.57	0.092	201 0.00
2034 ST CH5609X16	PASS (39.26 C	85-4.7 (C) -35.65	0.061	201
2035 ST CH1609X16	PASS 412.74 T	85-4.8.2.2 -40.75	6.877	12 0.00
2036 ST CH5409K16	PA35 386.81 T	85-4.8.2.2 -33.42	0.044	12 0.00
2037 ST CH3409X14	PASS 391.16 T	85-4.8.2.2 -37.84	0.073	12 0.00
2038 ST CH5609K16	73.55 272.15 c	AMEX 1.1 -207.75	0.154 30.13	205
2029 ST CH1609X16	PASS 275.11 C	ANNEX 1.1 -205.64	0.154	201
2040 ST CH5609K16	PASS 154.10 C	ANNEX 1.1 -49.43	0.296	204
2041 ST CH3603X16	PASS 154.05 C	ANNEX 1.1 -52.18	0.294	204
2042 57 9192736.0	PASS 352.43 C	AMMEX 1.1 -12.11	0.593	206
2043 57 \$1\$2736.0	PASS 188.43 C	85-4.7 (C) -7.55	0.201	206
2044 ST 7172736.0	PASS 553.40 C	85-4.7 (C) -15.46	0.590	206
2045 ST P1P2736.0	PASS	85-4.7 (C)	0.225	204
	215.19 C	-7.47	0.00	0.00

Voi TonalDale: 1

STAAD Pro for Windows 20 07 02 15



$\mathcal{D}$	TPL40581	Sheel No	a 192	Rev R4b-FAB
5	Partwind speed 32.	5-10		
THe Wisma Belia Swimming Pool	Ref Fabric R5	JAVS		
	BY TSM	Dak17-D	mc-11 Chd	SM
Majlis Perbandaran Kuantan	F# Q326-KSP-R4			2012 16:43
majna r ci barbaran	dere-filer -free	begand	10-94	2012 10.43
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - NN HETE (UNLESS OTKERWISE NOTED)				
HEMBER TABLE RESULT/ CALTICAL COMD/ RATIO/ LOADING/ FX NY HL LOCATION				
2047 ST F1F2736.0 FASS B5-4.7 IC1 0.108 205 103.28 C -3.88 0.00 0.00				
1044 ST \$197736.0 FASS 85-4-7 (F) 0.207 706				
193.50 C -4.33 0.60 0.60				
2049 ST F1F2736.0 FASS 85-4.7 (C) 0.185 205 39.57 C -2.45 0.00 0.00				
2050 37 FIF2736.0 FASS B5-4.7 (C) 0.127 208 115.46 C -4.11 0.00 0.00				
2051 ST PTP2736.0 PARS 85-4.7 ICI 0.176 206				
118.44 C -4.14 0.00 0.00				
2052 57 P1P2736.0 PASS AMREX 1.1 0.896 206 89.42 C -6.35 2.82 -				
2053 ST F1F2736.0 FASS 85-4.7 (C) 0.095 208 89.00 C -2.52 0.00 0.00				
2054 ST 9192736.0 PASS 85-4.7 (C) 0.108 208				
101.73 C -3.28 0.00 0.00				
2055 57 9192736.0 PASS 85-4.7 (C) 0.186 208 174.38 C -1.86 0.00 0.00				
2054 ST P1P2736.0 PASS 85-4.7 (C) 0.106 208 95.31 C -4.00 5.00 0.00				
2057 ST P1P2736.0 PASS 85-4.7 (C) 0.206 204				
193.11 C -2.28 0.00 0.00				
2058 ST PJP2736.0 PASS 85-4.7 (C) 0.202 208 189.38 C -5.37 0.00 0.00				
2059 ST P1P2736.0 PASS AWNEX 1.1 0.598 208				
2059 ST P17735.0 PASS AVEL 1.1 0.558 208 551.94 C -12.08 10.34 -				
2060 ST 9192736.0 PASS 85-4.7 (C) 0.230 200				
215.74 C -4.39 0.60 0.60				
2043 ST F1F2734.0 FASS 85-4.7 (C) 0.549 209 532.54 C -7.58 0.00 0.00				
2062 ST CH5219X9.0 PASS 85-4.7 (C) 0.394 202 141.48 C 0.00 0.00 13.05				
2063 ST CH5219X9.0 PASS 85-4.7 (C) 0.397 202 140.51 C 0.00 0.00 13.05				
2064 5T CH5213X3.0 PASS 33-4.7 (C) 0.332 202 118.66 C 0.00 0.09 13.65				
2045 ST CH5219X9.0 PASS 85-4.7 (C) 0.345 202				
2046 ST CHS219X3.0 PASS 83-4.7 (C) 0.123 5 25.48 C 0.00 0.00 0.00				
2867 ST EKS219X9.0 PASS 85-4.7 (C) 0.125 4 23.57 C 0.00 0.85 0.00				
2008 ST CHS215X8.0 PAGS 85-4.7 (C) 0.291 10				
103.26 C 0.00 0.00 0.00				

$\mathcal{D}$						100 No TPL40581	sheet.No a 193	Rev R4b-FAB
$\mathbf{D}$						Partwind speed 32.	E m/r	
	otware Ecensed I a Bella Swimi		te Lid			Ref Fabric R5	5 1125	
						BY TSM	Dale17-Dec-11 Ch	TSM
<sup>1</sup> Mallis	Perbandaran	Kuantan				Ple Q326-KSP-R4t		Jul-2012 16:43
ALL UNIT HOMER 2069 2070 2071 2072 2072 2073	TABLE TABLE ST CKS219X9.0 ST CKS219X9.0 ST CKS219X9.0 ST CKS219X9.0 ST CKS219X9.0	ETE (UNLE RESULT/ 72 134.07 C 101.58 C 103.58 C	0.00 33-4.7 (C) 0.00 85-4.7 (C) 0.00 85-4.7 (C) 0.00	8A710/ HZ 0.345 8,60 0.303 0.00 0.358 0.00 0.358 0.00 0.325 0.32 0.265 0.462 0.462 0.462	12353967/ 146231281 2 3 4 12 3 4 13 4 13 4 13 4 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 4 5 13 13 13 13 13 13 13 13 13 13 13 13 13			
2076 2	ST CH3219X9.0 ST CH5219X9.0	PASS 24.23 C PASS 22.16 C	0,00 85-4.7 (C) 0.00 85-4.7 (C) 0.00		13.05 3 0.00			
2079 1	IT P1P1686.0	PASS 201.40 7 PASS 208.06 C	85-4.7 (C) -6.75	0.436 6.00 0.449 0.00	201 5.50 202 5.50 205			
	IT PIPIERE.0	244.35 T	85-4.8.2.2 -1.55 85-4.7 (C) -6.72	0.00	5.75			
2082 5	T PIPIESE.0	PASS 183.91 C	85-4.7 (C) 0.00	0.397	5.30 18 8.00			
	T PIP1686.0		85-4.7 (C) -7.38 85-4.7 (C) 0.09	0.377 0.00 0.370	202			
2085 5	T PIPI686.0	PASS	ANNEX 1.1	0.00	0.00 202			
2086 5	T PIP1686.0		85-4.8.2.2 -5.96	0.520	201 5.90			
2047 5	T PIP1686.0	PASS 163.74 T	85-4.8.2.2 -4.30	0,412 0,00	201			
	T PIP1686.0		85-4.8.2.2 -0.52	0.324 0.00	201 5.75			
2089 5	T PIP1685.0	PASS 121.52 T	85-4.8.2.2 -5.96	0.520 0.00	201 5.90			
2050 5	T PIP1685.0	PASS	ANNEX 1.1 -7.66	0.417	202			

				Job No TPL40581	Sheet No a 194	Rev R4b-FAB
$\leq$				a state of the second		N40-TAD
Software licensed to Transer				Partwind speed 32.	5 m/s	
Tile Wisma Bella Swimming Po	ol		Ref Fabric R5		TSM	
		By TSM	Dale 17-Dec-11 C			
ent Majlis Perbandaran Kuanta	n			C326-KSP-R4	Sedegista lana internet 10-	JUI-2012 16:43
Steel Design (Track 0) ALL UNITS ARE - KR HETE KU HOHER TABLE AESUL	HLESS OTHERWISE NOTES	NATIO/	LOADING/			
244) ST PIPIERE 8 745	NT 5 85-1.7 (C)	HI 0.342 9.00	202			
154.79		9.00	5.90			
2092 ST PIP1686.8 PA3 164.43		0.342	202			
2035 57 PIP1484.0 PAS 187.55		0.418	202			
2094 ST P1P1686.0 PAS 175.57	S ANNEX 1.1 C -7.46	0.354 1.27	202			
2095 ST P1P1686.0 PAS 175.88	c -7,38	0.379	202 5.90			
2096 ST PIP1686.0 PAS 176.86	s #5-4.7 (C) C 0.66	0.368	202			
2097 ST PIP1685.0 PAS 183.85	s 85-4.7 (C) C 0,00	0.397	12 0.00			
2096 ST P1P1686.0 PAS 284.73	s 85-4.8.2.2 7 -4.42	0.440	201 5.90			
2035 57 PIP1686.0 PAS 210.11		0.453 0.00	202			
2100 ST PIP1486.0 PAS 270.21	5 85-4.4.2.2 T -1.57	0.357	207			
2101 ST PIP1686.0 PAS 208.53	s BS-4.7 (C) C -6.71	0.450	202			
2102 ST PIPIGOC.0 PAS 212.34	s 85-4.7 (C) C -5.28	0.442	202			
2103 ST P1P1404.0 PAS 214.17	5 85-4.7 (C) C 0.00	0.446	202 3.75			
2104 ST PJP1686.0 PAS 280.48	\$ 35-4.4.2.2	0.433	201 5.75			
2105 ST P191686.0 PAS 279.77		0.433	201			
2106 ST P1P1686.0 PAS 174.48		0.367	202			
2107 ST P1P1484.0 PAS 175.42		0.378 0.00	10			
2104 ST PIP1646.0 PAS 176.25		0.367	202			
2109 ST P191606.0 PAS	5 BS-4.7 [C]	0.310	202			
2110 ST PIP1646.0 PAS 264.06	*******************	0.413	203			
2311 ST PIP1484.0 PAS 244.07		0.413				
2112 ST P1P1686.0 PAS 263.71		0.412	201			
263.71	T -4.30	0.00				

2			Jeb No TPL40581	Sheet No a 196	Rev R4b-FAB
Software licensed to Transervo Pie Lid			Partwind speed 32.	5 m/s	
Job Title Wisma Bella Swimming Pool			Ref Fabric R5		
			By TSM	Dalt17-Dec-11 Ch	d TSM
Client Majilis Perbandaran Kuantan				-Deg.std Date/Time 10-	
					101 2012 10.40
Steel Design (Track 0) Checks Cont					
ALL UNITS ARE - HO HETE (UNLESS OTHERWISE HOTED)					
HENBER TABLE NESULT/ CRITICAL COND/	MATIO/	LOADING/			
		LOCATION			
2135 ST 9191644.0 PA35 85-4.7 (C) 184.28 C -2.46	0.384	10			
2136 ST P1P1606.0 PASS ANNEX 1.1 102.20 C -7.46	0.386	202			
	0.385	202			
184.84 C 0.00	0.00	3.75			
2138 ST P2P1686.0 PASS 85-4.8.2.2 321.79 T -5.96	0.570	201			
	0.00	0.00			
2135 ST PIP1484.0 PASS 85-4.8.2.2 315.51 T -1.36	0.411	201			
	0.00	0.00			
2140 ST P1P1446.0 PASS 85-4.8.2.2 321.51 T -5.96	0.520	201			
2141 ST PIP1486.0 PASS 85-4.8.2.2 320.03 T -1.36	0.412	201			
2142 ST P1P1686.0 PASS ANNEX 1.1 188.24 C -7.65	0.407	202			
	0.397	282			
	0.00	5.75			
2144 ST PIP1486.0 PADS AMMIX I.1 188.86 C -7.65	0.405	242			
148.44 C -7.45	1.29				
2145 ST PIP1446.0 PASS B5-4.7 (C) 193.50 C 0.00	0.359	202			
	*******				
2146 ST PIPI686.0 PASS ANNEX I.1 . 181.21 C -7,46	0.385	202			
2347 5T #191486.0 PASS 85-4.7 [C] 183.84 C 0.00	0.383	202 5.75			
2148 ST P1P1686.0 PARS ANOTOX 1.1 182.04 C -7.46	0.386	202			
	1.25				
2145 ST P1P1486.0 PASS 85-4.7 (C) 184,68 C 0.00	0.384	202			
	0.00	5.75			
2150 ST P1P1646.0 PASS 85-4.7 (C) 269.92 C 0.00	0.451	202			
2151 37 PIP1686.0 PASS 85-4.8.2.2 131.97 T -3.36	0.306	201 5.17			
2152 ST PIP1686.0 PASS 85-6.7 (C) 271.53 C -0.21	0.492 0.00	262			
2153 ST P1P1686.0 PASS B1-6.8.2.2 390.61 T -3.36	0.363	201			
130.61 7 -3.34	0.00	5.19			
2154 ST PIP1696.0 PASS 85-4.8.2.2	0.217	201			
144.21 7 -1.99	0.00	4.45			
2155 ST P1P2686.0 PASS 85-4.4.2.2 144.48 T -1.99	0.217	201			
144.47 -1.39					
2156 ST P1P1686.0 PASS 85-4.8.2.2 150.16 T -3.11	0.255	201 5.17			

	TPL40581		a 197	R4b-FAB
	Partwind speed 32.	Emle		
Software licensed to Transarve Pie Ltd so Tree Wisma Bella Swimming Pool	Ref Fabric RS			
	By TSM	Date17-De	10-11 Chd	TSM
Majlis Perbandaran Kuantan	FTe Q325-KSP-R4	b-Deg.std	Date/Time 10-Ju	-2012 16:43
Steel Design (Track 0) Checks Cont				
ALL UNITS ARE - KN HETE (UNLESS OTHERWISE HOTED)				
HDIBER TABLE RESULT/ CRITICAL COMD/ RATIO/ LOADING/ TX HY HI LOCATION				
2157 3T PIP1694.0 PASS B5-4.4.2.2 D.251 201 350.47 T -3.11 0.00 5.15				
2156 ST P1P1686.0 PA35 85-6.7 (C) 0.263 12 104,75 C 0.00 0.00 0.00 0.00				
2155 ST P2P1486.0 PASS 85-4.7 ICI 0.256 10 101.01 C 0.00 0.00 0.00				
2140 ST P1P1446.6 PASS 85-4.8.2.2 0.215 201 194.99 T -2.41 6.00 5.17				
2143 ST P1P1486.0 PASS B5-4.0.2.2 0.215 201 199.00 T -2.41 0.00 5.19				
2147 5T P1P3484.0 FASS 85-4.7 (C) 0.264 202 105.23 C 0.06 8.00 8.00				
2163 ST P1P1686.0 PASS 85-6.7 (C) 0.267 202				
2164 57 9291686.0 955 85-4.9.2.2 0,258 201 155.53 7 -2.14 0.00 5.17				
2145 ST PIP1444.0 PASS B5-4.8.2.2 0.258 201 156.32 T -3.15 6.80 5.19				
2146 57 PTP1686.0 PA55 86-4.8.2.2 0.217 201 142.69 7 -1.99 0.00 4.65				
2147 ST P1P1444.0 PASS 85-4.8.2.2 0.218 201 144.71 7 -1.59 0.00 4.45				
2144 ST P1P1444.0 PASS 85-4.8.2.2 0.250 201 150.46 T -3.11 0.00 5.17				
2149 57 7191446.8 PASS 85-4.8.2.2 0.251 201 150.53 7 -3.11 0.00 5.19				
2170 ST PIP1686.0 PASS 85-4.7 (C) 0.453 202 271.05 C 0.60 0.00 0.00				
2171 57 PTP1646.0 PASS 85-4.8.2.2 0.364 201 133.50 T -3.37 0.00 5.17				
2172 ST PIPJ646.0 PASS 85-4.7 [C] 0.492 202 271.63 C -0.22 0.09 5.17				
2173 ST PIP1484.0 PASS 85-4.8.2.2 0.355 201 192.14 T -3.25 0.60 5.19				
2174 ST 7171646.0 PASS 85-4.7 (C] 0.491 202 271.44 C -9.21 0.09 0.00				
2175 ST PIP1496.0 PASS 85-4.8.2.2 0.364 201 191.40 T -3.34 0.80 0.50				
2176 ST PIP1686.0 PASS 85-4.8.2.2 0.217 201 144.42 T -1.99 0.00 0.00				
2177 2T PIP1666.0 PASS 85-4.8.2.2 0.217 201 144.25 T -1.93 0.00 0.00				
2178 57 9191686.0 PASS 85-4.8.7.2 0.718 201 144.14 7 -1.95 0.00 0.00				

TAN SIEW MOI

						TPL40581		a 198	R4b-F
						Parlwind speed 32			1000
to Title Wisma Be		to Transerve P micon Pool	in Lid			Ref Fabric R5	LO TIVE		
Traine Or	the Official	nang r oor				By TSM	Delt17-D		TSM
iant Majlis Peri	andaran	Kuanlan				File Q326-KSP-R			-Jul-2012 16:4
mana r cr	and a lan	Keaman				4320-KSF-K	10-12 eg. 510	1	-JUI-2012 16:4
			hecks Cont						
			SS OTHERWISE NOTE						
HEHSEN T			CRITICAL COMD/	HATIO/	LOCATION				
2179 57 8									
4/9 57 1		143.94 7	85-4.8.2.2 -1.99	0.217 0.00	201 0.00				
2180 ST P		-	85-4.4.2.2	0.306	201				
		192.90 T	-3.35	0.00	0.00				
210) ST P	71696.0	PASS 272.60 C	85-4.7 (C) -0.22	0.494	202				
	•••••								
2182 ST P	P1686.0	PASS 270.02 C	85-4.7 (C) 0.00	0.491	202 5.19				
2183 ST P			85-4.9.2.2	0. 104	201				
		193.16 T	-3.36	0.00	8.00				
2184 ST P1	P1 64 6.0	PASS	85-4.8.2.2	0.251	201				
		150.94 T	-3.11	0.00	8.00				
2185 57 91	P1496.0	PASS	85-4.8.2.2	0.250	201 0.00				
2186 57 93	P1686.0		85-4.8.2.2 -3.41	0.315	201				
2187 ST P1	P1 64 6.0	PASS	85-4.8.2.2	0.315	201				
		198.93 T	-3.41	0.00	0.00				
2148 ST P1	71686.0	PASS	85-4.8.2.2	0.258	201				
		156.40 7	-3.15	0.00	0.00				
2169 ST PE	P1686.0	PASS 155.87 T	85-4.8.2.2 -3.15	0.258	201				
2196 ST P1	P1686.0	PASS 150.59 T	85-4.8.2.2 -3.11	0.251	201 0.00				
2141 57 91		mer	85-4.8.2.2	0.250	201				
2191 57 91		150.40 7	-3.11	0.00	0.00				
2192 57 91		1355	85-4.8.2.2	0.307	261				
		192.72 7	-3.37		0.00				
2193 ST PI	1686.0	7A55 270.30 C	85-4.7 (C) 0.00	0.492	202				
2194 ST CH	-JX5.16	PASS 0.01 C	85-4.8.3.3.3 -0.88	0.283	10				
2195 ST CH		PASS	ANNEX 1.1	0.095	205				
		0.00 C	-0.48	6.14					
2196 ST CH	73x5.16	PASS	AND/EX 1.1	0.020	206				
			-0.05	0.00	·····				
2197 ST CH		0.25 C	AMONEX 1.1	0.029	206				
2198 ST CK	72X5.16		ANNEX 1.1 -0.04	0.017	204				
2199 ST CH		2255	AMER 1.1	0.625	201				
			-0.07	0.03					
2200 ST CH			AMOUTY 1.1	0.096	208				
		0.05 C	-0.49	0.14					



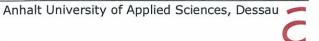
2	Job Ne TPL40581	Sheet No a 195	Rev R4b-FAB
Software licensed to Transerve Pile Ltd	Partwind speed 32.	5 m/s	
Wisma Belia Swimming Pool	Ref Fabric R5		
	BY TSM	Dale 17-Dec-11 Che	TSM
Majlis Perbandaran Kuantan	Fle Q326-KSP-R4	b-Deg.sld Date/Time 10-J	ul-2012 16:43

### n (Track 0) Checks Cont.

UNITE ANE - IN		SE OTHERWISE NOTED		
ICR TABLE	RESULT/ FX	CAITICAL COND/	N.110/ H1	LOCATION
1113 ST P1P1646.	0 7A35 160.57 C	85-4.7 (C) -2.31	0.334 0.00	12 0.00
2334 ST P393686.	0 PASS 283.44 T	85-4.8.2.2 -4.34	0.437 0.00	201 5.75
115 ST P171686.	0 PASS 212.60 T	85-4.8.2.2 -4.37	0.436 0.00	201
116 ST P1P1686.	0 FASS 214.52 C	85-4.7 (C) -5.31	0.447 0.00	702 5.75
117 ST PIP1646.	PASS 214.34 C	85-4.7 (C) 0.00	0.450	202
118 ST PIP1686.	PASS 211.97 C	05-4.7 (C) -5.28	0.441	202 5.75
119 ST P1P1686.	0 PASS 213.80 C	85-4.7 (C) 0.00	0.445	202
120 ST PIP1686.	0 PASS 242.50 T	85-4.8.2.2	0.437 8.60	201
121 ST PJP1686.	PA55 269.16 T	85-4.8.2.2 -1.56	0.356	205
123 57 9393686.0	0 FASS 285.57 T	85-4.8.2.2 -4.39	0.440	201
123 ST P1P1686.0	PASS 270.78 T	85-4.8.2.2 +1.59	0.356	207
124 ST PIP1686.0	PASS 212.90 C	85-4.7 (C) -5.38	0.443	202
25 57 9391686.0	PASS 214.74 C	85-4.7 (C) 0.00	0.447	202
126 57 9191696.0	PASS 143.00 C	83-4.7 ICI -4.66	0.339	202
127 ST PIPI696.0	PASS 161.67 C	85-4.7 (C) -6.95	0.345	202
28 ST PIPL686.6	PA35 160.04 C	85-4.7 (C) -4.62	0.333	202
29 ST P1P1686.0	PASS 141.37 C	85-4.7 (C) 0.00	0.336	202
30 ST PIP1606.0		NS-4.7 (C) -4.65	0.345	202
31 ST P1P1606.0		85-4.7 (C) -7.28	0.376	262
32 ST PIPI686.0		85-4.7 (CI -4.87	0.369	202
33 ST P1P1686.0		85-4.7 [C] 0.00	0.372	202
34 ST P3P1444.0		ANNEX 1.1 -7.46	0.385	202

2	Jeb No TPL40581	Sheet No.	a 199	Rev R4b-FAE
Software licensed to Transerve Pie Ltd	Partwind speed 32.	5 m/s		
Job Title Wisma Bella Swimming Pool	Ref Fabric R5			
	BY TSM	Dele17-D	ec-11 Che	TSM
Cleni Mallis Perbandaran Kuantan	Fie Q326-KSP-R4	b-Deg.std	Date/Time 10-	ul-2012 16:43

ALL UNITS			hecks Cont		
HEHBER	TABLE	MESULT/	CAITICAL COND/	AATIO/	LOADING.
	••••••				
2201 5	T CHS73X5.16	PASS 0.01 C	85-4.8.3.3.3 -0.89	0.205	12
2202 5	T CHS73X5.16	PASS 0.04 C	ANNEX 1.3	8.094	206
2203 5	T CH373X5.16	PASS 0.01 C	#5-4.4.3.3.3 -0.48	0.279	10
2204 5	T CHS73X5.16	PA55 0.08 C	ANNEX 1.1	0.495	206
		0.08 0			
2205 5	T CHS73X5.14	PASS 0.01 C	85-4.4.3.3.3 -0.89	0.243	12
2206 5	T CHE73X5.16	PASS 0.00 C	AMIEX 1.3 -0.04	0.018	206
			******		
2207 5	T CHS73X5.16	PA53 0.24 C	AMMEX 1.1 -0.07	0.025	206
2208 5	CHS73X5.16	PA33 0.00 C	AMMEX 1.1 -0.05	0.020	208
1965 5	CHS73X5.16	PASS	ANNEX 1.1	0.029	204
1103 5	05/363.14	0.25 C	-0.08	0.10	
2210 5	CHS73X5.14	PASS 0.00 C	ANNEX 1.1	0.021	206
		0.00 C	-0.05	0.09	
2211 51	CHS73X5.14	PASS 0.25 C	ANNEX 1.1 -0.09	0.031 0.11	206
2212 51	CHS73X5.16	PASS 0.08 C	ANNEX 1.1 -0.64	0.018	206
2213 51	CHS73X5.16	PASS 0.22 C	AMMEX 1.1 -0.07	0.025	205
	*****				
2214 51	CHS73X5.14	PASS 0.87 C	ADOREX 1.1 -0.04	0.020	208
1115	CHS73X5.16	PARE	AINER 1.1	0.076	208
		0.26 C	-0.07	0.10	
2216 51	CHS73X5.16	PASS 0.07 C	ANNEX 1.1 -0.05	0.021	208
	•••••				
2217 51	CHS73X3.16	PASS 0.25 C	AMMEX 1.1 -0.05	0.031 0.11	200
	CHS73X5.16	PASS	85-4.4.3.3.3	0.256	10
1210 31		8.00 C	-0.78	0.44	
2219 57	CHS73X5.16	PASS 0.14 T	85-4.8.2.2	0.009	205
2220 57	CHS73X5.16	PASS 0.14 T	25-4.8.2.2 -0.06	0.009	209
2221 51	CHS73X5.16	PASS 0.00 C	85-4.0.3.3.3 -0.75	0.257 0.44	12
2222 57	CH573X5.16	PASS	85-4.8.3.3.3	0.255	10
		0.00 C	-0.78	0.44	



8				TPL40581	Sheet No	a 200	Rev R4b-FAE
Software licensed to Transerv	Pie Lid			Partwind speed 32.5	m/s		
to Title Wisma Bella Swimming Poo	al de la companya de			Ref Fabric R5			
				By TSM	Dale17-D	lec-11 Chd TS	м
Majlis Perbandaran Kuantan				Fle Q326-KSP-R4b	Deg.std	Date/Tima 10-Jul-2	012 16:43
	LESS OTHERWISE NOTE		LOADING/				
2223 ST CR573X5.16 PASS	85-4.4.2.2.3	0.013	10				
0.03 C	85-6.1.3.3.3	0.02					
0.03 C	-0.03	0.62					
0.03 c		0.010 0.02	12				
2226 ST CHS73X5.16 PASS 0.03 C	85-4.8.3.3.3	0.013 0.02	12	<i>.</i>			
2227 ST CH572X5.16 PASS 0.00 C	85-4.8.3.3.3 -0.79	0.256 0.44	12				
2228 ST P1P2198.0 PASS 436.67 C	ANNEX 1.1 -28.15	0.757 24.08	202				
2229 ST P1P2198.0 PASS 435.89 C	ANNEX 1.1	0.755	202				
2230 ST PIP2198.0 PASS 435.36 C	AMMEX 1.1 -28.10	0.761	202				
2231 ST PIP2198.0 PASS 476.25 C	ANNUEX 1.1 -13.50	0.755 30.45	204				
2232 ST PIP2136.0 PASS 243.26 T	BS-4.6 (T)	0.220	206				
2233 ST P1P2198.0 PASS 279.06 C	BS-6.7 (C)	0.00	204				
2234 ST PIP2196.0 PAd3	0.00 B5-4.6 (T)	0.00	0.00				
244.05 7	0.00	0.00	12.23				
2235 ST PIP2198.0 PASS 241.11 C	85-4.7 (C) 0.00	0.722	206				
2236 5T PIP2196.0 PASS 364.67 T	85-4.6 (7) 0.00	0.330	205				
2237 ST FIF2196.0 FASS 350.05 T	85-4.6 (T) 0.00	0.317	204				
2238 ST P1P2156.0 PASS 29.18 T	BS-4.6 (T) 0.00	0.026	206				
2235 ST PIP2156.0 PASS 69.25 C	85-4.7 (C) 0.00	0.130	206				
2240 ST PIP2186.0 PASS 66.36 T	85-4.6 (7)	0.00	206				
2241 ST PIP2194.0 PASS	0.00 85-4.7 (C)	0.00	12.23				
77.69 C	0.00	0.00	0.00				
14.02 C	85-4.7 (C) 0.00	0.030	206				
2243 ST PIP2196.0 PASS 15.33 C	85-4.7 (C) 0.00	0.033	208				
2244 57 PIP2196.0 PASS 0.93 C	85-4.7 (C) 0.09	0.032	201				

STAAD.Pro for Windows 20.07.02.15

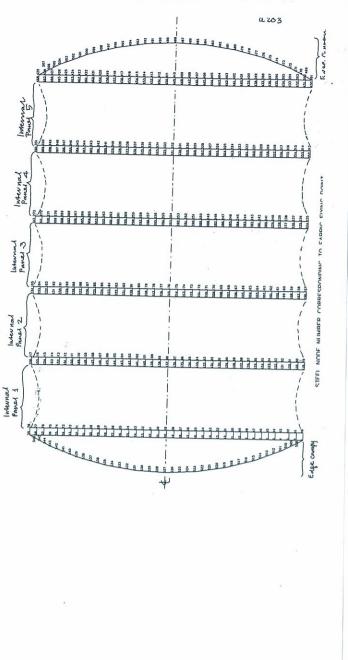
2					Jeb No TPL40581	Sheel No a 201	Rev R4b-FAB
Software Ec	insed to Transer	ve Pla Lid			Partwind speed 32.5	i m/r	
Tile Wisma Bella S	Swimming Pa	ol			Ref Fabric R5	1123	
					By TSM	Dels17-Dec-11 C	M TSM
Majlis Perband	laran Kuanta	n				-Deg.std Date/Time 10	TSM
					Q320-K3P-K4D	-Deg.std Users into 10	-Jul-2012 16:43
Steel Design	(Track 0)	Checks Cont					
		LESS OTHERWISE NOTE					
HENBER TABLE	RESULT	CRITICAL COND/	PATIO/	LOADING/			
••••••			HZ	LOCATION			
2245 ST PIP21	9.12	85-4.7 (C) C 0.80	0.033	201 0.00			
2246 ST PIP215	4.0 PASS	85-4.7 (C)	0.129	208			
	39.64	C 0.50	0.00				
2247 ST PIP219	6.0 PASS	85-4.6 (7)	0.026	209			
		0.00	0.00	11.25			
2248 ST P1P219	6.0 PASS 76.76	85-4.7 (C) 0.00	0.276	205			
			0.00	0.00			
2249 ST P1P219		85-4.6 (7)	0.059	205			
2250 ST PIP219			**********				
	277.72 0		0.669	208			
2251 ST PIP2196	.0 PASS	B5-4.6 (7)	0.219	208			
			0.00	12.23			
2252 ST PIP2198	.0 PASS	85-4.7 (C)	0.719	208			
		0.00	0.00	0.00			
2253 ST PIP2194	0 PASS 242.98 T	85-4.6 (T) 0.00	0.220	208			
			0.00	12.23			
2254 ST PIP2196	0 PASS 362.71 T	85-4.6 (T) 0.00	0.328	205			
2255 ST PIP2196	348.58 T	85-4.6 [T] 0.00	0.315	204 12.05			
2256 ST 8016	PASS		0.456	204			
	25.21 1	85-4.6 (T) 0.00 -	0.00	0.00			
2257 ST RD16	PASS	83-4.6 (T) 0.00	0.000	204			1
	0.00	0.00	0.00	0.00			
2258 ST R016	PASS 23.77 T	83-4.6 (T) 0.00	0.430	205			
			0.00	0.00			
2259 ST RD16	PASS 0.00	85-4.6 (T) 0.00	0.000	205			
2260 ST 8016				0.00			
	PASS 4.43 T	83-4.6 (7) 0.00	0.087	204			
2261 ST RD16	PASS		0.119				
	6.58 T	85-4.6 (T) 0.00	0.00	204			
2262 ST 8016	PASS	83-4.6 (T) 0.00	0.001	205			
	4.46 T	0.00	0.00	0.00			
2263 ST RD16	PASS 5.56 T	85-4.6 (7) 0.00	0.101	205			
	5.56 7	0.00	0.00	0.00			
2264 ST RD16	PASS 5.78 T	85-4.6 (T) 0.00	0.105	204			
••••••				0.00			
2245 ST AD16	PASS 5.91 T	85-4.6 (T) 0.00	0.107	204			
2266 ST 8016							
2266 ST RD16	PASS 4.51 T	83-4.6 (T) . 0.00	0.082	205			

STAAD.Pro for Windows 20.07.02.15

2					Jeb No TPL40581	Sheet No a 202	Rev R4b-FA
$\bigcirc$	11 2012 10 10 10						R4D-PA
Job Tile Wisma Bella Sw	ed to Transerve	Pie Lid			Partwind speed 32.	5 m/s	
					Ref Fabric R5		
Client Majlis Perbanda	ran Kuantan				By TSM	Date17-Dec-11 Che	TSM
					File Q326-KSP-R4b	-Deg.std Date/Time 10-J	ul-2012 16:43
Steel Design (	Track 0) (	hecks Cont					
ALL UNITS ARE - KN	HETE (UNL	ESS OTHERWISE NOTES	1				
MENDER TABLE		CRITICAL COND/	NATIO/	LOADING/			
2267 ST RD16							
	PASS 4.64 T	85-4.6 (T) 0.00	0.084	205			
2268 ST RD16	PASS	85-4.6 (T) 0.00	0.119				
	6.58 T	0.00	0.00	204			
2269 ST RD16	PASS 4.99 T	85-4.5 (T) 0.00	0.090	204			
2270 ST 8016				0.00			
	PASS 5.56 T	85-4.6 (T) 0.00	0.101 0.00	205 0.00			
2271 ST RD16	PASS	BS-4.6 (T) 0.00	0.083	205			
	4.57 7		0.00	0.00			
2272 ST RD16	PASS 0.00	85-4.6 (7)	0.000	205			
2273 ST RD16	PASS						
	25.58 T	85-4.6 (T) 0.00	0.463	204			
2274 ST 8016	PASS	85-4.6 (T) 0.00	0.000	204			
	0.00	0.00	0.00	0.00			
2275 ST RD16	PASS 24.18 T	85-4.6 (T) 0.00	0.437	205			
	24.16 7	0.00	0.00	9.00			
						20	
			Ť				

								TPL40581	Sheel No	a 204	Rev R4b-F
Software	licensed to Tra	serve Pia Lis					-	Partwind speed 32.	5 m/s		-
Tile Wisma Bella	Swimming	Pool						Ref Fabric R5	5 1193		
							-	TSM	Dale 17-D	ec.11 Chd	TSM
nt Majlis Perba	ndaran Kua	ntan					_	* Q326-KSP-R4b		Date/Time 10-Ju	
1								40201101 1140	-Deg.ald	10-30	J-2012 16:4
Beam Maxin	num For	ces by	Section	Prope	rty						
Section	_	Axial Max Fx		Max Fz	Tersion	Bar	ding				
		(kN)	(RN)	(0.N)	Max Mx (kNm)	Max My (kNm)	Max M (kNm)				
PIP2195.0	Max+ve Max-ve	459,193		9,445		14.728	21.0	75			
PIP89.1X4.0	MAX *VO	14.322	4,450	2.331	0.539	1.916					
PIP1395.0	Max-ve Max+ve	-76.184		-1.920	-0.540	-1,904					
P#P89.1X4.0	Max-ve	-41,006	-12.929	-8.370	-1.655	-7.095	-11.03	17			
	Max +ve	105.553	1.530								
PIP89.1X4.0	Max +ve	75.851	0.686	1.069	0.323	1.363	0.82	3			
PIP114.3X4.5	Max-we Max+ve	-86.999 120.540			-0.322 0.722		-0.82	2			
PP2195.0	Max-ve	-98,940	-2.611	-2.269	-0,722	-2.228	-3.07	1			
	Max +ve Max -ve	776.610		8.509		10.228	20.65				
PIP1395.0	Max +ve	171,797	7.819	3.055	0.507	3,403	8.15	4			
P#1398.0	Max-ve Max+ve	-58,616		-2.213	-0.510	-3.008	-8.11 28.42				
PIP2736.0	Max-ve Max+ve	-62,451 104,814	-47,563	-7.539	-1,560	-4.671	-28.29	7			
	Max-ve	-546.535	-38.638	31.139	25.641	65.907	63.57				
PIP1686.0	Max +ve	29.278	0.000	1.282	0.000	0.000	0.00	2			
PP1685.0	Max-ve Max+ve	-208.286 145.790	0.000	-1,282	0.000	0.000	0.00				
PP16810.0	Max-ve Max+ve	-3.950 417.212		-1,341	0.000	0.000	0.00	2			
	Max +ve	417.212	0.000	2.818	0.000	0.000	0.000				
PIP1668.0	Max +ve	193.628	0.000	2.264	0.000	0.000	0.000	5			
PIP2738.0	Max-ve	-101,300 322,343	0.000	-2.264	0.000	0.000	0.000				
CHS609X16	Max-ve Max+ve	-15.540	0.000	-5.300	0.000	0.000	0.000	1		S	
	Max-we		-137_375		124.287	278.833	773.536				
PIP40612.5	Max +ve	734,390	7,386	18.529	0.000	132.703	53.290				
CH5219X9.0	Max +ve	142,799	-5.981	-18.393	-0.000	-133,690 0.000	-43.155				
PIP2196.0	Max-ve	-216.920	8.000	-4.785	0.000	0.000	0.000				
	Max -ve	-364.673	0.000	1.783	0.000	0.000	0.000				
PIP2198.0	Max+ve Max-ve	478.320	13.258	2.356	7.771	13.554	30.579				
P#2738.0	Max +ve	553,401	-13.151	-10.503	-7.846	-28.160	-30.490	-			
PP1686.0	Max-we	-0.585 272.597	-0.951	-14.377	-0.843	-9.297	-9.990	1			
	Max-ve	-200.633	-0.292	1.057	0.000	3.358	1.517				
PP1685.0	Max +ve	216.364	0.413	1,497	0.254	7.656	2.433	1			
CH573X5.16	Max +ve	0.309	-0.409	-1,433	-0.288	-5.890	-2.381 0.621				
016	Max-ve	-0.290	-2.175	-4,135	-0.184	-1,169	-0.625				
	Max-ve	-25.582	0.000	0.178	0.000	0.000	0.000				

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES



-----

64

TAN SIEW MOI

65

Institute for Membrane and Shell Technologies

															2										
3.12	2.80	2.40	2.40					2.20			2.20	2.01		2.2	2.0	2.40	2.40	2.80	1.1	2.8	2.9	2.5	3.6		
2.36	2.36	0.63	1.53	00.0				-0.01	0.01	-0.01	0.01	0.00	-2.72	-0.29	0.00	-1.53	-0.63	-2.36	-2.36	-1.64	-1.37	11-1-	-1.99	-2.34	
4.80	4.81	5.23	4.98	5.26	40			5.54	5.24	5.24	5.54	5.34	5.11	5.40	5.26	4.90	5.23	4.81	4.80	4.44	5.03	3.60	4.20	1.50	
0.000	0.000	0.000	0.0000	0000	0000		0.000	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
0.000	0.0000	0.000	0.000	0.000	0.000		0000	0.000	0.000	0.0000	0.000	0.0000	0.000	0.000	0.0000	0.000	0.000	0.000	0.000	0.000.0	0.000	0.0000	0.0000	0.0000	
0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0000 0	0.0000	0.0000	0.000	0.0000	0.000	0.000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	
0.000	0.0000	0.0000	0.000	0.0000	0.000	0000 0	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.000	
0.000	0,0000	0.0000	0.0000	0.0000	0.000	0.000	0.000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
0.000	0.0000	0.0000	0.000	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.0000	0.000	0.000	0.000	0.000	0.0000	0.000	0.000	0.0000	0.0000	0.0000	0.000	0.0000	
13.2914	14.3104	14.7406	15.1707	15.8627	16.1246	16. 3864	16.7362	16.8241	16.9121	16.9121	16.8241	16.7362	16.3864	16.1246	15.8627	15.1707	14.7406	14.3104	13.2914	12.7025	12.1137	10.8936	10.2624	9.6312	0.13s
4.6914	7.9244	9.5935	11.2626	14.6722	16.4127	18.1512	21.6703	23.4469	25.2234	28.7766	30.5531	7626.26	35.8468	37.5873	39.3278	42.7374	44.4065	46.0756	49.3086	50.8724	52.4362	55.2500	56.5000	57.7500	Lation:
-5.2219	-6.2600	-6.6982	-7.1364	-7.8414	-8.1081	-8.3749	-0.7313	-8.8209	-8.9104	-8.9104	-8.8209	-8.7313	-8.3749	1801.8-	-7.8414	-7.1364	-6.6982	-6.2600	-5.2219	-4.6220	-4.0220	-2.7791	-2.1361	-1.4930	
0000000	10004001	0040002	0040003	1005001	2005000	1005001	10009004	90060002	E0009004	10001000	20001006	0001000	10008000	2008000	0008006	10006004	00090002	0000000	10000104	20000104	00000104	10001100	1000110002	00110003	Statik: Time

(120) jf	Using default value: NROB=	alue: NROF	-	0	
Statik Result from EASY Sta Date = 12/21/2011 Values from TNT-File	Statical analysis Time = 16:1	ysis 16:17:27			
or the	r (small	number)	0.1000000000E-07	0E-07	
Minimum stiffness of	a po	int	0.100000000E-06	005-06	
numbers	inner	iterations		200	
k: E	e: analysis				
ions					
5		:	(MAX)	576	20000
Number of fully f	fully fixed mints	:	:	498	
TTAT TO	TYEN POTING				
of cabl	a links		(1111)	000	40000
of links		Hookes law.	• •	860	
of links	T	force den:	density	0	
Number of t-eleme	t-elements		(MAX)	142	4000
Limit for convergence: Maximal number of iter Conjugate gradient	convergence: mber of iterations			20 E+00	
Statical calculation with loads	ion with load	5			
Informations to s	solve equations		with the method of conjugate	onjugat	e gradie
Number of inner i	inner iterations		residual	right	ht side
0	0	201	0.0000E+00	0.4	0.4309E+01
1	201	201	0.7548E-06	0.5	0.5904E+02
~	114	201		0.8	0.8495E+01
m	110	400	0.2682E-07	0.1	0.1083E+00

		SUBLIK: SUBLICET BUBINESSES	:			SCALLK	17/21	07:/T:0TTT07/T7/71	97:/1			
Nodes	2	Coordinates		Ceerd	Coordinate changes	sapr	AP	Applied nodes		Resi	Residual forces	
PointNo.	X-coor	Y-COOL	2-COOF	ă	YO	20	ResX	ResY	Rest	Ð	>	3
10000066	-0.8500	-5.0000	9.0000	0.0000	0.0000	0.0000	0.0000	0.000	-0.0329	-0.15	0.52	0.28
20000066	-0.8500	59.0000	0000.6	0.000	0.0000	0.0000	0.0000	0.0000	-0.0329	-0.15	-0.51	0.28
0000060	-3.4221	0.0000	11.5248	0.000	0.0000	0.0000	0.0000	0.0000	-0.1340	5.49	1.02	2.53
10000066	-5.8218	6.2553	13.6803	0.0000	0.0000	0.0000	0.000	0.000	-0.1084	8.76	0.26	2.83
2000005	-7.5746	12.9317	15.6008	0.0000	0.0000	0.0000	0.000	0.0000	-0.0946	10.48	0.96	3.24
90000066	-8.6417	19.8937	16.6483	0.000	0.0000	0.0000	0.000	0.0000	-0.0635	11.96	0.05	3.18
10000066	-9.0000	27.0000	17.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1269	12.49	0.00	3.36
80000066	-8.6417	34.1063	16.6483	0.0000	0.0000	0.0000	0.0000	0.000	-0.0635	11.98	-0.05	3.19
60000066	-7.5746	41.0683	15.6008	0.0000	0.0000	0.0000	0.000	0.000	-0.0946	10.52	-0.95	3.26
01000066	-5.8218	47.7447	13.8803	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1084	8.80	-0.26	2.85
11000066	-3.4221	54.0000	11.5248	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1340	5.56	-1.02	2.57
10001000	-0.8500	-3.5745	10.1434	0.000	0.0000	0.0000	0.0000	0.0000	-0.0892	-4.91	0.00	-2.95
90010002	-0.8500	-2.1081	11.2340	0.000	0.0000	0.0000	0.0000	0.0000	-0.0838	-4.84	0.03	-2.79
0001000	-0.8500	-0.6029	12.2703	0.0000	0.0000	0.0000	0.000	0.0000	-0.1038	-6.41	0.05	-3.54
10010004	-0.8500	1929.0	13.2509	0.0000	0.0000	0.0000	0.000	0.0000	-0.1006	-6.20	0.06	-3.50
90010005	-0.8500	2.5160	14.1745	0.0000	0.0000	0.0000	0.000	0.0000	-0.0946	-8.08	0.10	-4.71
90001000	-0.8500	4.1255	15.0399	0.0000	0.0000	0.0000	0.000	0.000	-0.1046	+1.74	0.10	-4.54
10001000	-0.8500	5.7656	15.8459	0.0000	0.0000	0.0000	0.000	0.000	-0.0945	-8.56	0.09	-5.02
80001008	-0.8500	1959.7	16.5914	0.0000	0.0000	0.0000	0.0000	0.000	-0.1109	-9.88	0.10	-5.85
60001000	-0.8500	9.1286	17.2755	0.0000	0.0000	0.0000	0.000	0.000	-0.1091	-9.62	0.10	-5.77
01001004	-0.8500	10.8471	17.8972	0.0000	0.0000	0.0000	0.000	0.0000	-0.1104	-10.21	0.10	-6.15
11001001	-0.8500	12.5870	18.4558	0.000	0.0000	0.0000	0.000	0.000	-0.1016	-11.31	0.09	-6.81
90010012	-0.8500	14.3463	18.9503	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1135	-11.47	0.08	-6.95
0010013	-0.8500	16.1224	19.3803	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1134	-11.53	0.08	-7.04
90010014	-0.8500	17.9131	19.7451	0.0000	0.0000	0.0000	0.0000	0.000	-0.1141	-11.90	0.07	-7.28
21001006	-0.8500	19.7158	20.0443	0.0000	0.0000	0.0000	0.000	0.0000	-0.1148	-12.32	0.05	-7.52
91001006	-0.8500	21.5284	20.2774	0.0000	0.0000	0.000	0.000	0.0000	-0.1055	-13.03	0.05	-0.00
10010017	-0.8500	23.3482	20.4441	0.0000	0.000	0.0000	0.000	0.0000	-0.1159	-12.63	0.03	62.7-
0010010	-0.8500	25.1729	20.5442	0.0000	0.0000	0.000	0.000	0000	-0.1157	-12.68	0.02	-7.80
61001006	-0.8500	27.0000	20.5776	0.0000	0.000	0.0000	0.000	0.000	-0.1158	-12.88	00.0	-7.90
0010020	-0.8500	20.0271	20.5442	0.000	0000	0.000	0.000	0000 0	-0.1154	12 60	00 0-	
12001000	-0 8500	10.6518	20.4441	0000	0000	0000 0	0000 0					
	0050 0-	3174 00										
TTOOLOUG	0000	2000 20					0000.0	0000.0				
120010	00000	C000.00	1041-01			0000.0	0000.0	0,000	7677.0-	F6.11-	10.0-	-1.30
SZODTONA	0008.0-	91.8.10	F085.61	0.000	0.000	0000.0	0.000	0.000	-0.1135	-11.54	-0.08	-1.05
90010050	-0.8500	1659.66	18.9503	0.000	0.000	0000.0	0.000	0.0000	-0.1018	-11.49	-0.08	-6.96
12001004	-0.8500	41.4130	18.4558	0.0000	0.0000	0.000	0.000	0.0000	-0.1135	-11.35	-0.09	-6.84
90010028	-0.8500	43.1529	17.8972	0.0000	0.0000	0.0000	0.0000	0.000	-0.1106	-10.22	-0.10	-6.15
90010029	-0.8500	44.8714	17.2755	0.0000	0.0000	0.000	0.0000	0.000	-0.1092	-9.67	-0.10	-5.80

 
 Sediabera Sán. Bbd.
 Project Ne: TPL 40581
 F

 No. 11 Jaina Astaku U8744, Szkcyen U8
 Date: 26 June 2011
 F

 Dati: 160105 (50 Shah Alam
 Date: 26 June 2011
 F

 Tel: (603)7847 3333
 Fax: (603)7847 2222
 Doc No: Q326-KSP-CAL-001 Rev 0
 Page: Project : Upgrading of Aquatic Center Wisma Belia Inders Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design APPENDIX B FABRIC OUTPUT DATAS B1. EDGE PANEL NEXT TO DIVING POOL FABRIC NODE NUMBER LAYOUT PLAN - PRESTRESS LOAD CASE - LIVE LOAD CASE - LIVE LOAD CASE b1 b2 - b4 b5 - b7 b8 - b10 b11 - b13 b14 - b16 b17 - b19 WIND UPLIFT WIND PRESSURE WIND FROM ENTRANCE WIND FROM AUDIENCE STAND 
 INTERNAL PANEL

 FABRIC NODE NUMBER LAYOUT PLAN
 b20

 - PRESTRESS LOAD CASE
 b21 - b23

 - LIVE LOAD CASE
 b24 - b26

 - WIND VULFT
 b27 - b29

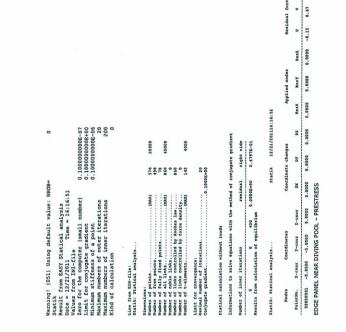
 - WIND PRESSURE
 b30 - b32

 - WIND PRESSURE
 b33 - b33

 - WIND FROM ENTRANCE
 b33 - b33

 - WIND FROM AUDIENCE STAND
 b36 - b38
 EDGE PANEL NEXT TO SCORE BOARD FABRIC MODE NUMBER LAYOUT PLAN - PRESTRESS LOAD CASE - LIVE LOAD CASE - WIND VOLIFT - WIND PRESSURE - WIND FROM ENTRANCE - WIND FROM ENTRANCE - WIND FROM AUDIENCE STAND b39 b40 - b42 b43 - b45 b46 - b48 b49 - b51 b52 - b54 b55 - b57

0010035 90010034 9002 90010032 90010032 90010031 90100001 99000010 90070002 90070001 9900007 900 60003 90010001 EDGE PANEL NEAR DIVING POOL 900200 9900000 FABRIC NODE NUMBER LAYOUT



62

hC



 Miniting
 Miniting

EDGE PANEL DIVING POOL - LIVE LOAD

67

9900002	-0.8500	59.0000	9.0000	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	-0.15	
20000066	-3.4221	0.0000	11.5248	0.0000	0.000	0.000	0,0000	0.0000	0.0000	3.96	
9900004	-5.8218	6.2553	13.8803	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	4.87	
3900005	-7.5746	12.9317	15.6008	0.000	0.000	0.000	0.0000	0.0000	0.0000	4.96	
33000006	-8.6417	19.8937	16.6483	0.000	0.0000	0.000	0.000	0.0000	0.0000	5.18	
10000066	-9.0000	27.0000	17.0000	0.000	0.000	0.000	0,000	0.0000	0.0000	5.24	
80000066	-8.6417	34.1063	16.6483	0.0000	0.000.0	0000.0	0.0000	0.0000	0.0000	5.10	
60000066	-7.5746	41.0683	15.6008	0.000	0.000	0.000	0.0000	0.0000	0.0000	4.96	
39000010	-5.8218	47.7447	C080.C1	0.0000	0.000	0.000	0.0000	0.0000	0.000	4.87	
11000066	-3.4221	54.0000	11.5248	0.0000	0.000	0.000	0.0000	0.0000	0.0000	3.96	
10001006	-0.8500	-3.5745	10.1434	0.000	0.000.0	0.000	0.0000	0.0000	0.0000	-4.71	
90010002	-0.8500	-2.1081	11.2340	0.000	00000	00000	0.000	0.0000	0.0000	-4.14	
2001000	-0.8500	-0.6029	12.2703	0.000	0.000	00000'0	0.0000	0.0000	0.0000	-4.87	
9001004	-0.8500	1626.0	13.2509	0.0000	0.000	00000	0.000	0.0000	0.000	-4.31	
9001005	-0.8500	2.5160	14.1745	0.000	00000'0	0.0000	0.000	0.0000	0.0000	-5.20	
90001006	-0.8500	4.1255	15.0399	0.0000	00000	0.000	0.0000	0.0000	0.0000	-4.64	
90010001	-0.8500	5.7656	15.8459	0.0000	0.0000	0.000	0.0000	0.0000	0.000	-4.87	
80001006	-0.8500	1969.7	16.5914	0.000	00000	00000	0.0000	0.0000	0.0000	16.3-	
9001006	-0.8500	9.1286	17.2755	0.000	0.000	0.000	0.0000	0.0000	0.0000	-4.96	
90010010	-0.8500	10.8471	17.8972	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.07	
11001006	-0.8500	12.5870	18.4558	0.000	0.000	0.000	0.0000	0.0000	0.000	-5.42	
90010012	-0.8500	14.3463	18.9503	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.35	
51001006	-0.8500	16.1224	19.3803	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	-5.27	
90010014	-0.8500	17.9131	19.7451	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.33	
90010015	-0.8500	19.7158	20.0443	0.0000	0.000	0.0000	0.0000	0.0000	0.000	-5.37	
90010016	-0.8500	21.5284	20.2774	0.000	0.000	0.000	0.0000	0.0000	0.000	-5.65	
1001006	-0.8500	23.3482	20.4441	0.0000	0.0000	0.000	0.000	0.0000	0.0000	-5.46	
90010018	-0.8500	25.1729	20.5442	0.000	0.0000	0.000	0.000	0.0000	0.0000	-5.43	
61001006	-0.8500	27.0000	20.5776	0.000	0.000	0.000	0.0000	0.0000	0.0000	-5.43	
90010020	-0.8500	28.8271	20.5442	0.000	0.000	0.000	0.0000	0.0000	0.0000	-5.43	
90010021	-0.8500	30.6518	20.4441	0.000	0.000	0.000	0.0000	0.0000	0.0000	-5.46	
90010022	-0.8500	32.4716	20.2774	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	-5.65	
90010023	-0.8500	34.2842	20.0443	0.000	0.000	0.000	0.000	0.0000	0.0000	-5.37	
90010024	-0.8500	36.0869	19.7451	0.0000	0.0000	0.000	0.0000	0.0000	0.0000	-5.33	
90010025	-0.8500	37.8776	19.3803	0.000	0.000	0.000	0.0000	0.000	0.0000	-5.27	
90010026	-0.8500	39.6537	18.9503	0.0000	0.000	0.000	0.0000	0.0000	0.0000	-5.35	
90010027	-0.8500	0214.11	18.4558	0.0000	0000"0	0.0000	0.0000	0.0000	0.0000	-5.42	
90010028	-0.8500	43.1529	17.8972	0.0000	0.000	0.000	0.0000	0.0000	0.0000	-5.07	
90010029	-0.8500	44.8714	17.2755	0.000	0000 0	00000	0.0000	0.0000	0.0000	-4.96	
0001006	-0.8500	46.5659	16.5914	0.000	0000.0	00000	0.000	0.000	0.0000	-5.31	
TEODIODE	-0.8500	48.2344	15.8459	0.0000	0.000	0.000	0.000	0.000	0.000	-4.87	
TEDOTOOS	0058.0-	Ch19.64	6650.CT	0.000	0000 0	0000	0.000	0.000	0.0000	19.64	
CCONTONS	-0.8500	21.4840	14.1745	0.000	0000	00000	0.0000	0.0000	0.0000	-5.20	
		6000.00	6007.01		0000-0	0000.0	0000.0	0.000	0000.0	15.1	
SCONTOOL		1001 33	CO12.21	0000.0	0000-0	0000.0	0000	0.000.0	0000.0		
		1001.00						0000	0000-0		
					0000.0				0000.0		
20002006	1961	2 2000	10 2524	0000			0000		0000.0		
1002000	1977.5-	-1 2500	10 001	0000 0							
10001006	-4.0220	1.5678	12.1137	0000	0000 0			0000 0	0000 0		
90030002	-4.6220	3.1276	12.7025	0.000	0000	0000	0000 0	0000 0			
EDGE PANEL NEAR DIVING POOL - PRESTRESS	L NEAR I	DIVING PC	JOL - PRE	STRESS							

4000

(XVH

576 78 860 860 142 142 5400

Hookes

points. fixed points. fixes finks finks controlled by controlled by ments

Fully fully all L cable Links Links

\*\*\*\*\*\*\*\* Menner Aumber Aumber Aumber Aumber Aumber Aumber Aumber Aumber r.49ht side 0.9920E401 0.9510F403 0.1055E404 0.5602403 0.1552E403 0.1552E403 0.1553E403 0.1553E403 0.9333E403

201 201 201 201 201 201 201 201 201 201

201 200 1100 1100 92 92

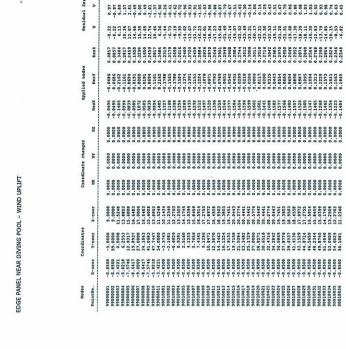
0.00005+0 0.00005+0 0.86136-0 0.11385-0 0.23345-0 0.55245-0 0.37155-0 0.34955-0 0.15955-0



Mile in the second Acress 444 (1997) (1997 

5,00 11,00 1,00 11,0 0,1237 0,1720 0,1720 0,1720 0,1720 0,1720 0,1720 0,1720 0,1207 0,120 

 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 10.0936 12.1137 12.1137 13.1201 14.7101 14.7101 15.1705 15.170 



68

cesidual 0.0008440 0.6512640 0.13416-03 0.12966-03 0.12966-03 0.10406-05 0.21646-03 0.57386-01

201 201 201 201 201 201 201 201

201 162 164 95 84 95 96

612

10000

516 498 860 860 860 142

points.... free points. fully fixed all links... cable links. links contro links contro. t-elements...

tartik: Statik: Statik: Aunber Aunber Aunber Aunber Aunber Aunber Aunber Aunter Aunter Aunit f

converge mber of gradient

688888

-2.75 5.75 5.75 5.75 5.75 111.66 111.66 111.65 112.29 112.29 112.29 112.29 112.29 112.29 112.29 112.29 112.29 112.29 112.29 112.39 112.39 12.24 112.35 111.65 111.65 111.65 111.65 111.65 111.65 111.65 111.73 12.34 12.35 12. -5.52 5.52 5.52 5.52 111.17 111.17 111.17 111.25 111.25 112.23 115.23 11 1,15500 1,15500 1,15500 1,15500 1,15500 1,15500 1,15500 1,15500 1,15500 -0.1128 -0.1011 -0.1011 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.11232 -0.122 0.1434 9.5212 9.5212 9.5212 9.5212 8. 97.5745 -2.7590 -2.7590 -1.7590 -1.7590 -1.7590 -1.7590 -1.7590 -1.7590 -1.750 

69

613

610

		0.1000000	0000001.0												· (HAX)			- (HAX)					- (HAX)			******						To body		and the second	INDERT			arter o	-35655.0	0.21395-0	0.42776-0	0.37068-0								000				IND PRES	
al analysis		number)			SUOTO	EURTO														Hontas lau	LOT ODVOOL	FOICE DEVI										a with the					100	1.1	107	400	201	400	equilibrium											M - 100	
Statical analy		outer (small nu	the gradient	and a so a	outer sterad	THINK THEFT	Lon			le:	analysis					oints	fixed points	nks	Links	antrolled by 1		A Dattoinuon	Ents		gence:	f Aterations	nt			tion with load		antive smarting	in the second	a number of the second	THE PARTY OF THE P	•		101	FOT	103	114		from calculation of equ			analysis				Coordinates				AR DIVING P	
Result from EASY Statical Analysis Date = 03/08/2012 time = 11-20	Values from INI-file	Zero for the computer (small	Minimum triffores of addant		Naximum numbers of outer trefactons	TO STRONG TO BE DELLA	NING BE CALCULAT			Line from EIN-file:	Statik: Statical analysis		" and an and	SUOTENANTO	Number of points(HAX)	Number of free points	Number of fully fixed points	Number of all links (MAX)	Number of cable links	Number of links		NUMBER OF THESE	NUMBER OF C-ELEMENTS (MAX)		Limit for convergence:	Maximal number of Iterations	Conjugate gradient0.10			Statical calculation with loads		Informations to solve substants with the mathematic		Number of Sunse Start (and		•		• •		-	-		Results from cal			Statik: Statical analysis				Nodes				EDGE PANEL NEAR DIVING POOL - WIND PRES	
																																																			1	61	15		
*		0.42	0.78	4.76	4.25	4.76	4.27	3.33	10 64														+1.74	-8.35										-2.22	-4.50	-5.91	-5.95	-5.07	-5.78	-5.97	-5.55	-4.94	-5.42	-5.47	-5.08				1 10	-1.18	-2.81				
>		0.74	-0.95	4.21	1.76	3.42	0.50	0.11	0 80				-5.40	0.12	0.20	0.31	35 0				0.56	0.65	0.64	0.69	0 78	0.79		0.84				0.72	0.40	0.31	0.75	1.04	1.14	1.08	1.21	1.28	1.29	1.24	1.28	1.29	1.27	-	1 05		0. 80	0.68	0.47				
D		-0.12	-0.19	1.69	13.27	15.71	17.49	5.62	16.30				6.70	-5.23	-5.80	-8.31	-7 48	10 11		11.01-	C8.11-	-13.20	TE.31-	-13.30	11 51-	-15.05	32 41-	-15.42				-12.76	12.1-	G-1-	-17.80	-23.29	-23.80	-20.70	-22.48	-22.54	-20.93	-18.67	-19.31	-18.80	-17.30	02 11-	-14.29	15 16	-10.43	-8.86	-6.91				
Rest		-0.0395	0.0526	-0.1608	-0.1300	-0.1135	-0.0762	0.2253	0.1650	0 2450		107.0	0.3484	-0.1070	-0.1006	-0.1245	1207	2011 0-			+CII.0-	1001.0-	-0.1309	-0.1325	-0.1219	-0.1362	1911 0-	-0.1370		110110		0501.0-	1821.0-	0.2107	0.3010	0.2716	0.3042	0.2985	0.2970	0.2950	0.2646	0.2952	0.2874	0.2840	0.2564	0.2788	0.2390	0 2804	0.2624	0.2346	0.2548				
ResY		0.0317	0.0421	8660.0	0.0536	0.0320.0	0.0088	0.0066	0.0191	0.0694	1911 0		0.2162	0.0825	0.0722	0.0825	0.0711				1650.0	0.0565	0.0498	0.0448	0.0365	0.0355	1010 0	0.0250				0.0100	10000	0.0022	0.0117	0.0200	500.0	0.0443	0.0554	0.0665	0.0694	0.0890	0.0987	0.1095	0.1094	FIEL 0	0.1229	0.1571	0.1611	0.1563	0.1845				
ResX		0.0228	10:004	0.0649	0.0459	0.0387	0.0233	-0.0716	-0.0505	-0.019			-0.1405	0.0612	0.0548	0.0646	0.0625	0 0505			0.0596	0.0698	0.0691	0.0701	0.0644	0.0720	0.0722	0.0728		11.00		1610.0	1990.0	-0.1124	-0.1601	-0.1441	-0.1608	-0.1582	-0.1577	-0.1566	-0.1400	-0.1557	-0.1520	-0.1500	1947	-0.1465	-0.1260	0.1462	-0.1354	-0.1223	-0.1404				
02 ResK		0.000	0.000	000010	0000 0	0.000	0.000	0.000	0.000	0.000			0.000	0.000	0.000	0.0000	0.0000	0000 0			0.000	0.000	0.0000	0.000	0.0000	0.000	0.000	0.000	00000						0000-0											00000		0000	0.000	0.0000	0.000				
		0.000	0.0000	00000	0.000	0.000	0000.0	0.000	0.000	0000	0000		0.000	00000.0	0.0000	0.000	0.0000	0000 0			0000.0	0.000	0.000	0.000	0.000	0.0000	0.000	0.000	0000 0			0000.0	0000.0		0.000	0.000	0.000	0.000.0	0.000.0	0.0000	0.000.0	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000.0	0.000.0			TRANCE	
XO		0.0000	0.000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0000 0		0.000	0.0000	0.0000	0.0000	0.0000	0000 0			0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0000 0						0000.0	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000			FROM FD	
2-001		9.0000	00000	8122.11	C088.CT	13.6008	16.6483	17.0000	16.6483	15.6008	LOBA LI		8670.11	10.1434	11.2340	12.2703	13.2509	14.1745			6668.61	16.5914	17.2755	17.8972	18.4558	10.9503	19.3603	19.7451	20.041	PLLC 00		1			20.02	20.4441	20.2774	20.0443	19.7451	19.3803	18.9503	18.4558	17.8972	17.2755	16.5914	15.8459	15.0399	14.1745	13.2509	12.2703	11.2340			NINI - K	
Y-COOL		-5.0000	29.0000	0.000	6.2553	12.9317	19.8937	27.0000	34.1063	41.0683	CAAT TA		0000.00	-3.5745	-2.1081	-0.6029	1666.0	2.5160	1266		2.1626	1969.1	9.1286	10.8471	12.5870	14.3463	16.1224	17.9131	10 7158						1178-87		32.4716		36.0869	37.8776	39.6537	41.4130	43.1529	44.8714	46.5659	48.2344	49.8745	51.4840	53.0609	54.6029	56.1081			VING POC	
X-COOF	Constants.	-0.8500	-0.8500	1775.6-	-5.8218	9112-1-	-8.6417	-9.0000	-8.6417	-7.5746	-5.8218	1000 0-	1776-0-	-0.8500	-0.8500	-0.8500	-0.8500	0058 0-	0058 0-		-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.950.0	-0.8500						-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500	-0.8500			NEAR DI	
FointNo. X-coor Y-coor Z-coor DX DY		10000066	2000000	C0000066	10000066	50000066	90000066	10000066	90000066	60000066	01000066	1100000	TTANAAC	10001006	90010002	0001006	9001004	2001000	20001006					01001006	11001006	90010012	01001006	90010014	21001005	91001006	21001000			CTONTONE		17001006	22001006	CZ001006	90010054	90010025	90010026	90010027	90010028	90010029	90010030	1001006	2001005	90010033	\$0010034	SEGOTOOS	90010036			EDGE PANEL NEAR DIVING POOL - WIND FROM ENTRANCE	
																																																						ű	

0.1000000000000000 20 200			Ť	78	(HAX) 860 40000	•	960	y 0	(HAX) 142 4000	20 20,1000E+00
iffness of a point of makers of a point makers of outer iterations makers of inner iterations iculation	EIN-file: atical analysis	: points(HAX)	free points	fully fixed points	all links(HAX)	cable 1inks	links controlled by Hookes law	links controlled by force density	t-elements(HAX)	convergence: wber of Lerations

\*ide \*ide \*ide \*ide \*ide \*ide \*ide

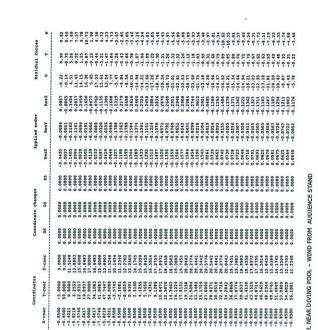
Number of inner iterations	terations		residual	right .
•	0	201	0.00005+00	0.58851
1	201	201	0.13418-05	10.13333
2	103	201	0.55938-05	0.23941
	109	400	0.21395-06	0.75241
•	114	201	0.42775-09	0.88751
\$	74	400	0.37062-07	0.17051

611

Anhalt University of Applied Sciences, Dessau 🦛

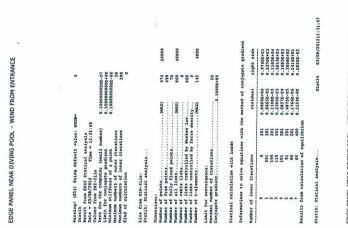
	900200	900200	900200
•	No.	1	

																																																	62
-0.44	-0.52	-0.76	-0.72	-0.94	-0.82	-0.88	-0.96	-0.87	-0.87	-0 65			CB.0-	-0.84	-0.84	-		-0.82	28.0-	78.0-	-					-0.42	-0.17	-0.87	-0.96	-0.88	-0.82	-0.94	71.0-	-0.52	-0.44	-0.48	-0.55	0.80	1.0		-0.30	-0.99	-0.89	-0.89	-0.94	16.0-	-0.87	-	-0.89
0.08	90.06	0.05	0.03	0.02	0.03	0.01	10.01	0.00	10.01	10.0				00.00	00.00	10.0	10-0-	10.0	00.0	10.0-	10-0	10.0-				-0.01	-0.01	0.00	-0.01	-0.01	-0.03	-0.02		-0.06	-0.08	0.08	90.06	0.05		10.0	0.01	0.01	0.00	0.01	10.01	0.00	0.0		00-0
	-4.12	-4.85	-4.30	-5.20	-1.63	-4.80	-5.31	-4.96	-5.07	-5.47					11.2								10.01	20. 20	21.2-	-5.42	-5.07	-4.96	-5.31	-4.88	-1.63	-3.20		-4.12	-4.65	4.66	1.1		02.1	19.4	4.88	5.32	4.96	5.07	5.42	5.35	2.27		10.0
	0000.0	0000.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0000			0000-0	0000 0			0000-0							0000	00000	0.000	0.0000	0.0000	0,0000	0000 0	0000.0	0000 0	0000	0.000	0.000.0	0.000	0000.0	0000 0	00000	0.000	0.000	0.000	0000 0	0000 0	0000 0	0000-0		0000-0
	0000-0	0.000	0.000	0.000	0000'0	0000 0	0.0000	0.0000	0.0000	0.0000	0.000			0000.0	0000.0			0000-0						0.000	0.000	0.000	0.000	0.000	0.0000	0.000	0.0000	0000.0	0000 0	0.000	0.000	0.000	0.000	0000-0	0000-0	0.000	0.000	0.0000	0.000	0.000	0000 0	0000-0	0000.0	0000 0	0000-0
	0.000	0.0000	0.000	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0000 0				0000			0000			0000 0	0000	0.0000	0.000	0.000	0.0000	0.000	0.000	0.000	0.0000	0000.0	0.000	0.0000	0.0000	0.000	00000	0000	0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	00000	0000	
	0000.0	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0000 0				0.0000	0000 0					0000 0	0.0000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	000000	0.0000	0.0000	0.0000	0.0000	0.0000		0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0000.0		0.0000	
		00000	0.0000	0.000	0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0000 0			0.0000	0000 0				0000	0000	0.000	0.000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	0.0000	0000 0	0.0000	0.0000	0.0000	0.0000	00000		0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0000.0	0000 0	0000	0.000	
		0000-0	0.0000	0.0000	0.000	0.000	0.0000	0.000	0.0000	0.0000	0.0000	0.000	0.000			0.000	0000 0		0000	0000	0.000	0.000	0.0000	0.0000	0.000	0.000	0.00.0	0.000	0.0000	0.0000	00000		0.000	0.0000	0.0000	0.0000	0.000		0.000	0.000	0.0000	0.000	0.000	0.000	0000-0		0000	0.000	
		E017-31	6002.61	C6/1-61	15.0399	10.840B	16.5914	17.2755	17.8972	18.4558	18.9503	19.3803	1945.01		ATTE DC	20.4441	20.5442	20. 5776	20.5447	20.4441	20.2774	20.0443	19.7451	19.3803	18.9503	18.4558	17.8972	17.2755	16.5914	15.8459	10.0399	522.61	12.2703	11.2340	\$6\$1.01	+6+1.01	COLC CI	0052 61	14.1745	15.0399	15.8459	16.5914	17.2755	17.8972	0000.01	COSC OF	19-7451	20.0443	
			1656.0	0910.7	1.1255	0.000	1.4341	9.1286	10.8471	12.5870	14.3463	16.1224	17.0121	19 7158	21.5284	23.348Z	25.1729	27.0000	28.8271	30.6518	32.4716	34.2842	36.0869	37.8776	7653.90	41.4130	43.1529	44.8714	46.5659	48.2344	C118.65	6090.55	54.6029	56.1091	57.5745	-3.5745	1001.2-	1616.0	2.5160	4.1255	5.7656	1424.1	9.1286	10.8471			1616.71	19.7158	
01 5500			0000.10	0000.10	0055.18	0000110	81.3500	81.5500	61.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	81.5500	01.5500	81.5500	81.5500	81.5500	81.5500	0000010	61.5500	81.5500	81.5500	81.5500	66.7500	0001.00	66.7500	66.7500	66.7500	66.7500	66.7500	66.7500	66.7500	0051 00	0051 99	66.7500	66.7500	
0001000		FUOD LOUG	LODATOOL	CONDITION	90001006	innotions.	RODDTODA	60007006	90010010	11001006	90010012	61001006	90010014	90010015	90010016	90010017	90010018	90010019	90010020	90010021	90010022	90010023	90010024	90010025	90010026	90010027	90010028	90010029	90010030	1001006	CENTING	90010034	90010035	90010036	90010037	10002006	1002000	9002004	90020005	9002006	90020007	9002008	2002009	90020010	1000000	11002006	90020014	90020015	



Media Patricia Patricia

618



20000 40000 4000

11192 78 78 2029 2029 166

law.

force

solve

Statical ... Informations to so Number of inner i

lysis 12:18 number

0.1434 9.5282 9.5282 9.5282 9.5282 9.5282 9.6273 9.6273 9.6273 1.52844 1.52844 1.52844 1.52844 1.52844 1.52844 1.52844 1.52844 1.52844 

000000

90020037

Line from EDP-(1): Excitin 12 etc.(a) malyal... Dimminani Dimminani Dimminani et from patter... Dimminani et from patter... Dimminani et from entrolled y in Dimmina et allan entrolled y in Diminani et allan entrolled y in Dimminani et allan et from EASY Statical anal 12/22/2011 Time = from JNL-file ' from JNL-file ' from Computer (amail n or the computer (amail n re computer (amail n n attifrems of a point n tumbers of outer itera n numbers of inner itera 90010006 Warningi Statik Result f Nalues f Values f Zero for Limit fo Hinimum Haximum Haximum

620

90010037

616

INTERNAL PANEL - FABRIC NODE NUMBER LAYOUT

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES

TAN SIEW MOI

621

¥ 15.01 15.21 15.22

v 21.90 -21.90 22.51

40.85

Res2 0.0000 0.0000 0.0000

ResY 0.0000 0.0000 0.0000

ResX 0.0000 0.0000 0.0000

20 00000.0 00000.0

0.0000

0.0000 0.0000 0.0000

2-5005 9.0000 9.0000 9.0000

Y-COOF -5.0000 59.0000 -5.0000

X-COOF 81.5500 81.5500 66.7500 66.7500

PointHo. 99000002 99000002 99000003 Nodes

617

Institute for Membrane and Shell Technologies

20.2774 20.4412 20.4412 20.5742 20.5742 20.5442 20.5442 20.5442 20.5442 20.5442 19.7459 19.7459 19.7594 11.259 21.5284 25.1702 25.1702 28.1702 28.271 28.271 28.271 29.2875 31.0805 3 75800 

-5.35 3.35 3.35 3.35 3.35 3.35 3.35 1.1, 5.2 1.1, 5.2 1.1, 5.2 1.1, 5.2 1.1, 2.2 1.1 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 0, 1667 0, 1258 0, 125 0.0500
-0.11232
-0.11232
-0.11232
-0.11232
-0.11232
-0.11232
-0.11232
-0.11232
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.112
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.1123
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0.112
-0 10.1.01 10.01 10.1. 57.575 57.5758 1.25508 1.25 -0.000 -0.000 -2.110 -2.110 -2.110 -2.110 -2.110 -2.110 -2.110 -2.110 -1.1100 -1.1100 -1.1100 -1.1100 -1.1100 -1.1100 -1.1100 -1.1100 -111104 1111104 Sector 11104 Sector 11104

623

Institute for Membrane and Shell Technologies

convergence: wmber of iter

20000

1192 78 78 2029 2029 2029 166

alled by Hookes alled by force

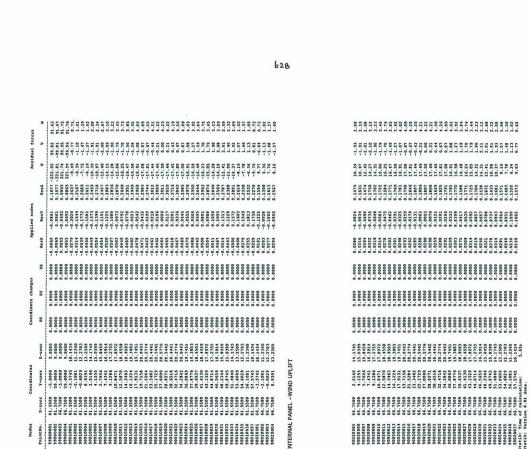
free points.... free points. fully fixed a all links... links control links control tectements...

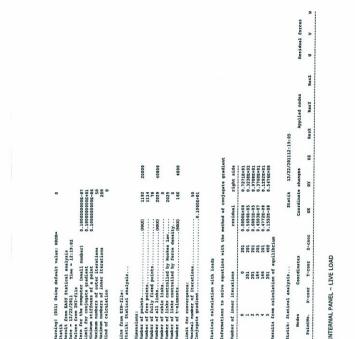
Differnations: Number of p Number of a Limit for o Limit for o Conjugate q



0.1453E+01 0.7096E+01 0.7947E+00

0.9231E-06 0.1450E-08 0.3753E-07





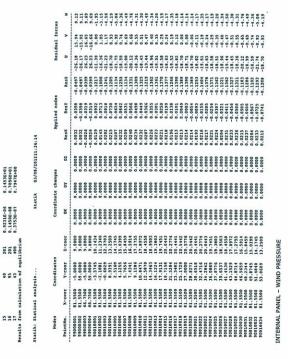
1,17 117.03 116.99 117.19 11 

 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 0
 

624

625

629



dia	cen Article Maall number) 0.100000008-07 teoryuste gradient 0.100000008-01 teoryuste gradient 0.100000008-01 Artfores of a paint numbers 0.1000000008-05 numbers of unter iterations 50 addoubtion 0 00	use a corderious time . Vulues from INL-file Zero for the computer (amal) Limit for conjugate gradient Maximum mumbers of outer ite Haximum numbers of inner ite Haximum numbers of inner ite
(MAN) pelates	lysis	ine from EIN-file: tatik: Statical an
points	1192 III	Number of points
		5
lled by Mookes law2 lled by force density 		
lled by force density	rolled by Nookes law 2029	
(XXX)		5
init for convergence.		5
ations	e: etations0.10005401	Limit for convergence: Maximal number of iter Conjugate gradient

40000

626

630

residest 0.0000;400 0.16246-04 0.16246-04 0.16246-07 0.28755-04 0.28755-04 0.28755-04 0.28755-04 0.28755-04 0.13925-04 0.13925-05 0.234125-05 0.234125-05 0.2345-05 0.2345-05 0.2345-05 0.2345-05 0

umber of inner iterations	terations		residual	right side
0	0	201	0.00005+00	0.20335+02
-	201	201	0.76485-04	0.34655+03
2	201	201	0.24155-02	0.77068+04
-	105	201	0.24555-01	0.28915+04
•	176	201	0.24205-02	0.21965+04
s	110	201	0.12216-02	0.90316+03
9	135	201	0.22426-03	0.67445+03
-	123	201	0.7894E-04	0.18776+03

0.18776+03	0.91246+02	0.60865+01	0.26976+00		statik 03/08/201211:35:4
0-1824E-04	0.74028-05	0.15025-05	0.7173E-08		Sta
107	201	201	400	equilibrium	
121	127	126	111	Results from calculation of equilibriu	Statik: Statical analysis
		6	10	tesults fro	itatik: Sta

631



TAN SIEW MOI



1.1.500 1.1.5000 1.1.5000 1.1.5000 

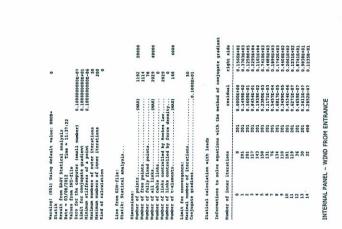
55855

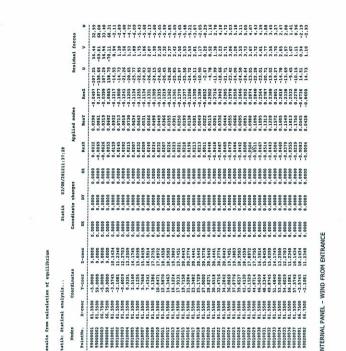
0.1000

lysis 11:38:1

632

636





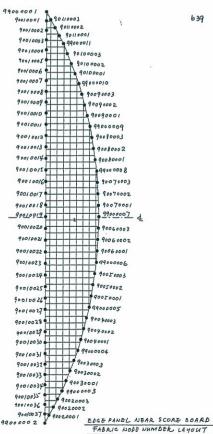
b 33

637

634

635

1.55 1.1.55 1.1.57 1.1.57 1.1.57 1.1.57 1.1.57 1.1.17 1.1. 22,25 23,25 24,25 25 0, 9745, 9756, 975 11. 200 11. -0.6039 -0.5116 -0.510 66, 7300 66, 7000 66, 7000 66, 7000 66, 7000 66, 7000 66, 7000 66, 7000 66, Control of Contro

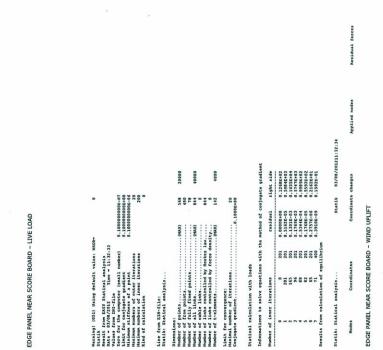


Anhalt University of Applied Sciences, Dessau 🦛 

Institute for Membrane and Shell Technologies

2.	0051											-
			0000 6	00000	0.0000	0.000	0.0000	0.0000	-0.0287	0.15	0.00	-0.12
	1776	0.000	11.5248	00000	0.000	0.0000	0.000	0.0000	-0.1219	-5.53	16.0	2.46
	9110	CCC2.0	5088.CT		0000	0000.0	0.000	0000 0	-0.0850	-8.84	0.56	2.93
16	1117	119.89.77	16.6483	0000			0.000	0000.0	00110-	-10.59	1.75	
99000007 91.	91.5000	27.0000	17.0000	0.000	0.0000	0.000	0.000	0000 0	5960 0-	12 51		
	11.1417	34.1063	16.6483	0.000	0.0000	0.000	0.0000	00000	-0.0747	-12 00		
	10.0746	41.0683	15.6008	0.000	0.0000	0.0000	0.0000	0.000	-0.1400	-10.55	-1.75	
	9120	47.7447	13.8803	0.0000	0.0000	0.0000	0.0000	0.000	-0.0850	-0.79	-0.56	2.90
	9221	54.0000	11.5248	0.0000	0.0000	0.0000	0.0000	0.0000	-0.1219	-5.46	-0.97	2.41
	3.3500	57.5720	10.1381	0.000	0.0000	0.0000	0.0000	0.000.0	-0.0894	4.85	0.00	-2.83
	0050.0	26.1036	11.2236	0.000	0.0000	0.000	0.0000	0.000	-0.1274	4.75	-0.02	-2.69
	0000.0	1965.10	12.2549	0.000	00000	0.0000	0.0000	0000 0	-0.1175	6.44	-0.04	-3.51
			BOC7	0000.0	0000.0	0.0000	0.000	0000 0	CICT.0-	61.3	-0.06	-1.43
1			1617-17	0000.0	0000	0000.0	0.0000	0000 0	-0.1401	8.08	-0.10	-4.62
		1098.64	60T0.CT	0000	0000.0	0.0000	0.000	0000 0	-0.1197	91.78	-0.09	-4.47
		C177.01	6718.01	0000 0	00000	0000.0	0.0000	0000 0	-0.1392	8.55	-0.09	-4.92
						0000.0	0000.0	0000-0	-0-1284	6.6	-0.10	-5.79
				0000.0	0000.0	0000.0	00000	0000.0	-0.1420	9.65	-0.10	-5.69
					0000.0	0.000	0.0000	0000 0	-0.1437	10.22	-0.10	-6.05
			5005 BT	0000.0	0000.0	00000	00000	0000 0	-0.1474	11.34	-0.09	-6.72
1			sinc. or		00000	00000	0.0000	0.000	-0.1324	11.55	-0.09	-6.88
		10.0.0	1675.61	0000-0	0000.0	00000	0.000	0000 0	-0.1475	11.57	-0.08	-6.96
		CO80.90	12.63.41	0000	0000	0.000	0.0000	0000 0	-0.1484	11.95	-0.06	-7.19
		6817.60	C686.61	0000 0	0000.0	00000	0.0000	0.0000	-0.1492	12.35	-0.05	-7.42
		9195.20	P122.02	00000	00000	0000.0	0.0000	0000 0	-0.1520	13.04	-0.04	-7.89
		1228 80	2105.02		0000.0	0000	0000.0	0000-0	-0.1357	12.68	-0.03	-1.70
-	0.3500	27.0000	20.5200	0.000	0000	0000				10 51	10.0-	
	0020.0	25.1743	20.4868	0000	0000 0	0000 0						
	3.3500	23.3509	20.3872	0.000	0.0000	0.0000	0000		1905	12 60	10.0	
-	3.3500	21.5324	20.2214	0.000	0.0000	0000	0000 0	0000 0	0211 0-			
	0050.01	19.7211	19.9895	0.000	0000	0000	0000 0					
	0.3500	17 9195	19 6970	0000			0000			10.11		
-	0051.1	16.1299	1955.91	0000 0				0000				DZ-1-
	0.3500	14.3546	10.9014	0.000	0.000	0000	0000 0					
	0050.0	12.5961	18.4094	0.000	0.000	0000 0	0000 0	0000 0				
	0.3500	10.8566	72.88.71	0.000	0.000	0000	0000 0					
	1. 3500	1185	2316 21				0000	0000		10.24	01.0	-
-	0050.0	1	16 5546						BTLT-D-			21.0-
	1.3500	1745	15 8129								01-0	
-	00SE	4 1749	15 0109	0000 0				0000.0	1777-0-		60.0	
	0050	2.5246	14.1498	0000				0000 0	7951.0-	CB-1	60.0	12.1-
	1500	0.9467	11.2108	0000			0000					
	0050.01	1965.0-	12.2549	0000 0			0000 0		5051-0-	87.0		
	3500	-2.1016	11.2276	0000	0000		0000	0000	1001.0-			
	03.3500	-3.5720	1911.01	0.000	0.000			0000 0	0601 0-			
	00666	-3.7500	9.6312	0000	0000	0000 0						
	1919	-2.5000	10 2624	0000							20.2	
90020003 85.	1975.	-1.2500	10.8936	0.000	0000							29.7
1			and and a			0000.0	0000.0	0000-0	110.0-		28.0	10.2

3.48	2.61	2.33	2.99	00.0	3.05	3.14	3.62	3.21	60.0		1.64	5.6	5.5	5.55	\$5.55 5.55 5.55 5.55 5.55 5.55 5.55 5.5	******	1.16	5.52 1.46 1.46 1.51 1.64	5.52 5.52 5.52 5.52 5.52 5.52 5.52 5.52	54 55 55 55 55 55 55 55 56 56 56 56 56 56	5.55 2 4 <del>6</del> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5.55	5.55.55.55.55.55.55.55.55.55.55.55.55.5	1.0000000000000000000000000000000000000	2000 2000 2000 2000 2000 2000 2000 200	
-0.65	-0.65	-0.83	-0.42	-0.81	-0.69	-0.68	-0.85	-0.44	-0.07		60.0-	-0.09	-0.04	-0.01	-0.02 -0.03 -0.04 -0.09	0.02 -0.02 -0.03 -1.53	0.02 -0.02 -0.03 -0.03	0.0 0.0 0.0 0.0 0.0 0.0 0 0.0		0.01 0.02 0.02 0.02 0.02 0.03	0.07 0.08 1.53 0.09 0.09 0.09 0.09 0.09 0.09 0.09	0.44 0.07 0.07 0.03 0.03 0.03 0.03 0.03 0.03	0.85 0.44 0.44 0.91 1.53 0.01 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03	0.68 0.85 0.07 1.53 1.53 1.53 1.53 1.53 1.53 1.53 0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.0	0.69 0.68 0.68 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02	0.81 0.65 0.66 0.65 0.11 0.01 0.01 0.01 0.02 0.02 0.02 0.02
	-1.65	-4.52	-7.48	-7.12	-8.15	-9.08	-10.26	-10.15	+11.34	-	-11.89	-11.81	-12.33	-12.82	-12.30	-12.29 -12.30 -12.82 -12.33	-12.01 -12.29 -12.30 -12.33 -12.33	-12.34 -12.01 -12.29 -12.30 -12.33	-11.52 -12.34 -12.34 -12.39 -12.33 -12.33	-11.89	-11.35	-10.16 -11.35 -11.35 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -12.39 -13.55 -1	-10.31 -10.16 -11.35 -11.35 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -12.30 -13.50 -1	-9.09 -10.11 -11.05 -11.05 -11.05 -11.05 -11.05 -12.05 -10	-6.20 -0.09 -11.35 -11.35 -11.89 -11.89 -12.39 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -13.55 -13.	-7.19 -6.20 -6.20 -6.20 -6.20 -6.20 -11.35 -11.35 -11.35 -11.23 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -12.33 -13.55 -
-0.0695	-0.1150	-0.0777	-0.1259	-0.1390	-0.1239	-0.1629	-0.1040	-0.1555	-0.0653		-0.1315	-0.1778	-0.0484	-0.0741 -0.0484 -0.1778 -0.1315	-0.0741 -0.0741 -0.0481 -0.1778	-0.0942 -0.0942 -0.0741 -0.1778	-0.0741 -0.0942 -0.0741 -0.0741 -0.1778	-0.0484 -0.0741 -0.0942 -0.0741 -0.0741 -0.1778	-0.1778 -0.0484 -0.0484 -0.0942 -0.0942 -0.0741 -0.1778	-0.1315 -0.1778 -0.0484 -0.0741 -0.0741 -0.0741 -0.0741 -0.1778	0.0853 0.01215 0.01210	-0.1555 -0.0553 -0.0953 -0.0942 -0.0953 -0.0954 -0.0954 -0.0953 -0.0954 -0.0054 -0.005	-0.1040 -0.1335 -0.1335 -0.1335 -0.0484 -0.0484 -0.0484 -0.0484 -0.0484 -0.0484 -0.0484	-0.1629 -0.1629 -0.1010 -0.1355 -0.1315 -0.1315 -0.1718 -0.0741 -0.0741 -0.0741 -0.0741 -0.0741 -0.1778	0.0110 0.0100 0.0100 0.0100000000	0.1390 -0.1255 -0.1040 -0.1040 -0.1040 -0.1046 -0.0415 -0.0410
0000.0	0.0000	00000 0	00000.0	0.000.0	0.000	0.000	00000 0	0.000	0000-0		0.0000	0.0000	0.0000	00000.0	0.0000	000000000000000000000000000000000000000	0000.00000.0000000000000000000000000000	0000.0000000000000000000000000000000000	0000.0000000000000000000000000000000000							
0.0000	0.0000	0.000	0.0000	0.000	0.000	0.0000	0.0000	0.000		0.0000	0.0000	0.0000	0.0000 0.0000 0.0000	0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0,000 0,000000	0,000 0,000000	0,000 0,000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0.0000 0.0					
0.0000	0.0000	0.0000	0.0000	0.0000	0.000.0	0.0000	0.000	0.0000		0.0000	0.0000	0.0000	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.000 0.0000 0.000000	0,0000 0,00000 0,00000 0,00000 0,000000	0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	0000 0 0 0000 0 0 0000 0 0 0000 0 0 0000	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.000000					
0.000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.000	0.0000	~000°		0.0000	0.000	0.0000	0.0000	0.0000	000000000000000000000000000000000000000	0.0000	0.0000	000000000000000000000000000000000000000							
0.000	0.0000	0.000	0.000	0.000	0.000	0.0000	0.000	0.0000		0.0000	0.0000	0.0000	0.0000	0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0000.0000.0000.0000.0000.0000.0000.0000.0000	0.000 0.0000 0.0000 0.0000 0.000000	0000 0000 0000 0000 0000 0000 0000 0000 0000	0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000		0.000 0.0000 0.0000 0.0000 0.0000 0.00000 0.000000					
9.6312	9.6312	0.8936	2.111.2	2.7025	3.2914	4.3104	4.7406	5.1707		1 2627	6.1246	6.1246	6.7362 6.3864 6.1246	6.8241 6.7362 6.3864 6.1246	6.9121 6.8241 6.7362 6.7364 6.1246	6.9121 6.9121 6.8241 6.7362 6.3064 6.1246	6.8241 6.9121 6.921 6.9241 6.7362 6.1246	6.7362 6.8241 6.9121 6.9121 6.3241 6.3266 6.2766 6.2246	6.3864 6.7362 6.9121 6.9121 6.9121 6.7362 6.7363 6.7363	6.1246 6.3364 6.7362 6.7362 6.9121 6.9121 6.9241 6.3241 6.3245 6.3246 6.2466	5.8627 6.1246 6.1246 6.9121 6.9121 6.9121 6.9121 6.9121 6.9124 6.91246	5.1705 5.1867 6.1864 6.1864 6.1216 6.1216 6.1216 6.1216 6.1266 6.1266 6.1266 6.1266 7.565 7.565	4.7405 5.827 6.1246 6.1246 6.1246 6.2124 6.3121 6.3121 6.3121 6.321 6.2162 6.1262	4.7104 4.7107 5.1707 6.1246 6.23664 6.9121 6.9121 6.9121 6.9121 6.2166 6.2166 6.1266	1.2914 4.700 4.700 5.8627 5.8627 6.7362 6.7362 6.7362 6.7362 6.7362 6.7362 6.7362 6.7362 6.7363 7.7363 7.7377 7.737777777777	2.27025 4.1104 4.1104 6.1246 6.1246 6.1246 6.1246 6.0241 6.0241 6.0241 6.0241 6.0246 6.0241 6.0246 7.0246 7.0246 7.0246 7.02666 7.02666 7.02666 7.026666 7.02666666666666666666666666666666666666
1.7500 ion:	7.7500 1																									1,12214 1,2224 1,2224 1,2224 1,2225 1,2525 1,126
ef calculat of calculat on 0.01 don	1.9930 5																									7,7,220 8,5,292 8,5,292 8,5,292 1,1,200 1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1
Time o Versio	003 8																									90010002 8 90010002 8 90040002 8 90040002 8 90050002 9 90050002 9 90050002 9 90050002 9 90050002 9 90050002 9 90070002 9 900700002 9 9007000000000000000000000000000000000



azningi (0	prisu (12	Marning! (051) Using default value: NROB=	e: NROB=		0							
Statik Result from EASY Sta Date = 12/21/2011 Values from INI-file	1/2011 1/2011	Statik Result from EASY Statical analysis Date = 12/21/2011 Time = 16:26:22 Values from THI-file	3 26:22									
Zero for the computer (small Limit for conjugate gradient Minimum stiffness of a point	e computer onjugate g	Zero for the computer (small number) Limit for conjugate gradient Hinimum stiffness of a point		0.1000000000000000000000000000000000000	001-00							
Maximum numbers of Maximum numbers of Maximum Numbers of Maximum States of Maximum S	bers of ou bers of in culation	Maximum numbers of outer iterations Maximum numbers of inner iterations Kind of calculation			200							
Line from EJN-file: Statik: Statical analysis	iN-file: tical anal	sisy										
Dimensions:												
Number of p	oints	Number of points (HAX)		HAXI	568	20000						
Number of f	willy fixed	fully fixed points.		::	84							
Number of a	11 Links	Number of all links		HAX)	844	40000						
	inks contr	links controlled by Hookes law.	kes law.	: :	844							
Number of 1	inks contr	links controlled by force density	ce densit	····	•							
Number of t	-elements.	t-elements(HAX)		HAX)	142	4000						
imit for c aximal num onjugate g	Limit for convergence: Maximal number of iter Conjugate gradient	Limit for convergence: Maximal number of iterations		0.1000	20 0E+00							
tatical ca	lculation	Statical calculation without loads										
nformation	is to solve	Informations to solve equations with the method of conjugate gradient	fth the m	ethod of c	conjugate	gradient	÷					
umber of 1	Number of inner iterations	tions		residual		right side						
esults fro	m calculat	0 0 400 Results from calculation of equilibrium		0.0000010		10-36989.0						
tatik: Sta	Statik: Statical analysis	yaka		15	Statik	12/21/201116:26:22	:26:22					
Nodes		Coordinates		Coord	Coordínate changes	anges	ldγ	Applied nodes		Rest	Residual forces	ces
PointNo.	X-CODE	Y-COOF	2-COOF	X	λq	20	ReaX	ResY	ResZ	Þ	>	*
99000002	83.3500	59.0000	9.0000	0.0000	0.0000		0.0000	0.0000	0.0000	0.15	0.00	-0.09
60000066	1226.00	0.000	11.5248	0.0000	0.0000		0000	00000	00000			

5.6008	15.6008
0.0000	0.0000
0.0000 0.0000	0.0000
	0.0000
	0.000
0.0000 0.0000	0.0000
0.0000	
0.0000	•
0.0000	•
0.0000	•
0.0000	
0.000	
0000.0	00000 0 2557.11
0000.0	
0000	
0.0000	
0.0000	
0.0000	•
0.0000	
0.000	
	0000 0 FLOG 81
0.0000	c
0.0000	
0.0000	15.8129 0.0000
0,0000	15.0109 0.0000
0.0000	
0.0000	•
0.000	
0.0000	
0000.0	
0.0000	•
0.0000	•
0.0000	•
0.0000	•
0.0000	•
0.0000	•
0000	•
	>

 Normer
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1
 1/1<

640

644

. 641

645

642

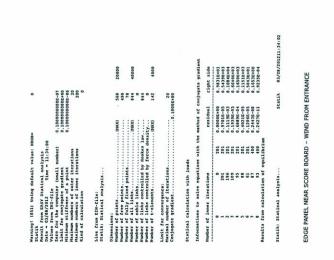
646

LIVE LOAD	BOARD -	AR SCORE	EDGE PANEL NEAR SCORE BOARD - LIVE LOAD	EDGE	٦								F	IND UPLIF	ARD - WI	SCORE BO	EL NEAR S	EDGE PANEL NEAR SCORE BOARD - WIND UPLIFT	
					4														
ac DX	OF 2-COOL	X-COOL Y-COOL	PointNo. X-C	Poir	b	6.68	5.24	-3.46	0.1807	-0.1414	0.0986	0.0000	0.0000	0.0000	9.6312	-3.7500	83.9930	90020001	
						-2.53		\$.35	0.2804	-0.2147	0.1563	0.0000	0.0000	0.0000	10.1381	-3.5720	83.3500	1001006	
Ceordin	ates	Coordinates	Nodes	-		-2.87	19.0-	6.87	0.2834	-0.2026	0.1501	0.0000	0.0000	0.0000	11.2236	-2.1036	83.3500	90010036	
						B6.1-		14.83	101C-0	-0.2048	C171.0	0.0000.0	0.0000	0.0000	13.2308	0.9467	83.3500	10010034	
Stat		analysis	Statik: Statical analysis	Stati		-4.26		13.82	0.3541	-0.1802	0.1810	0.0000	0.0000	0.0000	15.0109	4.1349	83.3500	90010032	
						-1.62		15.40	1610.0	-0.1585	0.1636	0.0000	0.0000	0.0000	15.8129	5.7755	83.3500	10001006	
	equilibrium	from calculation of	ts from calc	Results		-5.08	-1.03	18.11	0.3686	+611.0-	0.1900	0.0000	0.0000	0.0000	17.2352	5861.6	03.3500	90010029	
0.48328-11	400		•			-4.95		18.34	1676.0	-0.1256	0.1930	0.0000	0.0000	0.0000	17.0537	10.8566	83.3500	90010028	
0.29875-07	400	118				4.42		17.31	0.3428	-0.1023	0.1772	0.0000	0.0000	0.0000	19.4094	12.5961	83.3500	12001002	
90-396c1 0	102	EII	• •			10.0-		96.94	SCAL O	5060.0-	1984	0.000	00000	0.000	18.9014	14.3546	83.3500	90010026	
0.00001100	201	0.00	0+			-5.27	-0.66	21.18	9586.0	-0.0700	0.2004	0.000	00000	0.0000	19.12920	16.1299	0051.15	52001006	
			**********			-4.54		19.15	0.3876	-0.0557	0.2015	0.0000	0.000	0.0000	19.9895	19.7211	03.3500	001005	
residual		terations	Number of inner iterations	Number		-5.50		22.52	0.3563	-0.0386	0.1850	0.0000	0.0000	0.0000	20.2214	21.5324	0055.58	90010022	
informations to solve equations with the method of cor	ions with th	olve equati	mations to a	Infor		-5.32		22.19	0.3910	7610.0-	0.2034	0.0000	0.0000	0.000	20.4868	25.1743		90010020	
	spec	TON VIEN LC	statical calculation with loads	SCALL		-5.31	0.14	20.14	0.3910	0.0007	0.2036	0.0000	0.0000	0.0000	20.5200	27.0000	83.3500	61001006	
						-5.79		23.50	0.3529	0.0259	0.1834	0.0000	0.0000	0.0000	20.3872	30.6491		1001006	
						-5.46		22.49	0.3952	0.0434	0.2047	0.0000	0.0000	0.0000	20.2214	32.4676		90010016	
faximal number of iterations		terations	Maximal number of iterations.	Conju		-5.26	0.67	21.15	0.3858	1120.0	0.2004	0.0000	0.0000	0.0000	19.6920	34.2789		90010015	
		ence:	imit for convergence:	Limit		-5.50		21.49	+COC.0	0.0859	0.1990	0.0000	0.0000	0.000	19.3291	1018.11	93.3500	CT001006	
(XY44) · · ·			(XV4)	a crum N		1.1		11.23	C.01.0	0011.0	161.0	0000.0	0000.0			**** of		21001005	
nsity	y force der	ontrolled b	r of links o	Number		-4.93		18.27	0.3736	0.1276	0.1930	0.0000	0.0000	0.0000	17.8537	43.1434		01001006	
	y Hookes 14	ontrolled b	Number of links controlled by Hookes law.	Number		-5.05	1.02	18.02	0.3692	0.1416	0.1904	0.0000	0.0000	0.0000	17.2352	44.8615	-	9001009	
···· (NAX)		KS	sumber of sil links	Number		1.51		16.16	0.3520	0.1416	1111 0	0.0000	0.0000	0.0000	16.5546	46.5559		0001006	
		ixed points	Number of fully fixed points	Number		-4.24		13.68	0.3112	0.1592	0.1598	0.0000	0.0000	0.0000	15.0109	49.8651	83.3500	90001006	
		ints.	Number of free points.	Number		18.4-	0.96	14.63	0.3642	0.2031	0.1852	0.0000	0.0000	0.0000	14.1498	51.4754	83.3500	90010005	
1ANN			Dimensions: Aumher of moints	Dimen		-2.86		8.21	0.3056	0.2025	0.1547	0.0000	0.0000	0.0000	12.2349	1965.95	0050.08	10001006	
		•				-2.51		6.39	C1CC.0	0.2390	0.1774	0.0000	0.0000	0.000	11.2236	56.1036	83.3500	90010002	
		analysis	statik: Statical analysis	Stati		1.14		10.0-		E821.0	1111.0	0.0000	0.0000	0.0000	1901.01	57.5720		10001006	
						0.25		-10.35		1160.0	0.0758	0.0000	0.0000	0.0000	10.88.01	7447.74	88.3218	01000066	
						9.59		-12.75		0.1038	0.1222	0.0000	0.0000	0.0000	15.6008	41.0683		60000066	
	LACIOUS	C INNEL ICE	saximum numbers of inner iterations sind of calculation	Kind o		10.18	0.00	-15.45	8052.0	0.0000	1110.0	0000 0	00000	0000	16.6483	14.1063	91.1417	80000066	
	rations	f outer ite	faximum numbers of outer iterations	Haxim		9.82		-14.80		-0.0296	0.0628	0.0000	0.0000	0.000	16.6483	19.8937	1101.1417	9000006	
0.1000000000		of a point	Minimum stiffness of a point	MINIM		9.60		-12.84		-0.1038	0.1222	0.0000	0.0000	0.000	15.6008	12.9317	90.0746	50000066	
0.1000000000	(lagunu	uter (small	tero for the computer (small	CIA2		8.17		-6.22	8910.0	-0-1957	0.1242	0000.0	00000 0	00000	852C.11	1955	1276.00	F0000066	
		ile .	Values from INI-file	Value		10.01		0.21	0.0746	-0.0595	0.0424	0.0000	0.0000	0.0000	0000 6	-5.0000	0020.08	2000002	
	Time = 16:26:31	Time	Date = 12/21/2011	Date -		10.01	0.08	0.21	0.0746	0.0595	0.0424	0.0000	0.0000	0,0000	9.0000	59.0000	83.3500	10000066	
			Statik	Statik		*	>	Ð	Rest	ResY	ResX	20	μ	X	Z-C001	Y-COOL	X-COOK	PointNo.	
-00	value: NRC	ing default	farning! (051) Using default value: NROB-	MAENAL														000000000000000000000000000000000000000	

ate = 12/21/2011	/2011	ate = 12/21/2011 Time = 16:26:31 alues from TNT-file	:26:31									
the second secon	computer computer finess of ers of in ers of in ulation	reo for the computer (amail number) rest for computer gradient Inition stiffness of a point axisum numbers of outer iterations and any autor structions and of calculation	ber) ons	0.100000000000000000000000000000000000	200 200 200 000 000 000							
ine from EIN-file: tatik: Statical analysis	N-file: ical anal	ysås										
imensions: umber of points	ints	: points (HAX) free points				20000						
umber of al	1 links.	umber of all links				10000						
umber of li umber of li umber of t-	nks contr nks contr elements.	umber of links controlled by Hookes law umber of links controlled by force density umber of t-elements	okes law		142	4000						
imit for convergence: aximal number of iter onjugate gradient	nvergence er of ite adient	imit for cenvergence: aximal number of tecations. onjugate gradient		init for convergance: aximal number of iterations	-00 +00							
tatical calculation with loads nformations to solve equations	culation to solve	with loads	with the	catical calculation with loads mformations to solve equations with the method of conjugate gradient	njugate gr	adient						
umber of inner iterations	ner iterations	tions		residual	right side	ide						
0 1 2 3 3 4 4 4	calculat	0 0 201 1 201 201 201 2 113 400 3 112 400 400 400 400 400 400 400 400	201 201 201 201 400 400	0.000025+00 0.38155-06 0.12965-05 0.28875-07 0.48322-11	0.43025+01 0.61155+02 0.89015+01 0.11335+00 0.10735-00	10++						
tatik: Statical analysis	ical anal	yais		Stat	Statik 12/	12/21/201116:26:32	:26:32					
Nodes		Coordinates		Coordir	Coordinate changes	5	łdę	Applied modes		Residu	Residual forces	
PointNo.	X-coor	Y-COOF	2-C00E	Xa	λū	20	ResX	ResY	Res2	9	>	3

# Anhalt University of Applied Sciences, Dessau

150



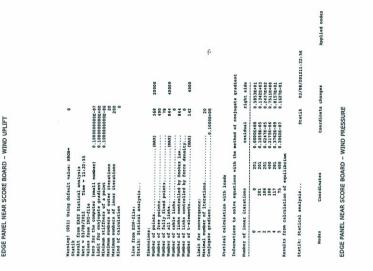
Nodes	-	Coordinates		Coord	Coordinate changes	safe	PA N	Applied nodes	2	Resi	Residual forces	ces
PointNo.	X-coor	Y-COOL	2-COOF	XQ	DY	20	ResX	ResT	Rest	Ð	>	
10000066	83.3500	59.0000	9.0000	0.0000	0.0000	0.0000	0.0424	0.0595	0.0746	0.21	0.08	0.0
9900002	83.3500	-5.0000	0000 6	0.000	0.000	0.0000	-0.0195	0.0274	+0.0344	0.12	0.04	-0.1
0000066	85.9221	0000.0	11.5240	0.000	0.0000	0.0000	-0.0573	0.0903	-0.1462	-7.80	4.22	4.6
10000066	88.3218	6.2553	13.8603	0.000	0.0000	0.0000	-0.0350	0.0420	-0.1020	+6.61-	3.20	4.7
	9410.04	1166.21	12.6008	0.000	00000	0.000	-0.0564	0.0479	-0.1680	-15.77	5.22	5.1
	1161.14	1068.61	19-9193	0.000	0.0000	0.0000	-0.0290	0.0136	-0.0892	-17.50	2.45	4.5
		0000.17	0000-11	0000	0000.0	0.000	0.0513	0.0050	0.1717	-5.75	0.10	3.2
					0000.0	0.000	0.0628	0.0296	0.1932	-16.31	-0.81	10.8
			8009.01	0000	0.0000	0.000	0.1222	0.1038	0.3640	-14.11	-2.64	10.0
otononee	8177.00	1661-16	CO88.CT	0.000	00000	0.0000	0.0758	1160.0	0.2210	-11.34	-2.23	8.3
11000066	1226.58	0000	11.5248	0.0000	0.0000	0.0000	0.1242	0.1957	0.3166	-6.42	-5.27	7.4
TODOTOO	00000.00	07/2-10	THEY OF	0.000	00000	0.0000	11111.0	0.1783	0.2325	5.34	0.23	-2.6
20001000		9601.90	11.2236	0000	0.0000	0.0000	0.1774	0.2390	CICC.0	6.50	0.45	-2.5
10001006	0000	24.5967	12.2549	0.000	0.0000	0.000	0.1547	0.2025	0.3056	8.58	0.65	-3.0
10001006	83. 3500	0223	13.2308	0.0000	00000	0.0000	0.1713	0.2083	0.3413	10.21	0.78	-3.3
50001006	83.3500	51.4754	14.1498	0.000	00000	0.0000	0.1852	1602.0	2196.0	14.93	1.06	-5.00
90001006	0000.00	1098.65	6010.01	0.0000	0.0000	0.0000	0.1598	0.1592	0.3112	14.18	1.05	-
10001006	0000.00	C122.85	15.8129	0.000	0.0000	0.000	0.1855	0.1697	0.3620	13.54	1.07	8.6-
80001006	0050.08	46.5559	16.5546	0.0000	0.000	0.0000	1171.0	0.1416	8000.0	17.30	1.26	-4.9
0001000	83.3500	44.8615	17.2352	0.000	0.0000	0.000	0.1904	0.1416	0.3692	18.70	1.28	-5.30
01001006	83.3500	\$C\$1.C\$	17.8537	0.0000	0.000	0.0000	0.1930	0.1276	0.3736	19.19	1.28	-5.2
11001006	0050.08	41.4039	18.4094	0.000	0.0000	0.0000	0.1977	0.1150	0.3033	18.61	1.23	-4.71
90010012	83.3500	39.6454	18.9014	0.0000	0.0000	0.0000	0.1782	0.0898	0.3442	20.98	1.28	-5.42
C1001006	83.3500	1018.76	19.3291	0.0000	0.0000	0.000	0.1990	0.0859	\$202.0	22.51	1.28	-5.81
1001006	83.3500	36.0805	19.6920	0.0000	0.0000	0.0000	0.2004	0.0717	0.3858	22.42	1.21	-5.6]
80010013	83.3500	34.2789	19.9895	0.0000	0.000	0.0000	0.2012	0.0573	0.3878	20.67	1.07	-4.9
9001006	0050.0500	32.4676	20.2214	0.0000	0.0000	0.0000	0.2047	0.0434	0.3952	23.76	1.14	-5.7
1001006	83.3500	30.6491	20.3872	0.000	0.0000	0.0000	\$C81.0	0.0259	0.3529	10.02	1.03	-5.7
81001006	0050.08	20.8257	20.4868	0.0000	0.0000	0.0000	0.2036	0.0152	0.3910	17.81	0.75	-4.3
61001006	83.3500	27.0000	20.5200	0.0000	0.0000	0.0000	0.1429	0.0029	0.2738	7.54	0.31	-2.13
90010020	83.3500	25.1743	20.4868	0.0000	0.000	0.0000	-0.0866	0.0060	-0.1664	7.29	0.40	-4.23
12001006	83.3500	23.3509	20.3872	0.000	0.0000	0.0000	-0.0938	0.0130	-0.1807	12.79	6.73	-7.9
90010022	63.3500	21.5324	20.2214	0.000	0.000	0.0000	-0.0854	0.0179	-0.1644	16.11	0.91	-10.15
62001006	0056.68	19.7211	19.9895	0.0000	0.0000	0.0000	-0.0930	0.0257	-0.1789	16.26		-10.23
90010024	83.3500	2616.71	19.6920	0.0000	0.0000	0.0000	-0.0925	0.0323	-0.1780	15.45		-9.74
52001006	0050.08	16.1299	19.3291	0.000	0.0000	0.0000	-0.0917	0.0389	-0.1768	14.78	0.80	-9.30
92001006	0055.58	14.3546	10.9014	0.0000	0.0000	0.000	-0.0916	0.0459	-0.1772	15.12	0.80	-9.42
12001005	0052.58	12.5961	18.4094	0.000	0.0000	0.0000	-0.0818	0.0472	-0.1582	15.35	61.0	-9.4
87001005	0000.00	10.6560	11.8537	0.000	0.000	0.0000	1680.0-	0.0580	-0.1722	13.32	0.69	-8.23
67001000	0005.50	CB51.6	262.11	0000 0	0.000	0.0000	-0.0877	0.0643	-0.1701	12.43	0.64	-7.65
ACONTOOS	0000.00		10.3346	0.0000	0.0000	0.0000	-0.0887	0.0732	-0.1732	13.29	0.65	-8.0
TCOOTOOC	0000.00	CC11.0	6218.61	0.0000	0.000	0.0000	-0.0755	0.0686	-0.1473	11.89	0.56	-7.10
2001006	0000	665T-6	5010.51	0.0000	0.000	0.000	-0.0839	0.0832	-0.1634	10.28	0.50	-6.1
renotions.	0.000	0175.7	2651-5T	0.000	0.0000	0.0000	-0.0753	0.0819	-0.1475	10.44	0.48	-6.2]
LCOOTOOL	0000.00	1956.0	8052.51	0.000	0.0000	0.0000	-0.0791	0.0945	-0.1571	8.10	0.36	-4.67
CENTING	DOCC. 10	1962.0-	22.2349	0.0000	0.0000	0.0000	-0.0817	0.1069	-0.1621	8.51	66.0	1
SCOTORS	0055.58	-2.1036	11.2236	0.0000	0.0000	0.0000	-0.0693	0.0935	-0.1308	5.87	0.21	-3.43
	Contraction of the											
EDGE PANEL NEAR SCORE BOARD - WIND FROM ENTRANCE	EL NEAR S	SCORE BO	ARD - WI	ND FROM	ENTRANC	-						

5.08 -5.19 -5.19 -5.19 -5.19 -10.19 -11.07 -11.07 -11.07 -11.07 -11.07 -11.02 --0.0721 -0.0755 -0.0675 -0.0675 -0.07721 -0.0001 -0.0721 -0.07 10.1301 9.5512 10.2654 10.2654 10.2654 10.2654 11.2514 11.2514 11.2514 11.2514 11.2514 11.2104 11.2 -1,5720 -1,5720 -1,550 10,1500 10,10 11001000

b 52

648

6.14 6.54 6.54 6.54 6.54 112.02 12.02 12.05 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 11.99 12.77 11.99 11.99 11.99 11.99 12.77 11.99 11.9 -5, 66 -11, 39 -11, 39 -11, 30 0.1451 0.0657 0.12455 0.12455 0.12455 0.12455 0.12455 0.12455 0.12758 0.02758 0.12758 0.02758 2010-2024 2010-2024 2010-2014 -2.2500 1.2500 1.2500 1.2500 1.2501 1.2502 1.2512 1.2522 1.2502 1.4502 1.4602 1.2522 1.4602 1.2522 1.4602 1.2522 1.4602 1.2522 1.4602 1.2522 1.4602 1.2522 1.4602 1.25222 1.25222 1.25222 1.2522 1.25222 1.25222 1.25222 1. 4.551 15.229 15.229 15.229 17.229 



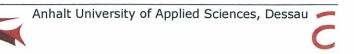
649

653

5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
5.0000
<p 

650

654



the last on the				
		equilibrium	ulation of	Results from calculation
0.92485-01	0.27598-08	400		
0.5083E+01	0.81822-06	201	63	9
20+3000.0	0.45456-05	201	60	s
0.16675+03	0.67002-04	201	96	•
0.6784E+03	0.18535-03	201	109	•
0.11652+04	0.11265-03	201	193	2
0.54585+03	0.9151E-05	201	201	1
0.97196+01	0.00005+00	201	•	•
right side	residual		Iterations	Number of Inner J
jugate gradien	with the method of conjugate gradien		tion with loads solve equations	Statical calculation with loads Informations to solve equations
20	convergence: Mber of Aterations		rgence: of iterations	Limit for convergence: Maximal number of iter Conjugate gradient
142 4000		····· (HAX)	-elements	Number of t-elene
				of Links
111		by Wookes law.	controlled b	of Links
0			links	Number of cable 1
344 40000	(HAX)		1 inks (HAX)	of all
78			fully fixed points.	10
568 20000	(XVH)		free points	Number of points.
				ons
			analysis	Line from EIN-file: Statik: Statical analysis
•			uo	Kind of calculation
200		iterations	inner	
20		<b>iterations</b>	outer	
-06	0.1000000000		od w	Hinimum stiffness of
00+	0.1000000000000000000000000000000000000		. 1	Limit for conjugate
			alls	Values from INI-file
		- 11:34:46	114	Date = 03/08/2012
		analvsis	Statical an	Result from EASY
•				

90020003 85.2791 90030001 86.2220 90030002 87.1220 90040003 87.7219 90040003 89.7819 90040003 89.1982 90040003 89.2564	1.2500	10.8936	0000 0								
				0.0000	0.000	-0.0395	0.0670	-0.0932	-5.97	1.24	0.0
		12.1137	0.0000	0.0000	0.000	-0.0671	0.0826	-0.1511	-10.08	0.76	3.8
		12.7025	0.0000	0.0000	0.000	-0.0726	0.0900	-0.1668	-9.76	1.25	3.05
		13.2914	0.0000	0.0000	0.000	-0.0585	0.0774	-0.1487	11.11-	1.05	3.9
		14.3104	0.0000	0.0000	0.000	-0.0789	0.0718	-0.1955	-12.12	0.93	10.6
-		14.7406	0.0000	0.0000	0.0000	-0.0509	0.0455	-0.1248	-13.71	1.09	
		15.1707	0.0000	0.0000	0.000	-0.0687	0.0636	-0.1866	-13.36	0.62	
		15.8627	0.0000	0.0000	0.000	-0.0400	0.0217	-0.1024	-14.69	0.16	
		16.1246	0.0000	0.0000	0.000	-0.0623	0.0331	-0.1578	-15.40	0.19	
		16.3864	0.0000	0.0000	0.000	-0.0798	0.0427	-0.2133	-14.75	1.65	
		16.7362	0.0000	0.0000	0.000	-0.0216	0.0041	-0.0580	-15.66	0.08	4.2
		16.8241	0.0000	0.0000	0.000	-0.0346	0.0061	-0.0890	-16.36	0.06	4.61
		16.9121	0.0000	0.0000	0.000	-0.0406	0.0071	-0.1130	-15.53	0.04	4.1.9
		16.9121	0.0000	0.0000	0.0000	-0.0406	-0.0071	-0.1130	-15.51	-0.04	
		16.8241	0.0000	0.0000	0.000	-0.0346	-0.0061	-0.0890	-16.37	-0.06	
		16.7362	0.0000	0.0000	0.0000	-0.0218	1900.0-	-0.0580	-15.64	-0.08	4.26
		16.3864	0.0000	0.000.0	0.000	-0.0798	-0.0427	-0.2133	ET.41-	-1.64	4.30
-		16.1246	0.0000	0.0000	0.000	-0.0623	100.0-	-0.1578	-15.40	-0.19	
		15.8627	0.0000	0.0000	0.000	-0.0400	-0.0217	-0.1024	-14.68	-0.16	
		15.1707	0.0000	0.000	0.0000	-0.0687	-0.0636	-0.1866	-13.35	19.0-	
		14.7406	0.0000	0.0000	0.000	-0.0509	-0.0455	-0.1248	-13.64	-1.10	
		14.3104	0.000	0.0000	0.000	-0.0789	-0.0718	-0.1955	-12.12	-0.93	3.91
		13.2914	0.0000	0.000	0.000	-0.0585	-0.0774	-0.1487	-11.04	-1.05	3.85
		12.7025	0.0000	0.000.0	0.0000	-0.0726	-0.0900	-0.1668	-9.64	-1.25	3.82
		7611.21	0.0000	0.0000	0.000	-0.0671	-0.0826	-0.1511	-10.01	-0.76	3.80
10110001 85.2791		10.8936	0.0000	0.000.0	0.000	-0.0395	-0.0670	-0.0932	-5.87	-1.25	2.93
-		10.2624	0.0000	0.000	0.000	-0.0670	-0.1027	-0.1380	-5.54	-1.03	30.0
90110003 83.9930		9.6312	0.0000	0.000	0.0000	-0.0455	-0.0653	-0.0814	-1.85	-2 44	
Statik: Time of calcul	- 2	0.964									

655

 Mode
 Control to the product of the produc

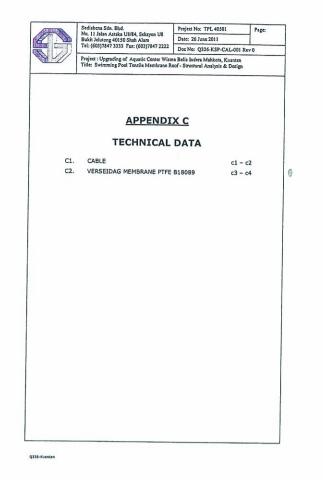
b56

 Note
 <th

EDGE PANEL NEAR SCORE BOARD ~ WIND FROM AUDIENCE STAND

Institute for Membrane and Shell Technologies

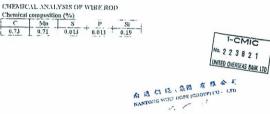




### NANTONG WIRE ROPE (GROUP) CO., LTD. MILL TEST CERTIFICATE DATE: Oct. 27 2005

	DATE. Oct. 27 2005
1. Manufactory	NANTONG BIRE ROPE (GROUP) CO., I TD.
2. Ordering company.	KENG WAII HARDWARE CO PTE LTD
3. 5/C No.	KWNT-0504
4. Length of rope	300 M
5. Rope diameter,	16 MM
5. Construction.	1×19
5 Kind of core.	
8. Surface of wire rope.	G.N 1
2. Nominal tensile strength.	1570 N/MM2
10. Nominal breaking force.	211.0 KN
11 Actual breaking force	215.5 XN
) 2. · ay	RHRI.
13. Total weight.	1.532 KGS
14. Amount of cail	1
15. J.uhe.	DRV.
16. Delivery date.	Oct 28, 2005

clured and delivered wir of above indicated order corr spond with the cal term of delivery acco ling to BS 302.



Manho Rope & Wire Ltd. 130-1, HWA MYOUNG-DON BUSAN, KORE P.O.BOX NO.277 DUSAN TELEX NO.83561. HEAD OFFICE TEL1332-31

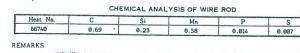
Chemical con

### Registered by AMERICAN BUREAU OF SHIPPING LLOYD'S REGISTER OF SHIPPING Sheet No. 2007 A-292-01-R1 Date SEP. 30. 2007

MILL TEST CERTIFICATE

Customer : Messr	S KENG WAH HARDWARD	E CO PIE LID				
Supplier : Messi	S MANHO ROPE & WIRE	E LTD.				
L/C No.			Order No		5	
Commodity PE CC	DATED GALVANIZED STR	EL WIRE ROPE				
Construction	6X37 IWRC		Grade			
rification	BS 302		Lubrication			
Order Quantity	300	feature m	Reel No	1		
Graza-Weight=	· · · · · · · · · · · · · · · · · · ·	Liber Hes =	Net Weight			Lbs=Kgs
		TEST RESU	LT			

Rope Dia 28X32 (Ac	ual) 28X32	Juck,mm Preform	ing GOOD	
Kind of Lay RHRL		Length of Lay		Inch_mm
Actual Breaking Strength of	Wire Rope		51,300	Liber Kgs
Nominal Dia. of Wire				Ineh_mm
Tensile Strength of Wires	Min	Max		PSI-Kg/mm <sup>2</sup>
Number of Torsion of Wires	Min	Max		Times
Weight of Zinc Coating			· · · · · · · · · · · ·	g/m; QZ-/4+2



0

(203×280)

MHS- B102-30

Remarque : le dans le cadre d savoir actuel et

so total (g

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15<sup>TH</sup> MALAYSIA GAMES



# 

0

O

behaller

Base fabric Coating Total weight (g/m<sup>2</sup>) Width (cm<sup>3</sup>) Tensile strength (N/ Tear resistance (N) Adhesion (N/5 cm<sup>3</sup>)

CI

62

C3

duraskin<sup>≈</sup> B 18089 The reliable protection N 6 C4 duraskin\* Glasfaser EC'3/4 PTFE – Polytetrafluorethyler DIN EN ISO 2286-2 DIN EN ISO 2286-1 DIN 53354 DIN 533563 DIN 53357 DIN 5036 DIN 5036 DIN 5036 Kette/Schuss Kette/Schuss Type III Glass fibre EC 3/4 PTFE – polytetrafiue DIN EN ISO 22862 DIN EN ISO 22861 DIN 53354 DIN 53353 DIN 53357 DIN 53357 DIN 5036 DIN 4102 warp/welt O ilional certificates e range ± 5%. All Fibre de verre EC 3/4 PTFE - Polytétrafluoréthyléne DIN EN ISO 2286-2 DIN EN ISO 2286-1 DIN EN ISO 2286-1 DIN 53354 DIN 53355 DIN 53357 DIN 5036 DIN 4102 chaine/trame disponibles sur demande. Sous réser ne tolérance de ± 5%. Les indication Fibra de vidrio EC 3/4 PTFE - Politetrafiusrativo DIÑ ÉN ISÓ 2286-2 DIÑ ÉN ISÓ 2286-1 DIN 53354 DIN 53353 DIN 53357 DIN 53357 DIN 53357 DIN 4102 urdimbre/trama urdimbre/trama 0 D duraskin

Anhalt University of Applied Sciences, Dessau 🛹