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# First Principles Density Functional Theory Prediction of the Crystal Structure and the Elastic Properties of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>

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**Abstract:** The Molybdenum rich ternary alloys Mo-M-B (M = Zr, Hf) contain, next to the Mo solid solution (bcc Mo with small amounts of Zr or Hf as substitutional atoms), the binary borides Mo<sub>2</sub>B, MB and MB<sub>2</sub>. Recently, it was found that there is also ternary Mo<sub>2</sub>MB<sub>2</sub>, but the crystal structure and further properties are currently unknown. Density functional theory (DFT) calculations were used not only to predict the crystal structure of the Mo<sub>2</sub>MB<sub>2</sub> phases, but also to estimate the isotropic and anisotropic elastic properties like bulk, shear and Young's modulus, as well as the Vickers hardness of these new borides. Several known crystal structures that fulfill the criterion of the chemical composition were investigated, and the AlMn<sub>2</sub>B<sub>2</sub> type structure seems to be the most stable crystal structure for Mo<sub>2</sub>HfB<sub>2</sub> and Mo<sub>2</sub>ZrB<sub>2</sub> as there are no signs of electronic or dynamic instability. Regarding the elastic properties, it was found that Mo<sub>2</sub>HfB<sub>2</sub> shows higher elastic moduli and is less elastically anisotropic than Mo<sub>2</sub>ZrB<sub>2</sub>.

**Keywords:** density functional theory; elastic properties; crystal structure; borides; intermetallics; molybdenum based alloys

# 1. Introduction

There is a significant demand for new high-performance materials for technically challenging applications, e.g., in the metal processing industry, or in the energy generation and the aviation sectors. It is well-accepted that the materials capability affects the performance of machines, like turbines [1]. State-of-the-art materials for heavily stressed structural components are single-crystalline nickel-based superalloys. However, beyond ~1100 °C, the strength of these materials drops significantly and, thus, they become unusable for structural components.

The most challenging goal is to develop new high-temperature materials that provide balanced properties in a wide temperature range, i.e., sufficient fracture toughness at low and ambient temperatures, as well as creep strength and appropriate oxidation resistance at ultra-high temperatures. This target could be met by tailored refractory metal alloys, e.g., those based on molybdenum [2–5]. Mostly, the alloying strategy is due to the formation of temperature and oxidation-resistant intermetallic phases in a molybdenum solid solution matrix, like different silicides [6,7]. Recently, systems that incorporate borides as strengthening phases were described in terms of their microstructural evolution and mechanical properties, namely the ternary systems Mo-Hf-B and Mo-Zr-B [8–10]. It could be shown that this class of materials is very attractive in terms of a promising combination of high fracture toughness and outstanding creep resistance. The borides especially, e.g., ZrB, HfB or Mo<sub>2</sub>B, and the respective ternary borides that form in Mo-rich alloys, provide excellent creep resistance. Since boride phases, as well as the molybdenum solid solution phase, show a loss of environmental resistance at

intermediate temperatures, a coating strategy based on Si-N and Si-O ceramic phases was already developed [11].

However, there is a lack of data on the properties of the ternary phases, especially their thermodynamic stability within the ternary systems Mo-Hf-B and Mo-Zr-B. The latest versions of the respective phase diagrams were published by Rogl, which do not contain the Mo-rich ternary intermetallic phases [12,13]. In our preliminary work so far, we found undescribed ternary phases, which were provisionally named  $Mo_2HfB_x$  and  $Mo_2ZrB_x$  in previous publications [9,10]. More precise information on the exact chemical composition of the phases was derived from Atom Probe Tomography (APT) measurements [14,15]. These results give evidence on the type of phases to be  $Mo_2MB_2$  (M = Zr, Hf), but the crystal structure and stability of the phases is still unclear.

The prediction of the crystal structure of new materials or of known crystals at extreme conditions is an ongoing research topic. Diverse methods exist, e.g., Random Sampling [16], Simulated Annealing [17] and Evolutionary Algorithms [18], often in combination with Density Functional Theory (DFT) calculations. One drawback of using these methods, however, can be the high demand of calculation power and/or time. To overcome these drawbacks, a different approach was used to predict the crystal structure of  $Mo_2MB_2$  (M = Zr, Hf) by simply using known crystals structures of intermetallics with the 2-1-2 or 3-2 chemical composition within our DFT calculations.

### 2. Materials and Methods

Based on the measured chemical composition 2-1-2 for Mo, M (M = Zr, Hf) and B, respectively, for the new compounds [14,15], we took 50 crystal structures of already known 2-1-2 and 3-2 intermetallics that fulfill the above-mentioned criterion of composition. Of those 50 types of crystal structures, the nine that showed the lowest total energy were those of the AlMn<sub>2</sub>B<sub>2</sub>-type [19], the  $Mo_2FeB_2$ -type [20], the  $Nb_2OsB_2$ -type (a superstructure variant of the  $Mo_2FeB_2$ -type) [21], the  $U_2Pt_2Sn$ -type [22] (also a superstructure variant of the Mo<sub>2</sub>FeB<sub>2</sub>-type, but no boride is currently known), the CeAl<sub>2</sub>Ga<sub>2</sub>-type (e.g., the known boride DyCo<sub>2</sub>B<sub>2</sub> [23]), the  $\beta$ -Cr<sub>2</sub>IrB<sub>2</sub>-type [24], the  $Mo_2IrB_2$ -type [25], the  $HoNi_2B_2$ -type [26] and the  $W_2CoB_2$ -type [27]. First-principles calculation were carried out with Quickstep [28], as implemented in the CP2K version 5.1 program package, for a first structural relaxation and a quick estimation of the total energy [29]. Using the Gaussian plane wave method (GPW) [30], for Mo, Zr, Hf and B, the DZVP-MOLOPT-SR-GTH basis was set [31] and GTH-pseudopotentials were chosen [32–34]. Cell shape and volume variations were allowed during the structural optimization until a total energy self-consistency of  $10^{-8}$  Ha and until the self-consistency for the forces and maximum geometry change of  $10^{-6}$  Ha/Bohr and  $10^{-6}$  Bohr, respectively, were achieved. The energy cut-off for the plane waves on the grid was 600 Ha, and the k-meshes were sampled via the Monkhorst–Pack algorithm [35]. Exchange and correlation in this density functional theory (DFT)-based method were treated with the generalized gradient approximation (GGA) functional as parameters by Perdew, Burke and Ernzerhof (PBE-GGA) [36]. Additionally, the PHONOPY program [37] was used to check for the dynamically most stable structure, similar to an approach made in Ref. [38].

The Density-Of-States calculation was done on the most stable energy ground-state structure using the tight-binding, linear muffin-tin orbitals with the atomic spheres approximation (TB-LMTO-ASA) [39,40] as implemented in the TB-LMTO 4.7 program. The Fermi level ( $E_F$ ) was set to 0 eV. The Monkhorst–Pack algorithm generated k-mesh was 27 × 27 × 27. Exchange and correlation were treated with the PW91-GGA functional by Perdew et al. [41]. The bonding analysis was done by calculation of the crystal orbital Hamilton population (COHP) [42] and its integrals (ICOHP). The ICOHP can be seen as a semi-quantitative bonding energy that measures covalent contributions in solids.

For the calculation of the elastic properties, a further structure optimization of the most stable crystal structure was carried out with Quantum ESPRESSO [43,44] using PAW pseudopotentials [45] from the PSLibrary version 1.0.0 [46]. The kinetic energy cut-off of the plane waves was set to 100 Ry, while the cut-off for the charge of density and potential was set to 400 Ry. The structural relaxation stopped until a total energy convergence of  $10^{-6}$  Ry and a force convergence of  $10^{-5}$  Ry/Bohr were

reached. The Marzari–Vanderbilt cold smearing [47] and a Gaussian spreading of 0.01 Ry were chosen to account for the Brillouin-zone integration in metals. The k-mesh was divided by  $20 \times 4 \times 20$  using the aforementioned Monkhorst–Pack algorithm. Exchange and correlation in this density functional theory (DFT) based method were again treated with PBE-GGA. The elastic properties were determined with thermo\_pw [48], a Fortran program using Quantum ESPRESSO routines as the underlying engine. In order to get the Voight–Reuss–Hill [49–51] approximated bulk, shear and Young's modulus, the standard algorithm and frozen ions were used. To calculate the Vickers hardness, Tian et al.'s formula [52] was used. The formulas for the anisotropic bulk and Young's modulus were taken from Ref. [53], while the formula for the anisotropic shear modulus is based from the formula given in [54]. Because of the usage of directional cosines of the elastic constants along the *x*-, *y*-, *z*-, *xy*-, *xz*- and *yz*-directions (see Ref. [53]), the elastic moduli along the crystallographic {111} direction is the average of the {111} directions within the *ab-c-*, *ac-b-* and *bc-a-*plane, which is spanned by the vectors along {110} & {001}, {101} & {010} and {011} & {100}, respectively.

The elastic anisotropy was determined in two ways: First, we calculated the Universal Elastic Anisotropy Index using the Voigt and Reuss bulk and shear moduli [55]. Second, as there are maxima and minima of the anisotropic elastic moduli, one can make another estimation of the anisotropy for the bulk, shear and Young's modulus as well as the Vickers hardness using the following Formula (1) [56]:

$$EMAI = \frac{EM_{max}}{EM_{min}}.$$
(1)

*EMAI*: Elastic modulus anisotropy index;  $EM_{max}$ : Maximum of the elastic modulus;  $EM_{min}$ : Minimum of the elastic modulus.

If *EMAI* = 0, then the elastic modulus is isotropic; a higher *EMAI* should display a more anisotropic elastic modulus.

# 3. Results and Discussion

#### 3.1. Crystal, Electronic and Phonon Structure

To predict the crystal structure of a compound, the total energy per formula unit is the main decision criterion. Here, nine crystal structure candidates for  $Mo_2MB_2$  (M = Zr, Hf) and their total energy difference to the energetically most stable structure type will be presented: the AlMn<sub>2</sub>B<sub>2</sub>-type [19], the Mo<sub>2</sub>FeB<sub>2</sub>-type [20], the Nb<sub>2</sub>OsB<sub>2</sub>-type (a superstructure variant of the Mo<sub>2</sub>FeB<sub>2</sub>-type) [21], the U<sub>2</sub>Pt<sub>2</sub>Sn-type [22] (also a superstructure variant of the Mo<sub>2</sub>FeB<sub>2</sub>-type, but no boride is currently known), the CeAl<sub>2</sub>Ga<sub>2</sub>-type (e.g., the known boride DyCo<sub>2</sub>B<sub>2</sub> [23]), the  $\beta$ -Cr<sub>2</sub>IrB<sub>2</sub>-type [24], the Mo<sub>2</sub>IrB<sub>2</sub>-type [25], the HoNi<sub>2</sub>B<sub>2</sub>-type [26] and the W<sub>2</sub>CoB<sub>2</sub>-type [27].

Their calculated energy differences are shown in Figure 1. It is obvious that the AlMn<sub>2</sub>B<sub>2</sub>-type structure (see inlay of Figure 1) is the most stable one of all investigated structures for Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>. The AlMn<sub>2</sub>B<sub>2</sub>-type is a structure variant within the orthorhombic spacegroup *Cmmm*. The Mo<sub>2</sub>FeB<sub>2</sub>-type structure for Mo<sub>2</sub>ZrB<sub>2</sub> (Mo<sub>2</sub>HfB<sub>2</sub>) is less stable with an energy difference of +23 kJ/mol (+15 kJ/mol). The Nb<sub>2</sub>OsB<sub>2</sub> and U<sub>2</sub>Pt<sub>2</sub>Sn types are structurally unstable as they both changed towards the Mo<sub>2</sub>FeB<sub>2</sub>-type during the cell optimization. The CeRu<sub>2</sub>Al<sub>2</sub>-type,  $\beta$ -Cr<sub>2</sub>IrB<sub>2</sub>-type, Mo<sub>2</sub>IrB<sub>2</sub>-type, HoNi<sub>2</sub>B<sub>2</sub>-type and W<sub>2</sub>CoB<sub>2</sub>-type are even more unstable with energy differences of +24 kJ/mol (+55 kJ/mol), +42 kJ/mol (+54 kJ/mol), +51 kJ/mol (+60 kJ/mol), +109 kJ/mol (+132 kJ/mol) and +134 kJ/mol (+129 kJ/mol), respectively.

140

120





**Figure 1.** The calculated energy differences of the phases Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> per formula unit with the different types of crystal structures. \*: Unstable crystal structures, which turn to the Mo<sub>2</sub>FeB<sub>2</sub> type during the structural relaxation.

To check if the AlMn<sub>2</sub>B<sub>2</sub> type is electronically and dynamically stable, we also calculated the electronic Density-Of-States (DOS, Figure 2) and the Phonon-Density-of-States (PDS, Figure 3). In Figure 2 (left), the DOS of Mo<sub>2</sub>ZrB<sub>2</sub> shows no signs of electronic instabilities as the Fermi level lies in the vicinity of a local DOS minimum. However, the Fermi level of Mo<sub>2</sub>HfB<sub>2</sub> (see Figure 2, right) lies close to a small maximum of the DOS, which might indicate the formation of boron vacancies, but is no serious sign of an instability of the crystal structure. Because of the non-vanishing DOS at the Fermi level,  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  should be metals.

The PDS of  $Mo_2ZrB_2$  with the AlM $n_2B_2$  type structure in Figure 3 (left) contains no occupied imaginary frequencies and, hence, no dynamic instability is found. The same is valid for the PDS of  $Mo_2HfB_2$  (Figure 3, right).

In terms of geometry, the lattice parameters of  $Mo_2ZrB_2$  and of  $Mo_2HfB_2$  after the cell optimization with CP2k are presented in Table 1. After a further structural optimization for the subsequent calculation of the elastic properties (see Section 3.2) with Quantum ESPRESSO, the lattice parameters of  $Mo_2ZrB_2$ and  $Mo_2HfB_2$  do not change much (see also Table 1 for the respective volumes).

Because of the similar atomic radius in crystals of Zr and Hf (both 155 pm according to Slater [57]), the lattice parameters a and c of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> differ by less than 1%, while the difference for the lattice parameter b is about 2%. The difference might come from the slightly different chemical behavior of Zr and Hf.



**Figure 2.** Electronic density of states (DOS) of Mo<sub>2</sub>ZrB<sub>2</sub> (**left**) and Mo2HfB2 (**right**) both with AlMn<sub>2</sub>B<sub>2</sub>-type structure.



**Figure 3.** Phonon-Density-of-States (PDS) of  $Mo_2ZrB_2$  (**left**) and  $Mo_2HfB_2$  (**right**) both with  $AlMn_2B_2$ -type structure. The dashed boxes show that there are no imaginary phonon frequencies for  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ .

Compound	a (Å)	b (Å)	c (Å)	V (Å <sup>3</sup> )
Mo <sub>2</sub> ZrB <sub>2</sub>	3.145 (3.146)	12.59 (12.60)	3.208 (3.208)	127.1 (127.2)
Mo <sub>2</sub> HfB <sub>2</sub>	3.143 (3.141)	12.33 (12.35)	3.213 (3.212)	124.6 (124.6)

**Table 1.** Lattice parameters *a*, *b*, *c* and volumes of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  as calculated with CP2k (Quantum ESPRESSO).

In conclusion, the AlMn<sub>2</sub>B<sub>2</sub>-type is found to be the most energetic, electronic and dynamic stable structure for both  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ .

#### 3.2. Elastic Properties

#### 3.2.1. Isotropic Elastic Properties

In this section, the isotropic bulk, shear and Young's modulus along with the Vickers hardness of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  will be discussed (see also Table 2).

**Table 2.** Isotropic bulk modulus *B*, shear modulus *G*, Young's modulus *Y*, Vickers hardness  $H^V$  and the Universal Elastic Anisotropy Index  $A^U$  of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>.

Compound	B (GPa)	G (GPa)	Y (GPa)	$H^V$ (GPa)	$A^{U}()$
Mo <sub>2</sub> ZrB <sub>2</sub>	241.19	148.34	369.30	18.24	0.03
$Mo_2HfB_2$	250.31	158.73	393.11	19.81	0.02

It is clear that all the isotropic elastic moduli and the Vickers hardness of Mo<sub>2</sub>HfB<sub>2</sub> are higher than those of Mo<sub>2</sub>ZrB<sub>2</sub>.

The Universal Elastic Anisotropy Index [52] of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> was also calculated and while it is slightly larger for Mo<sub>2</sub>ZrB<sub>2</sub> than for Mo<sub>2</sub>HfB<sub>2</sub>, it is very small for both compounds. A deeper analysis of the anisotropic elastic properties is presented in the next subsection.

#### 3.2.2. Anisotropic Elastic Properties

In this section, the anisotropic elastic moduli bulk, shear and Young's modulus, along with the Vickers hardness of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , will be discussed. The discussion starts with the anisotropic bulk modulus shown in Figure 4.

The minimum of the anisotropic bulk modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  is 227.14 GPa and 239.41 GPa, respectively, and can be found along the {010} direction. Along the {100}, the bulk modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  is 257.32 GPa and 263.00 GPa, respectively, which is the maximum.

Taking into account the maximum and minimum of the elastic moduli of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>, one can make an assumption of the anisotropy (see Table 3): For the bulk modulus, the anisotropy is 0.13 and 0.10 for Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>, respectively.

**Table 3.** Anisotropy of the bulk, shear and Young's modulus as well as the Vickers hardness of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ .

Compound	B Anisotropy	G Anisotropy	Y Anisotropy	H <sup>V</sup> Anisotropy	B and G Averaged
	Index ( )	Index ( )	Index ( )	Index ()	Anisotropy Index ()
Mo <sub>2</sub> ZrB <sub>2</sub>	0.13	0.10	0.21	0.21	0.12
Mo <sub>2</sub> HfB <sub>2</sub>	0.10	0.08	0.18	0.18	0.09



Crystallographic direction

**Figure 4.** Anisotropic bulk modulus in the *a-b, a-c* and *b-c*-plane (**lower part**) and the *ab-c, ac-b* and *bc-a*-plane (**upper part**) of Mo<sub>2</sub>ZrB<sub>2</sub> (red, orange and purple) and Mo<sub>2</sub>HfB<sub>2</sub> (blue, cyan and black), respectively, both with the AlMn<sub>2</sub>B<sub>2</sub>-type structure.

The anisotropic shear modulus *G* is shown in Figure 5.

The shear modulus near the {011} direction in the *b*-*c* plane of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> is 139.93 GPa and 152.27 GPa, respectively, and it is the minimum. The maximum of the shear modulus is observed near the {101} direction in the *a*-*c* plane, as it is 153.26 GPa and 164.12 GPa, for Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>, respectively.

The anisotropic shear modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  within the *ab-c* plane, as well as the *a-c* plane, behaves differently. While within the *ab-c* plane, *G* of  $Mo_2HfB_2$  is only slightly changing, while *G* of  $Mo_2ZrB_2$  shows clear a clear minimum near the {111} direction and maxima near {110} and {001}. Within the *a-c* plane, *G* of  $Mo_2ZrB_2$  is almost constant between the {101} and {001} directions, while *G* of  $Mo_2HfB_2$  shows clear minimum and maxima between these directions. This different behavior of the

shear modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  also effects the Young's modulus and Vickers hardness in the same planes.



Crystallographic direction

**Figure 5.** Anisotropic shear modulus in the *a-b*, *a-c* and *b-c*-plane (**lower part**) and the *ab-c*, *ac-b* and *bc-a*-plane (**upper part**) of Mo<sub>2</sub>ZrB<sub>2</sub> (red, orange and purple) and Mo<sub>2</sub>HfB<sub>2</sub> (blue, cyan and black), respectively, both with the AlMn<sub>2</sub>B<sub>2</sub>-type structure.

Using the maximum and minimum shear modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , the anisotropy of *G* is 0.10 and 0.08 for  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , respectively (see also Table 3).

The anisotropic Young's modulus is shown in Figure 6.



Crystallographic direction

**Figure 6.** Anisotropic Young's modulus in the *a-b*, *a-c* and *b-c*-plane (**lower part**) and the *ab-c*, *ac-b* and *bc-a*-plane (**upper part**) of Mo<sub>2</sub>ZrB<sub>2</sub> (red, orange and purple) and Mo<sub>2</sub>HfB<sub>2</sub> (blue, cyan and black), respectively, both with the AlMn<sub>2</sub>B<sub>2</sub>-type structure.

The Young's modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  near the {110} direction in the *a-b*-plane is the minimum, as Y is 340.83 GPa and 371.43 GPa, respectively. The maximum of the Young's modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  is 411.43 GPa and 438.21 GPa, respectively, and it is found along the {100} direction.

Taking into account the maximum and minimum Young's modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , the anisotropy of Y is 0.21 and 0.18 for  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , respectively (see also Table 3).

In Figure 7 the anisotropic Vickers hardness  $H^V$  of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> is shown.



Crystallographic direction

**Figure 7.** Anisotropic Vickers hardness in the *a-b*, *a-c* and *b-c*-plane (**lower part**) and the *ab-c*, *ac-b* and *bc-a*-plane (**upper part**) of Mo<sub>2</sub>ZrB<sub>2</sub> (red, orange and purple) and Mo<sub>2</sub>HfB<sub>2</sub> (blue, cyan and black), respectively, both with the AlMn<sub>2</sub>B<sub>2</sub>-type structure.

The anisotropic Vickers hardness was calculated using the bulk and shear modulus according to the formula of Tian et al. [52]. The minimum of the Vickers hardness of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> is along the {100} direction, as  $H^V$  is 16.13 GPa and 17.48 GPa, respectively. However, the maximum of the Vickers hardness of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> is along different crystallographic directions. Near the {110} direction in the *a-b* plane, the maximum Vickers hardness of Mo<sub>2</sub>ZrB<sub>2</sub> is 19.47 GPa, while for the same direction, the  $H^V$  of Mo<sub>2</sub>HfB<sub>2</sub> is 20.62 GPa, which is not the maximum  $H^V$  of Mo<sub>2</sub>HfB<sub>2</sub>. The maximum Vickers hardness of Mo<sub>2</sub>ZrB<sub>2</sub> is 18.85 GPa. The experimental Vickers hardness of Mo<sub>2</sub>ZrB<sub>2</sub> is 19.50 GPa [10,14]; thus, the DFT calculated numbers of the anisotropic Vickers hardness are in very good agreement with the experiment. Unfortunately for Mo<sub>2</sub>HfB<sub>2</sub>, no experimental Vickers hardness is currently known.

Taking into account the maximum and minimum Vickers hardness of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , the anisotropy of  $H^V$  is 0.21 and 0.18 for  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ , respectively, which is similar to the one of Y (see also Table 3).

In summary, the anisotropic bulk, shear and Young's modulus as well as the Vickers hardness of  $Mo_2HfB_2$  are for the same directions in the same plane higher than the elastic moduli of  $Mo_2ZrB_2$ , which might be due to their respective interatomic bonding conditions. This hypothesis will be investigated in Section 3.3. The maxima of the bulk and Young's modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$ were observed for the {100} direction, while the maximum of the shear modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  was found near the {101} direction. The maximum of the Vickers hardness of  $Mo_2ZrB_2$  was found near the {110} direction, while the maximum of the Vickers hardness of  $Mo_2ZrB_2$  was found near the {110} direction, while the maximum of the Vickers hardness of  $Mo_2HfB_2$  is near the {101} direction. The minimum of the bulk modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  is along the {010} direction, while the minimum of the shear modulus of these borides is along the {011} direction. The minimum of the Young's modulus of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  is along the {110} direction, while for the Vickers hardness the minimum is along the {100} direction.

Also, the elastic moduli of  $Mo_2HfB_2$  are less anisotropic than the elastic moduli of  $Mo_2ZrB_2$ . To better compare this with the Universal Anisotropy Index  $A^U$ , one can also define a *B* and *G* averaged anisotropy index and for  $Mo_2HfB_2$ ; this is 0.09 ( $A^U = 0.02$ ), while for  $Mo_2ZrB_2$  it is 0.12 ( $A^U = 0.03$ ). The similarity of the calculated *B* and *G* averaged anisotropy index and the Universal Anisotropy Index indicates that both indexes can be used to determine the elastic anisotropy, and that  $Mo_2ZrB_2$ and  $Mo_2HfB_2$  show only slightly elastic anisotropic behavior.

#### 3.3. Influence of the Chemical Bonding on the Elastic Properties

In this section, we will use the integrated crystal orbital Hamilton population (ICOHP) as a measure for the strength of the chemical bonding to explain the differences of the elastic properties between Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>. The respective ICOHPs per bond type are presented in Table 4.

Bonds (Number)	Direction Along Axis	ICOHP of the Bonds in Mo <sub>2</sub> ZrB <sub>2</sub> (eV)	ICOHP of the Bonds in Mo <sub>2</sub> HfB <sub>2</sub> (eV)
B-B (2×)	ab	-6.56	-6.67
M-B (2×)	b	-2.51	-2.79
Mo-B, short $(4\times)$	ас	-9.09	-8.92
Mo-B, long $(2\times)$	bc	-3.80	-3.74
M-M, short $(2\times)$	а	-1.54	-1.66
M-M, long (2×)	С	-1.51	-1.58
Mo-M $(4\times)$	ab-c	-5.24	-5.62
Mo-Mo, short $(2\times)$	ab	-2.23	-2.13
Mo-Mo, medium (2×)	а	-1.65	-1.63
Mo-Mo, long $(2\times)$	С	-1.29	-1.24
Mo-Mo, longest $(1\times)$	b	-0.26	-0.36
Sum		-35.68	-36.33

**Table 4.** Integrated crystal orbital Hamilton population (ICOHPs) per formula unit of the Mo-Mo, Mo-M, Mo-B M-M, M-B and B-B bonds (M = Zr, Hf) in Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>.

The ICOHP of the bonds B-B short and long M-M (M = Zr, Hf), Mo-M and longest Mo-Mo are higher in  $Mo_2HfB_2$  than in  $Mo_2ZrB_2$ , while in  $Mo_2ZrB_2$ , the short and long Mo-B bonds and the short, medium and long Mo-Mo bonds are stronger than in  $Mo_2HfB_2$ . If one sums up these ICOHPs, it becomes clear that the chemical bonding in  $Mo_2HfB_2$  is stronger than in  $Mo_2ZrB_2$ . This might be the explanation why the elastic moduli of  $Mo_2HfB_2$  are larger than the elastic moduli of  $Mo_2ZrB_2$ . A similar correlation of ICOHP per formula unit and the elastic moduli were also found in other  $A_2MB_2$  borides (A = Nb, Ta; M = Fe, Ru, Os) [56,58].

However, the ICOHPs of individual bonds alone are not sufficient to explain the different behavior of the anisotropic shear modulus *G* of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> within the *ab-c* and *a-c* plane. A closer look at the bonding situation reveals that the Mo-Mo, Mo-M and M-M bonds are along the *a*, *c*, *ab* and *ab-c* directions and, thus, for the directions, the different behavior of *G* was observed. The DOSs of Mo and Zr in Mo<sub>2</sub>ZrB<sub>2</sub> differ from the DOSs of Mo and Hf in Mo<sub>2</sub>HfB<sub>2</sub>, especially in the area between -5 eV and 0 eV (see Figure 2). Taking a look on the Phonon-Density-of-States of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub> (Figure 3), the PDSs of Mo and Zr show a similar dispersion between 5 THz and 8 THz, while, because of the higher atomic weight, the PDS of Hf is mainly at lower frequencies below 5 THz and shows no similar dispersion like the PDS of Mo. Therefore, these differences in the DOSs and the PDSs might explain the different anisotropic behavior of the shear modulus of Mo<sub>2</sub>ZrB<sub>2</sub> and Mo<sub>2</sub>HfB<sub>2</sub>. The influence of the electronic structure on the shear modulus was also observed in other A<sub>2</sub>MB<sub>2</sub> borides (A = Nb, Ta; M = Fe, Ru, Os) [56,58].

# 4. Conclusions

In this work, we predicted the crystal structure of  $Mo_2ZrB_2$  and  $Mo_2HfB_2$  to be of the AlMn\_2B\_2 type structure, as there are no signs of electronic or dynamical instability found in the DOS and the PDS, respectively. Further, we investigated the elastic properties of these ternary borides and the isotropic and anisotropic elastic moduli like the bulk, shear and Young's modulus, as well as the Vickers hardness, which of  $Mo_2HfB_2$  are higher than those of  $Mo_2ZrB_2$  because of the chemical bonding situation. Also, it was shown that  $Mo_2HfB_2$  is less elastically anisotropic than  $Mo_2ZrB_2$ .

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